NASA TECHNICAL MEMORANDUM

TABLES OF ISENTROPIC EXPANSIONS OF PARAHYDROGEN AND RELATED TRANSPORT PROPERTIES FOR TOTAL TEMPERATURES FROM 25 K TO 300 K AND FOR TOTAL PRESSURES FROM 1 ATM TO 10 ATM

Ву

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TABLES OF ISENTROPIC EXPANSIONS OF PARAHYDROGEN AND RELATED TRANSPORT

PROPERTIES FOR TOTAL TEMPERATURES FROM 25 K TO 300 K AND

FOR TOTAL PRESSURES FROM 1 ATM TO 10 ATM

By

Richard C. Haut* and Jerry B. Adcock NASA Langley Research Center

SUMMARY

The isentropic expansions of parahydrogen at various total pressures and total temperatures were numerically determined by iterating Mach number and by using a modified interval halving method. The calculated isentropic values and related properties are presented in tabulated form.

INTRODUCTION

The wind-tunnel has been the primary tool for experimental aerodynamic research and development for many decades. Because of the increase in size and speed of aircraft in recent years, a need has developed for an increase ground testing capability in terms of Reynolds number. This need has been well documented, for example, in reference 1 and 2. The need for a higher Reynolds number testing capability than presently exists is particularly apparent in programs aimed at the development of efficient transport aircraft or maneuvering fighter aircraft designed to operate at transonic speeds. A major problem in the transonic region is the effect of Reynolds number on shock boundary layer interactions, and in turn, on the aircraft stability and performance characteristics.

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At a given Mach number, the Reynolds number may be increased by using a heavy gas rather than air as the test gas, by increasing the size of the tunnel and model, by increasing the operating pressure of the tunnel, and by reducing the test temperature. The method chosen to increase Reynolds number will, in general, also affect dynamic pressure, mass flow rate, and the power consumption of the tunnel per unit run time. The use of a heavy gas is a well-known method of achieving high Reynolds number. However, the differences in the ratio of specific heats becomes important when compressibility effects become significant, thus making Freon-12 a questionable transonic test medium. The more common approaches of increased size and increased stagnation pressures involve serious problems related to such questions as construction and operating costs, model and support loads, and the possibility of providing continuousflow capability. The fourth method, that of reduced test temperature, appears to offer an attractive solution to the preceding problems. However, as the test temperature is reduced, the properties of the test gas will begin, at some point, to deviate from the properties of an ideal gas. At cryogenic temperature real-gas effects may become appreciable and these effects on the aerodynamic test results must therefore be analyzed in order to determine if a particular gas is acceptable as a wind-tunnel test gas at cryogenic temperatures.

A cryogenic wind-tunnel concept has evolved at NASA-Langley Research Center in which liquid nitrogen is sprayed directly into the tunnel circuit to cool the tunnel structure, remove the heat input from the drive fan, and balance the heat conducted through the tunnel walls. Nitrogen is the

resulting test gas using this cooling procedure. Throughout the evolution of the cryogenic wind-tunnel concept at NASA-Langley Research Center, experimental and theoretical studies have been made to access the suitability of cryogenic nitrogen as a test gas. After analyzing real-gas isentropic and normal shock solutions, and performing two-dimensional airfoil pressure tests, Adcock, Kilgore, and Ray in reference 3 concluded that the real-gas effects of nitrogen pose no problem as far as its use in a transonic wind tunnel operating at cryogenic temperatures and at stagnation pressures up to 5 atmospheres.

Nitrogen is, of course, not the only gas which might be considered for use at cryogenic temperatures. However, in order to assure similarity between the flow over the model in the wind-tunnel and the vehicle is flight, it is essential that any candidate test gas behave, for all practical purposes, like an ideal diatomic gas.

In addition to nitrogen, one of the most promising diatomic gase; is hydrogen. Due to its very low vapor temperature it is possible to achieve even higher test Reynolds numbers at a given total pressure by using cryogenic hydrogen rather than cryogenic nitrogen as the test gas. Alternatively, for a given size tunnel it is possible to achieve a required test Reynolds number at a lower total pressure in hydrogen than in nitrogen thus reducing model, sting, and balance loads.

As a part of a larger program aimed at determining the suitability as well as the practicality of using cryogenic hydrogen as a wind-tunnel

test gas, the various ratios describing isentropic expansions of parahydrogen" at various total pressures and temperatures have been determined
up to Mach 2 and compared with the corresponding values for an ideal
diatomic gas. In addition, the local isentropic expansion coefficient,
viscosity, thermal conductivity, and Prandtl number have also been
determined for the various combinations of pressure, temperature and Mach
number.

The purpose of this report is to present in tabular form the various isentropic expansion ratios and the corresponding transport properties of parahydrogen.

In order to expedite the publication of the tabular results no analysis is made in this paper.

SYMBOLS

A area

c speed of sound

H enthalpy

M Mach number

^{*}Equilibrium hydrogen consists of ortho- and parahydrogen molecules. The difference in the direction of spin of the protons in the hydrogen molecule results in the two forms of hydrogen; ortho, in which the spins are in the same direction, and para, where the spins are in opposing directions. When liquid hydrogen evaporates, the equilibrium condition is essentially pure parahydrogen. This stable condition can even be maintained at ambient temperatures.

P pressure entropy temperature T increment (i.e. AT increment of temperature) local isentropic expansion coefficient ζ density ρ Subscripts: i iteration value value used in subroutine ISENT total conditions Superscript:

sonic conditions

REAL-GAS ISENTROPIC SOLUTIONS

A computer program giving the thermodynamic and related properties of parahydrogen from the triple point to 300 K at pressures to 1000 bar was obtained from the National Bureau of Standards (NBS). The NBS program is an updated version of the one used by Weber in reference 4. Although the NBS program is slightly different from the one used by Weber, the uncertainty in the results are the same in each program and are discussed in the report by Weber. In order to make use of the NBS program, it was modified into a subprogram form (subprogram THERMO). The inputs to this subprogram are temperature and pressure, and the outputs are the thermodynamic and related properties.

Besides the main program, a subprogram (ISENT) was also developed that made use of THERMO. By using a modified interval halving technique, ISENT calculates pressure and other thermodynamic properties for a given temperature and entropy.

The main program basically centers around ISENT. By iterating on Mach number and employing a modified interval halving technique, the isentropic expansion of parahydrogen at various total temperatures and total pressures is calculated.

Other converging techniques, such as the Newton-Raphson and Müller methods were considered along with the interval halving technique. But, because of the additional calculations involved, which would mean calling THERMO more often, and due to the fact that a good first approximation could be made through the use of the ideal gas equations, the interval halving technique was selected.

Since the only region under consideration is in the gaseous phase, the saturation boundary was considered as the lower temperature and pressure limit and the calculations were stopped when the static pressure was within 10% of the saturation pressure at the particular static temperature. From a temperature point of view, this means that the static temperature was within approximately 1 K of the saturated condition.

Generalized flow charts for both the main program and subprogram ISENT are given in figure 1.

For the main program, the values of the total temperature and total pressure are initialized in step 1. The resulting total conditions (density, sound velocity, etc.) are then computed in step 2 using subprogram THERMO. In steps 3 through 7 the sonic conditions are determined using the interval halving technique. Step 8 is the start of the Mach number iteration and in steps 9 through 12 the conditions at the iterated Mach number are determined by using the interval halving method to converge on the corresponding static temperature. The ratios to the ideal gas values are computed in step 13 and the values are then printed in step 15.

ADDITIONAL FLOW AND TRANSPORT PROPERTIES Local Isentropic Expansion Coefficient

The pressure and density relationship for the isentropic expansion of a real-gas may adequately be described by the exponential equation

Ρ∝ρζ

where ζ is defined as the local isentropic expansion coefficient. For ideal gases this coefficient is constant and equal to the specific heat ratio. For real-gases, the coefficient of isentropic expansion is, in general, not equal to the specific heat ratio, and may vary. In this report the local isentropic expansion coefficient is defined as:

$$\frac{P_{i-1}}{P_i} = \left(\frac{\rho_{i-1}}{\rho_i}\right)^{\zeta}$$

The values of this coefficient are listed on the second page of each table in the second column.

It was previously stated that to assure similarity between the flow over a model in the wind-tunnel and the vehicle in flight, it is essential that any candidate test gas behave, for all practical purposes, like an ideal diatomic gas. In addition to this requirement, the transport properties of the test gas should vary approximately the same as the transport properties of the atmosphere. In particular, for heat transfer studies the variations of the thermal conductivity and Prandtl number are of importance. Similarly, for the study of viscous effects, the variations of viscosity and Reynolds number should be considered.

The program supplied by the National Bureau of Standards does not calculate the transport properties. The viscosity is determined using the equation given by McCarty in reference 5. In his report McCarty discusses the development by Diller in obtaining this equation and the estimation of the error involved.

Roder, McCarty, and Hall give a linear interpolation subprogram for thermal conductivity in reference 6. Reference 6 also contains a discussion of the sources of the data and an estimation of the error to be expected.

USE OF TABLES

The tables are separated by total pressure conditions and subdivided by total temperature values. The divisions are as follows:

Table number	Total pressure, atm	Subdivision	Total temperature, K
I	1.0	. A	25.0
-	, 5 - 2	B	30.0
		Ɓ C	40.0
		D	60.0
		E	80.0
		D E F G	100.0
		G	200.0
		H	300.0
II	3.0	A	30.0
		В	35.0
		C	40.0
		\mathbf{D}	60.0
		E	80.0
		F	100.0
		G	200.0
		H	300.0
III	5.0	A	35.0
		В	40.0
		C	60.0
		Ð	80.0
		E F	100.0
		F	200.0
		G	300.0
IV	8.0	A	40.0
		В	45.0
		C	50.0
		D	60.0
		臣 F G	80.0
		\mathbf{F}	100.0
			200.0
		H	300.0

Table number	Total pressure, atm	Subdivision	Total temperature, K
V	10.0	A	45.0
		В	50 .0
		C	60.0
		D	80.0
		E	100.0
		F .	200.0
		G	300.0

An explanation of the column headings is given in the section entitled Computer Output Dictionary, which immediately precedes the tables.

The last five columns of the first page of each table give the values of the various isentropic expansion ratios relative to the ideal diatomic gas values. For example, table II F at a Mach number of 1.0 gives a value of 0.9513 for the relative pressure ratio. This means that the real gas value of the pressure ratio necessary to expand to Mach 1.0 differs from the ideal gas value by 4.87%.

Some tables, for example table I A, have the statement "saturation boundary reached" printed on the last line. This means that at the last Mach number listed the static pressure is within 10% of the saturation pressure at that particular static temperature.

CONCLUDING REMARKS

The isentropic expansions of parahydrogen at various total pressures and temperatures were determined numerically by iterating Mach number and using a modified interval halving technique. These basic real-gas solutions and comparisons with the ideal diatomic gas solutions are

presented in tabular form for a range of total temperatures from 25 K to 300 K and a range of total pressures from 1 atm to 10 atm. Also included in the tables are the corresponding values of viscosity, thermal conductivity, Reynolds number per unit length, Prandtl number, and local expansion coefficient.

REFERENCES

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- 6. Roder, H. M.; McCarty, R. D.; and Hall, W. J.: Computer Programs for Thermodynamic and Transport Properties of Hydrogen (Tabcode-11). Nat. Bur. Stand. Tech. Note 625, 1972.

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(B) (C)

COMPUTER OUTPUT DICTIONARY

A*/A	ratio	of	critical	area	(where	the	local	speed	is	egusl	to
	4.7	7					- 7	تستندها			

the local speed of sound) to the local area

CP/CV ratio of the specific heat at constant pressure to the

specific heat at constant volume

MACH Mach number

PT total pressure, atm (1 atm = $101.3 \times 10^3 \text{ N/m}^2$)

P/PT ratio of static pressure to total pressure

RE/M Reynolds number per meter, m-1

RHOT total density g/cm³

RHO/RHOT ratio of static density to total density

SVT sound velocity at total conditions, m/sec

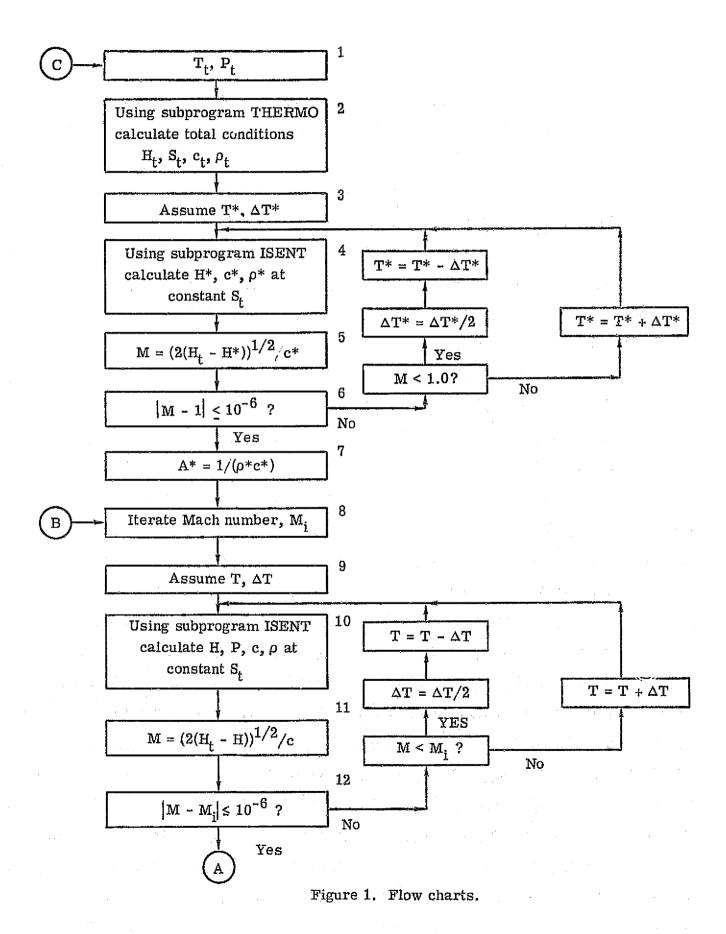
SV/SVT ratio of the sound velocity at static conditions to the sound

velocity at total conditions

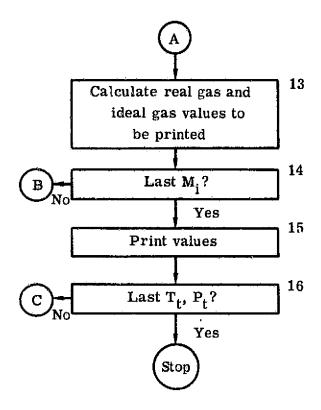
TT total temperature, K

T/TT ratio of the static temperature to the total temperature

Z compressibility factor, P/pRT



MAIN PROGRAM, continued



SUBPROGRAM ISENT

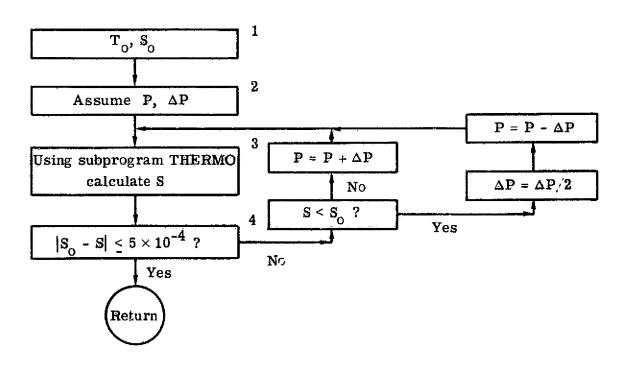


Figure 1. Concluded.

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"MARL" I. . POAL-GAS ISTATEOPIC FERPANSIONS OF PARAMYPROGEN

		A. TT	= 25.0	K PT =	1.0 ATM	₽H0* =	-104F-19	G/CH*	SVT = 40+	.139 M/SE			
MACH	PE/M	7	CENCA	SV/SVI	L'AL.L	7/17	RHOZRHOT	A*/A	SV/SVT	P/PT	17/11	PHO/PHOT	A*/A
sa jiri								100		PELATIVE 1	G IDEAL	GAS VALUES	
0.000	0.	9455	1.7767	1.0900	1.0000	1.0000	1.0000	0.0000	1.0000	1.0000	1.0000	1.0000	1.0000
# U F II	-1535+08	•9→56	1.7767	9996	9979	9992	9989	.0889	9998	.9997	9997	1.0000	1.0303
170	<u>. ₹895€±04</u>	9-56	1.7766	. 938*	9916	9966	9949	.1769	.9993	9986	9986	9999	1.0297
.150	.4557+04	9456	1.7765	• 996?	0813	.9925	9884	.2631	9984	. 9969	9969	1.0000	1.0266
.200	.6035+0P	•9+56	1.7764	. 9932	.9672	.9867	9802	.3467	.9972	.9945	9946	1.0000	1.0275
.250	·7485+08	.9456	1.7762	9895	9496	.979-	9696	. 4271	9956	9918	9916	1.0002	1.0262
*3P1	9805+98	• □56	1.7769	.9849	.9284	.9716	.9566	.5933	.9937	9882	.9881	1.0002	1.0242
350	.1032+09	. 9456	1.7759	.9795	-911-5	.9604	-9415	.5750	9916	. 9844	.9839	1.0005	1.0224
×400	•116E+09	.9456	1 . 7755	.9737	• 8 <i>777</i>	.9+89	.9251	.6415	9691	9800	9793	1.0009	1.8202
.450	.1295+09	.9455	1.7752	.967.0	.8468	.9362	-9057	.7026	9864	.9753	9741	1.0013	1.0176
0.00	-1415+09	.9455	1.7740	.9598	.81P1	.9224	.8869	.7579	.9835	. 9704	9685	1.0020	1.8155
. 550	.1521+119	.9455	1.7745	.9519	.7858	.9077	.8659	.8072	.9803	. 9652	.9626	1.0028	1.0130
	.163:+09	•9455	1.7741	• 94 3E	•7526	.8920	+8438	. 4507	.9769	.9600	. 9563	1.0040	1.0107
•650	·174E+89	9455	1.7777	.9347	.7188	·8757	.8210	. 8882	-9734	. 9548	94 97	1.0055	1.0987
•700	.1837+09	9455	1.7777	92 55	.6845	.8587	.7975	.9197	9698	9495	9428	1.0072	1.0065
.750	·1935+89	. 9455	1.772A	•915 ^p	.6584	.6411	.7733	9458	•9660	9445	9356	1.0094	1.0048
.800	•201E+09	9-55	1.7723	.9059	. 6163	.8232	-7487	• 9662	9621	9395	9285	1.0118	1.0032
•850	•209=+09	• 9456	1.7719	.8956	.5827	.8849	-7240	.9815	.9581	9346	9212	1.0146	1.0018
•900	•216:+09	9456	1.7714	. 8451	.5499	.7864	6993	.9920	9541	9301	9138	1.0179	1.0006
•95 n	.223:+09	•9456	1.7711	.8744	.5181	.767#	6748	.9981	.9501	9260	.9063	1.0217	1.0003
1.000	\$5.05+0.9	.9456	1.7705	.8636	4871	.7491	.6503	1.0000	9460	9271	. 6989	1.0258	1.0000
1.050	·2355+09	.9457	1.7702	. 5526	. +574	.7304	6762	9983	.9419	9187	8914	1.0306	1.0003
1.100	.240E+09	.9457	1.7599	.8415	·4288	.711 ^p	•6025	9931	9379	9157	.8840	1.0357	1.0010

SATURATION BOUNDARY REACHED.

A. (CONTINUED)

MACH	LOCAL ISENTROPIC	VISCOSITY	THERMAL CONDUCTIVITY	PRANDTL
	EXPANSION COEFF.	G/CM-SEC	CAL/CM-SEC-K	NUMBER
0.000	ī	.13738E-04	•45514E-04	.7561
•050	1.6967	.13726E-04	.48474E-04	.7561
.100	1.6554	.13693E-04	.48351E-04	.7562
-150	1.6768	.13637E-84	.48149E-04	.7563
-200	1.6724	.13560E-04	.47869E-04	.7564
.250	1.6856	.13462E-04	.47514E-04	.7565
.300	1.6656	.13344E-04	.47084E-04	.7567
.350	1.6804	.13207E-04	•46586E=04	.7570
.400	1.6716	.130525-04	.46021E-04	.7573
. 450	1.6729	.12601E-04	.45396E-74	.7576
.500	1.6721	.126945-04	.44716E-04	.7581
.550	1.6713	.12+93E-04	.43984E-04	.7585
.600	1.6730	.12279E-04	-43207E-04	.7591
.650	1.6748	.1205EE-04	.42390E-04	.7597
•700	1.6698	·118275-04	.41538E-94	.7604
.750	1.6743	.11577E-04	.40658E-04	.7611
800	1.6692	.11328E-04	.39753E-04	.7620
.850	1.6682	.11072E-04	.38829E-04	7629
.900	1.6687	.108125-04	.38075E-04	7602
951	1.6711	.10549E-04	.373905-04	.7558
1.000	1.6667	.10284E-04	.36711E-04	.7511
1.050	1.6692	.1001*E-04	.36841E-04	.7460
1.100	1.6665	.97519E-05	.35381E-04	.7496

SATURATION BOUNDARY REACHED.

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TABLE I. PTAL+GAS ISENTROPIC EXPANSIONS OF PARAHYCROGEN

		B. TT	= 30·n	K PT =	1.0 ATM	RH01 =	.847E-03	S/CH*	SVT = 447	.506 M/S	EC		
MACH	RE/M	7	CP/CV	SV/SVT	PZPT	1/11	RHOZRHOT	A+/A	SV/SVT	P/PT FELATIVE	T/TY	RHO/RHOT GAS VALUE	
												O-5 THEOL	•
0.000	0.	•966+	1.7347	1.0000	1.0000	1.0000	1.0000	0.0000	1.0000	1.0000	1.0000	1.0000	1.0000
.050 .100	.1175+PR	•9664	1.7347	. 9995	• 9979	.9992	9988	.4888	.9998	.9997	. 9997	1.0000	1.0300
•150	.233∑+08 .3485+08	.9654 .9554	1.7346	9983	9916	•9966	.9949	.1768	.9993	. 9986	. 9986	• 9999	1.0294
.200	.461E+08	9654	1.7345	- 9962	.9813	•9925	-9888	-2630	.984	• 9969	. 9970	1.0000	1.0285
.250	.572E+08	.9664		.9933	9672	•9867	-9802	• 3466	• 9972	• 9945	- 9946	1.0000	1.0273
.300	•680±+08		1.7345	9895	• 9496	•9794	• 96 96	• 4270	.9957	9918	• 9917	1.0002	1.0260
.350	.784E+08	9663	1.7343	9851	9284	.9706	• 9566	.5032	.9938	- 9882	- 9881	1.0002	1.0240
.400	.885E+08	9663	1.7342	.9798	9045	•9604	•9418	.5749	9917	- 9844	.9840	1.0006	1.0222
450	•951E+08	• 9663	1.7341	9738	. 2777	+9490	•9251	.6414	-9893	• 9880	9793	1.0009	1.8200
•500	•107E+89	9662	1.7339	.9672	.8488	•9363	9067	.7025	• 9866	• 9753	.9742	1.8013	1.0177
.550		•9562	1.7337	•9601	.8181	. 92 25	.8875	•7579	.9837	.97114	• 9686	1.0020	1.0154
e, ·	.116E+79	956?	1.7375	.9522	.7858	.9877	.8659	.8072	.9806	• 9652	. 9627	1.9029	1.0130
•600	-1245+09	9662	1.7333	• 9439	•7526	.8921	.8439	•6507	.9772	.9600	. 9563	1.0841	1.0108
.650	1325+09	. 9651	1.7331	. 9351	-7187	•8757	·8209.	.8882	.9738	• 95 47	. 94 97	1.0055	1.0086
.700 .750	1392+89	• 9661	1.7325	9256	• 6 B44	-8587	.797*	• 91 98	.9701	9493	.9429	1.0072	1.0066
	•146E+09	.9661	1.7325	• 9162	.E501	.8411	.7731	.9457	. 9664	. 9442	.9358	1.0093	1.0048
.800	-1535+09	.9661	1.7323	9963	•6161	• 62 32	·7487	- 9663	.9625	• 9391	• 9285	1.0117	1.0022
.85 C	.158E+09	.9651	1.7328	•8961	. 5825	.8048	.7240	. 9816	.958€	• 9342	.9211	1.0145	1.0019
.900	*164E+09	.9561	1.7316	8856	-5497	•7863	•6993	• 9922	.9546	9297	.9137	1.0178	1.0009
•95 1	•169E+n9	9661	1 - 7313	• B749	-5177	7676	.6747	. 9962	.9506	. 9254	. 9061	1.0215	1.0003
1.000	.173E+09	9661	1.7310	. 5641	. 48E7	.7488	•6501	1.0000	.9465	• 9213	.8986	1.0255	1.0000
1.050	.177E+89	9561	1.7306	.8531	4569	.7301	•6260	• 9982	.9425	.9177	.8911	1.0302	1.0003
1.100	+181E+89	• 9662	1.7303	-8420	.4284	.7114	•6023	• 9931	.9384	9146	.8836	1.0354	1.0010
1.150	*184E+09	.9662	1.7300	•8409	•+011	-6928	.5790	- 9849	. 9344	• 9119	.8761	1.0411	1.0021
1.200	•187£+09	. 9652	1.7296	• 81 9 8	,3751	•6745	.5563	.9742	.9303	• 90 97	. 8687	1.0474	1.0038
1.250	1900+09	•9663	1.7293	-8086	.3585	.6564	5341	•9610	.9264	.9079	.8515	1.0540	1.0059
1.300	1925+09	.9663	1.7290	• 7 975	. 3272	6385	-5125	.9458	.9225	.9065	.8543	1.0613	1.0085
1.350	•194E+89	9664	1.7287	.7864	.3052	6209	-4916	.9290	.9186	9058	.8473	1.0691	1.0117
1.400	•196E+89	• 9664	1.7284	.7754	.2846	-6037	.4714	.9109	.9148	9056	. 6404	1.0777	1.0156
1.450	·198E+09	.9565	1.7282	.7644	•26°2	-5868	.4519	.8916	.9111	9059	8336	1.0867	1.0199
1.500	•199E+09	9655	1.7279	•7535	.2+70	-5784	.4330	. 5713	9074	9067	.8270	1.0963	1.0248
1.550	.200E+09	•96 6 6	1.7278	.7425	.230t	•5543	.4149	.6503	9038	9081	.8206	1.1064	1.0302
1.670	.201E+09	• 9566	1.7276	•7322	•2140	.5386	. 3974	.8787	.9003	9098	.6143	1.1170	1.0360

SATURATION BOUNDARY REACHED.

P. (CONTINUED)

MACH	LOCAL ISENTROPIC	VISCOSITY	THERMAL CONDUCTIVITY	PRANDTL
	EXPANSION COEFF.	G/CM-SEC	CAL/CM-SEC+K	NUMBER
0.000		.16211E-04	.57156E-04	.7345
.050	1.6953	.16198E-04	.57109E-04	.7346
.100	1.6551	•16161E-04	•56969E=04	.7347
• 150	1.6765	.16098E-04	•56737E+0+	. 7348
.200	1.6720	.16012E-04	.56415E-04	.7350
. 250	1.6853	.15902E-04	.56007E-04	.7352
.300	1.6655	.15769E-04	•55515E-04	. 1354
. 350	1.6808	.15615E-04	.54945E-114	.7357
• 400	1.6720	.15440E-04	.54302E-04	.7360
• 450	1.6736	.15247E-04	.5359BE-N4	.7364
.500	1.6737	.15036E-0+	.52817E-04	.7367
.550	1.6725	.14809E-04	.51967E-04	.7371
• 500	1.6748	.14567E-B4	•51108E-04	.7374
•650	1.6730	•1431 TE-04	•50185E-0+	.7377
.700	1.6721	.14047E-04	•49213E-04	.7382
.750	1.6727	•13771E-04	•48201E-04	.7388
.000	1.6723	.13487E-04	.47160E+04	.7394
.850	1.6712	.131965-04	.46895E-04	.7401
• 900	1.6721	•12899ē-04	.45813E-N4	.7408
.950	1.6709	.12599E-84	.43917E-04	.7415
1.000	1.6678	.12295E-04	.42813E=04	.7422
1.050	1.6710	•11990E-04	.41705E-04	.7429
1.100	1.6701	•11584E-04	.40601E-04	.7436
1.150	1.6694	.11378E+04	.39501E-04	.7443
1.200	1.6704	.11074E-04	.38409E-04	.7451
1.250	1.6675	.10772E-04	.37519E-04	.7420
1.300	1.6672	.10472E-04	.36789E-04	.7357
1.350	1.6681	.10176E-04	.36079E-04	.7291
1.400	1.6700	.98642E-05	.35389E-04	.7222
1.450	1.6683	.95966E-05	.34719E-04	.7149
1.500	1.6679	.93142E-05	.34070E-04	.7073
1.550	1.6674	.90370E-05	.33441E-84	.6994
1.600	1.6654	.87655E-05	.32632E-04	.6913

SATURATION BOUNDARY REACHED.

ORIGINAL PAGE IS OF POOR QUALITY

TARLE I. PEAL-GAT ISENTROPIC EXPANSIONS OF PARAHYDROGEN

		c. Tr	= 40.0	K F* =	1.0 ATM	२ Н0Т =	.624£-93	G/CM3	SVT = 521	.238 M/S	EC		
MACH	RE/M	2	CPZCV	SV/SVT	P/PT	T/TT	RHOZRHOT	A*/A	SV/SVT	P/PT	7/11	RHO/RHOT	A*/A
				14. The second of the second o						RELATIVE	TO IDEAL	GAS VALUES	
0.000	0.	.9845	1.6993	1.0007	1.0000	1.0000	1.0000	0.0900	1.0000			4 6000	
.050	-781E+07	9845	1.6993	9996	9979	•9992	•9988	.0888	.9998	1.0000	1.0000	1.0000	1.9900
.100	.156E+0A	9845	1.6993	.9983	9916	9967	9949	.1767	9993	9986	9987	1.0000	1.0295
.150	.232E+04	9845	1.6993	9962	.9813	9925	9885	.2629	9985	9969	9970	•9999 •9999	1.0288 1.0280
: • 2# ft	80+280°.	.9945	1.6993	.993*	9674	986R	9804	3465	.9973	.9948	.9947	1.0002	1.0270
.250	.3825+08	9845	1.6994	.9896	9496	9795	9696	4268	9958	9918	9917	1.0002	1.0254
.300	.454E+08	.9844	1.6994	.9852	9286	9707	9567	.5031	9940	9885	9882	1.0004	1.0238
.350	.523E+08	. 9844	1.6994	.9900	.9045	.9606	9+17	.5747	9919	.9844	.9841	1.0005	1.9217
.400	•590 <u>5</u> +08	4944	1.6994	. 9741	8779	9491	9251	6413	9895	.9802	.9795	1.0009	1.0197
. 450	.653E+88	.9847	1.6993	9675	8489	9365	9067	.7023	.9869	.9755	.9744	1.0013	
.500	.7145+08	.9843	1.6903	.9603	.8182	9227	8869	.7577	.9840	9705	9689	1.0020	1.0175
.550	·7715+08	. 9842	1.6993	.9525	.7861	9080	.8660	.8072	9809	9655	9629	1.0020	
.600	.825F+08	.9842	1.6992	.9443	7526	6924	8437	-6505	.9777	9601	9567	1.0039	1.0130
650	. P76E+08	9841	1.6991	9355	.7197	.876	8277	8879	9742	9547	.9501		1.0105
.700	.9235+08	.9841	1.6990	9263	€845	8591	7972	9197	.9706	9495		1.0053	1.0084
.750	•967E+08	.9949	1.6989	9167	.6501	-8415	7730	9455	.9669	9442	•9432 •9362	1.0071 1.0090	1.0865 1.0045
.800	.101E+09	9840	1.6988	9068	.6161	8236	.74 A5	9661	9631	9391	9290	1.0115	1.0038
. 85 በ	•174E+R9	.984n	1.6987	8966	5825	.8753	7278	9815	9592	9342	9216	1.0113	1.0038
.900	.1985+09	.9839	1.5985	6862	£497	.7867	6991	9921	9553	9297	9142	1.0176	
.950	·111E+89	-9839	1.6984	8755	.5177	.7680	•6745	9981	•9513	9254	9067	1.0213	1.0009 1.0003
1.000	.114E+09	9838	1.6982	.8647	.4867	.7493	.6590	1.0000	9472	•9213	8991		
1.050	-116E+89	9838	1.6981	.8537	- 569	.7305	6259	9983	9432	•9213		1.0254	1.0000
1.100	.118E+R9	9838	1.6979	8427	4272	7119	.6020	9329	9391		8916	1.0301	1.0003
1.150	.120:+09	9838	1.6978	8316	-01B	.6933	•5739	9849		9143	-8841	1.0350	1.0008
1.200	·122E+09	9838	1.6976	.8204	3750	6749	.5561	• 9741	.9351 .9311	.9118	.8767	1.0408	1.0021
1.250	.1235+09	9839	1.6974	8093	• 3504	.6568	•5339	9609		9094	. 8693	1.0470	1.0037
1.300	.125E+R9	g g T g	1.6972	7982	3271	•6₹89	•5123	9458	9272	9176	.6620	1.0536	1.0056
1.390	1265+09	9434	1.6971	7871	3051	6214	4914	9290	.9232	9062	. 8549	1.0609	1.0065
1.400	1275+09	9838	1.6969	.7760	2844	6041			9194	-9054	.8478	1.0687	1.0117
1.450	1275+09	.9838	1.5967	.7651	.2650	5872	4717	.9107	9156	.9051	.8409	1.0771	1.0154
1.500	.128E+09	9838	1.6965	7547	• 24c6	.5787	•4516 •4328	-8914	9119	9053	.8342	1.0661	1.0197
1.550	.1295+09	9873	1.6964	7435	• 2398	.5546		.8711	9082	9061	8275	1.0957	1.0246
1.600	·129E+09	9839	1.6962	.7328	2139	•5389	•4147 7072	8511	.904€	.9073	.8211	1.1059	1.0300
1.650	1295+09	9839	1.6960	7223	.1998	.5236	.3972	•8285	9011	9090	-8148	1.1165	1.0359
1.700	.1295+09	9839	1.6959	7119			-380+	8067	.8977	.9114	- 80 86	1.1278	1.0424
1.750	.129E+09	9839	1.6957	7917	.1852 .1723	•5087	3644	-7846	-8943	9142	.8027	1.1397	1.0495
1.000	1295+09	.9879	1.6955	6916		.4942	3497	.7624	.6911	9175	• 7969	1.1522	1.0571
1.850	1295+09	9840	1.6954	•6917	.1603	4801	•3342	•7492	.8879	. 9213	•7912	1.1651	1.0651
1.900	1295+09	• 9849	1.6952	•6720	.1492	.466F	.3201	•7183	.8848	.9258	.7857	1.1790	1.0740
1.950	+1295+09	.98+1	1.6951	• 6 2 U	•1389 • 1303	4532	•3065	•6964	.8818	• 93 05	-7804	1.1929	1.0531
2.000	1295+09	9841	1.6950		.1293	4484	•2937	•6750	.8789	.9360	.7753	1.2079	1.0931
r white	■ 16 75 ¥ U 7	+7741	T・ロココリ	.6531	.1203	.42,79	-2813	6537	8760	.9416	-7713	1.2230	1.1031

C. (CONTINUED)

MACH	LCCAL ISENTPOPIC	VISCOSITY	THEPMAL CONDUCTIVITY	PRANOTE
	EXPANSION COFFF.	G/CM-SEC	CAL/CM-SEC-K	NUMBER
0.000	I	.20797E-84	.73845E-04	.7120
.050	1.6929	.20782E-04	.73788E-84	.7121
100	1.6516	.20737E-04	.73615E-04	.7122
.150	1.6734	.20663E-04	.73329E-84	.7124
.280	1.6886	.20560E-04	.72933E-04	.7126
.250	1.6671	.20429E+04	.72430E-04	.7129
. 300	1.6762	.20271E-84	.71826E-04	.7133
.350	1.6568	.20087E-04	.71126E-04	.7137
.400	1.6752	.19879E-04	.70336E-94	.7141
. 450	1.6717	.19647E-04	.69463E-04	.7146
•500	1.6721	.19395E-04	.68514E-74	.7151
•550	1.6757	.19123E-84	.67497E-04	.7156
.600	1.6661	.18834E+84	.66419E-04	.7161
-650	1.6722	.18528E-84	.65289E-04	.7166
.700	1.6753	.182095-04	•64114E-04	.7170
.750	1.6687	.17877E-04	.62902E-74	.7174
.800	1.6720	.17534E-04	•61659E-04	.7178
.850	1.6720	.17183E-04	.60392E-04	.7180
900	1.6722	·16824E-04	.59039E-04	.7191
. 950	1.6713	.16468E-84	•57671E-04	.7201
1.000	1.6690	.16091E-04	.56296E-04	.7210
1.050	1.6717	.1571 SE-04	•54921E-04	.7219
1.100	1.6664	.15346E-04	.53548E-04	.7227
1.150	1.6735	-14973E+8+	.52184E+04	.7235
1.200	1.6690	.1460RE-04	.50631E-04	.7241
1.250	1.668B	.14229E-114	.49495E-04	.7247
1.300	1.6687	.13860E-04	.48137E-04	.7257
1.350	1.5694	-134955-84	.46787E+04	.7269
1.400	1.6686	.13134E-04	.45458E-04	.7280
1.450	1.6695	.1277 EE-84	.44154E-04	.7290
1.500	1.6693	.12427E-84	•42876E-04	.7300
1.550	1.6685	.12081E-04	.41625E-04	.7310
1.600	1.5668	.11742E-84	.40403E-74	.7316
1.650	1.6690	.11489E-84	.39211E-94	.7326
1.700	1.6666	.11083E-04	.38051E-04	.7333
1.750	1.6579	.10765E-94	.37079E-04	.7306
1.800	1.6665	•10453E-04	.36367E-04	.7234
1 . 55%	1.6706	-10149E-04	.356805-04	.7158
1.900	1.6647	.98517E-85	.35017E-94	.7080
1.950	1.6705	•95623E-05	.34377E-04	•6999
2.080	1.6642	-92804E-05	.33760E-04	•6916
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TABLE I. REAL-GAS ISENTROPIC EXPANSIONS OF PARAHYCPOGEN

		D. TT	= 60.0 K	PT =	1.8 ATM	PHOT =	.4115-83	G/CM3	SVT = 635.	.721 M/SE	C	. •	
MACH	8E/H	7	CPZCV	SV/SVT	P/PT	T/TT	RHOZRHOT	A*/A	SV/SVT	P/PT	T/TT	RHO/RHOT	A*/A
										ELATIVE	TO IDEAL	GAS VALUES	
0.000	0.	. 9954	1.6482	1.0000	1.0000	1.0000	1.0000	0.0000	1 0000	4 0000			
•050	.453E+07	.9954	1.6484	• 9996	9979	9992	•9987	.0682	1.0000	1.0000	1.0000	1.0000	1.0900
+100	•903E+07	.9954	1.6488	9986	9918	9968	9950	•1755	9999	• 9997	- 9997	1.0000	1.0221
•150	.135E+B8	9954	1.6495	9968	9818	9929	9889	and the second second	9996	.9988	• 9988	1.0000	1.0218
.200	.178E+0A	.9954	1.6505	9943	9679	9874	• 9894	•7612 •3444	• 9998	.9974	. 9973	1.0001	1.0214
.250	.221E+08	.9954	1.6518	9911	9503	9804	9594		.9983	•9953	. 9953	1.0001	1.0206
-300	-2632+08	. 9953	1.6533	9373	9296	9719	9565	4243	.9973	• 9926	9926	1.0000	1.0195
-350	.303E+08	9953	1.655 0	9827	9058	9621		.5005	9961	. 9895	- 98 94	1.0002	1.0185
.400	+341E+08	.9953	1.6568	9775	.8793	9517	•9416	.5721	•9947	.9859	-9857	1.0003	1.0172
.450	.378E+08	9952	1.6586	9717	.8505	9387	.9748	6388	.9931	.9818	.9814	1.0006	1.0157
.500	.412E+08	9952	1.6606	9652	and the second of the second o	5.50.0	.9863	.7000	•9912	•9773	. 9767	1.0009	1.0141
.550	445E+08	9951	1.6625	9581	8199	•9252	+6864	• 7556	•9890	.9726	.9715	1.0014	1.0125
.600	476E+08	9951	1.6644		7878	•9107	•8653	+6055	.9867	. 9676	.9658	1.0022	1.0108
650	.5045+08	9951	1.6562	9505	.7543	-895₹	•842B	.8491	-9841	• 9622	. 9598	1.0028	1.0089
.700	-531E+08	9950	1.5686	9+23	.7704	.8791	8198	.8870	-9813	• 9569	. 9534	1.0041	1.0073
•750	•555E+08	9949	1.6696	- 9337	6860	8622	.7960	9190	.9784	- 9515	.9467	1.0056	1.0057
.800	-5775+08	9949		.9246	.6515	.8448	•7716	-9451	•9752	• 9461	9398	1.8072	1.0041
.650	•597E+08	9945	1.6710	.9150	.6172	.8268	•7469	•9658	-9716	•9408	9326	1.0093	1.0027
.900	•615E+D8		1.6723	. 9051	-5834	.8785	.7278	.9812	.9683	. 9356	. 9253	1.0117	1.0015
•950		9945	1.6735	.8950	• 5503	•7899	6971	9918	•9647	.9307	•9179	1.0146	1.0006
1.000	•631E+08	9947	1.6744	8945	•5182 J	.7712	.6724	•9980	.9610	• 9262	.9104	1.0181	1.0002
	.6465+08	. 9947	1.6753		•4871	.7524	-6479	1.0000	.9572	.9220	9928	1.0220	1.0000
1.050	.6585+08	• 9946	1.6759	•8629	•4570	.7335	·6276	9980	.9533	.9180	. 6953	1.0262	1.0001
1.100	.669E+08	9946	1.6765	-8519	. 4284	.7148	-5998	9929	.9494	9146	8876	1.0311	
1.150	.679E+05	• 9945	1.6769	.840A	010	•6961	•5766	9848	•9455	9118	- 5503		1.0008
1.200	.687E+08	9945	1.6772	.6296	.3749	.6777	.5537	-9738	-9416	-9091	.8729	1.0367	1.0020
1.250	.694E+08	.9945	1.6775	. 6184	• 3502	-6595	-5316	.9697	9376	.9972	•8656	1.0425	1.0034
1.300	•699E+08	.9944	1.6776	.8072	.3269	-6415	.5190	9455	9336	9057		1.0492	1.0057
1.350	.703E+08	9944	1.6777	.7961	.3049	.6239	-4892	9288	•9299	9049	. 6564	1.0562	1.0062
1.400	.707E+08	.9944	1.6775	7849	2842	.6966	.4691	.9105	.9261	9045	-8513	1.0640	1.0114
1.450	.709E+08	9944	1.6779	.7739	.2648	-5896	4495	8910	9224		. 8444	1.0723	1.0152
1.500	•71 0E+0 A	.9943	1.6778	7529	*2466	.5771	4377	6797	.9187	9045	.6376	1.0810	1.0193
1.550	•711E+00	9943	1.6778	.7521	.2295	-5569	4127	· 8497	•9151	9052	.8310	1.0905	1.0241
1.600	•711E+08	.9943	1.6778	.7413	-2136	-5411	3953	.6282		.9064	. 8245	1.1006	1-0295
1.650	.711E+08	.9943	1.6777	.7307	1986	.5258	3786	•8063	.9115	9881	-8182	1.1112	1.0354
1.700	.7105+08	.9943	1.6777	.7202	.1850	•510A	•3626		.9051	9104	.6120	1.1224	1.0419
1.750	.708E+08	9943	1.6776	7099	1771	.4963	3472	7842	.9847	.9131	.6061	1.1342	1.0490
1.800	.706E+0A	9943	1.6776	6997	.1602	·4822		.7629	-9014	. 9164	.8002	1.1465	1.0565
1.850	•703E+08	9942	1.6775	.6897	•1•90		3326	.7399	-8982	• 9203	.7946	1.1595	1.0647
1.900	.700E+08	9942	1.6774	.6798	•1387	.4685 .4552	3145	-7178	•6951	.9245	.7891	1.1730	1.0733
1.950	.697E+08	9942	1.6774	•6701	•1367 •1291		.3050	-6960	•8921	• 9293	.7838	1.1870	1.0824
2.000	.694E+08	9942	1.6773	.6606	.1202	.4423	.2922	6745	.8891	. 9347	.7787	1.2018	1.0923
t			· · · · · · · · · · · · · · · · · · ·	10000	● T ⊆ U ≤	·4298	•2810	.6534	.8862	. 9404	.7737	1.2170	1.1025

D. (CONTINUED)

MACH	LCCAL ISENTROPIC	VISCOSITY	THERMAL CONDUCTIVITY	PRANDTL
	EXPANSION COEFF.	G/CH-SEC	CAL/CM-SEC-K	NUMBER
0.000	T	.28543E-04	•10769E-13	.6847
.050	1.6379	-288255-04	.10788E-03	.6847
.100	1.6428	.28771E-04	.10754E-03	-6847
.150	1.6487	-28681E-04	•10711E-03	-6849
.200	1.6491	-28556E-84	*10651E-03	.6850
.250	1.6379	-28397E-84	.10575E-03	.6853
.300	1.6473	.28204E-04	.10464E-83	.6856
.350	1.6465	.27978E-84	.10377E-03	.6860
.400	1.6477	.27722E-04	.10256E-03	-6866
· 450	1.6485	.27436E-84	.10121E-03	.6873
.500	1.6526	.27122E-84	.99442E-114	6982
•550	1.6564	.26783E-04	.97976E-04	-6905
•601	1.6507	.26420£-04	.96417E-84	.6909
. 650	1.6610	.26035E-84	•94776E-04	-6914
.700	1.6597	.25630E-04	.93068E-04	.6928
.750	1.6591	.252B8E-64	.91302E-04	.6927
.800	1.6611	.24771E-04	.89486E-04	.6935
.85D	1.6624	.24322E-04	.87638E-04	.6944
• 900	1.6638	.23862E-04	.05762E-04	.6954
•95n	1.6676	.23393E-84	.83843E-84	-6966
1.000	1.6659	.22918E-04	.81912E-04	.6960
1.050	1.6540	.22438E-04	.79895E-04	.7001
1.100	1.6679	•21955E-04	.77991E~04	.7013
1.150	1.6699	•21471E-04	.76100E-04	.7026
1.200	1.6652	.20986E-04	.74227E-04	.7037
1.250	1.6699	.20503E-04	.72378E-84	.7049
1.300	1.6665	.20422E-04	.70556E-04	.7859
1.350	1.6702	•19544E-04	•68758E+04	.7969
1.400	1.6688	.19071E-04	.66992E-04	.7879
1.450	1.6657	•18603E-84	.65263E-04	.7087
1.500	1.6693	·16140E-04	•63571E-04	.7093
1.550	1.6680	•17684E-84	•61920E+04	.7099
1.600	1.6682	•17235E-84	•60309E-04	.7183
1.650	1.6586	.16793E-84	•58664E-04	.7114
1.700	1.6679	•16359E-04	•57035E-04	.7128
1.750	1.6672	•15933E-04	•55451E+84	.7148
1.800	1.6689	•15516E-84	.53911E-84	.7151
1.850	1.6665	.15107E-04	•52416E-04	.7160
1.900	1.6667	.14707E-04	.50966E-04	.7169
1.950	1.6692	•14315E-04	•4956 1 E=04	.7175
2.000	1.6670	-13933E-04	.48166E-04	.7185

OF POOR QUALITY

NO SEE OF REAL PROPERTY.

TABLE I. REAL-GAS ISENTROPIC EXPANSIONS OF PARAHYDROGEN

E. TT = 80.0 K PT = 1.0 ATM PHOT = .306E-03 G/CH3 SVT = 713.635 N/SEC

			- 0040 1	F1 =	T40 MIN	PHU1 =	*3005-83	G/CM3	SVY = 713	.635 M/SI	EC		
MACH	PE/M	2	CP-/CV	SV/SVT	PZPT	1111	RHOZRHOT	- AT/A	SV/SVT	P/PT PELATIVE	T/TT	RHO/RHOT	
0.000	0.	.9986	4 6, 60	4 0000			1 3223						
.058	•306E+07		1,5489	1.9000	1.0000	1.0000	1.0000	0.000	1.0000	1.0000	1.0000	1.0000	1,0000
.100	.610E+87	9985	1.5492	9998	• 9961	•9993	9988	.9867	1.0008	- 9998	. 9998	1.0000	1.0849
•150	•910E+07	•9955 •9955	1.5501	•9990	. 9923	.9973	•9950	•1726	1.0000	• 9993	• 9993.	1.0090	1-8649
.200	.1215+0#	9985	1.5516	.9978	.9826	.9910	•9889	-7570	1.0000	. 9984	. 9984	1.0000	1.0050
250	-149E+08	9985	1.5536	9961	• 9696	•9892	-9803	.3391	1.0000	. 9971	. 9971	1.0000	1.0049
300	•177E+98	9985	1.5562	.9938	•9530	.9831	• 96 95	4183	1.0008	•9954	. 9954	1.0000	1.0849
.350	*204E+08	9985	1.5593	.9910	.9331	.9758	.9564	.4936	•9999	•9933	• 9933	1.0000	1.0046
	2305*08	A CONTRACTOR OF THE CONTRACTOR	1.5639	.9878	•9103	•9672	•9413	•5651	•9998	.9908	. 9909	1.0000	1.0040
-450		9984	1.567?	9840	.6847	•957*	.9242	.6317	.9997	.9878	. 9880	1.0000	1.0045
•500	.255E+08	.9954	1.5718	9798	• 8569	• 9463	•9056	6934	•9994	• 9846	- 9846	1.0001	1.0044
	•278F+08	.9984	1.5769	.9750	.8268	.9342	.8853	.7494	.9991	.9808	-9809	1.0001	1.0041
.550	.300E+08	.9983	1.5924	9697	.7952	-9210	.8637	.7999	•9986	+9767	.9767	1.0003	1.0038
-600	•327E+U8	.9983	1.5882	• 96 • 0	.7623	.9568	. 8419	. 6445	.9981	, 9723	. 9720	1.0005	1.0035
.650	*379E+08	.9982	1.5942	. 9577	.7252	.8916	-6170	.8831	~9973	-9673	-9670	1.0007	1.0029
.700	.3572+08	.9982	1.6004	. 9508	• 6 9 3 8	.8756	·7925	.9161	.9964	.9624	9614	1.0013	1.0026
.750	•373E+08	9982	1.6067	• 9435	·65P9	.8589	.767+	. 9430	•9952	.9569	. 9555	1.0018	1.0019
.800	•367E+nc	.9951	1: 6131	· • 935 *	-6741	8415	.7420	. 9645	.9938	.9514	9492	1.0027	1.0014
850	4015+08	9981	1.6193	• 9275	5697	.823E	.7164	.9807	9922	9458	9426	1.0039	1.0009
•900	.412E+08	. 99A9	1.6253	•9187	- 5559	.8052	•6907	9917	.9904	9402	9357	1.0053	1.0005
•95 D	.422E+08	•9980	1.6711	• 90 96	•5228	.7865	.5651	9980	.9883	.9345	9285	1.0070	1.0801
1.000	-431E+08	.9979	1.6366	•9000	• 4 90 8	.7676	-6398	1.0000	•9859	9291	9711	1.0093	1.0000
1.050	+439E+08	•9979	1.6417	.8901	.4601	.7485	-6151	9982	9834	9241	.9136	1.0122	1.0002
1.100	•446E+118	.9979	1.6463	.8799	.4386	.729=	.5907	.9927	.9806	-9193	9060	1.0154	1.0006
1.150	.451E+08	.9978	1.6505	.8694	•4025	.7104	.5670	9843	.9776	9151	- 8983	1.0194	1.8015
1.200	.4565+08	9978	1.6541	.8587	.3758	-6915	-5438	9730	.9745	9112	.8907		
1.250	.459E+88	9978	1.6574	.8+78	.3505	-6728	-5213	9594	.9713	9079		1.0238	1.0027
1.300	.462E+08	.9977	1.6601	.8368	•3768	6544	4997	9440	.9679	.9053	. 6831	1.0289	1.0043
1.350	.464E+08	9377	1.6625	.8257	.3044	-6363	-4788	9267	9645		8756	1.0349	1.0066
1.400	.465E+88	. 9977	1.6645	. 8145	2534	.6185	4587	9082	.9610	9032	.8682	1.0413	1.0092
1.450	.466E+08	.9976	1.6661	.0033	.2638	-6011	4392	8885	9575	-9019	.8609	1.0486	1.0126
1.500	•466E+08	.9976	1.6674	.7922	.2455	-5841	4207	. 3689	9539	-9011	-8539	1.0563	1.0164
1.550	.466E+D8	.9976	1.6685	.7811	.2283	5675	4827	.8467		.9011	. 8469	1.0650	1.0209
1.600	.465E+08	9975	1.6693	.7701	.2124	5514	.3856	.8251	-9504	• 9 015	- 84 02	1.0741	1.0258
1.650	.463E+08	.9975	1.6700	.7591	.1976	5356	-3692	and the second s	•9469	• 90 28	.8336	1.0840	1.0315
1.700	.462E+08	.9975	1.6705	.7483	1837	•520₹	• \$535	.8031	-9434	-9846	.8273	1.0946	1.0378
1.750	.460F+08	9975	1.6709	.7376	.1709	5055	• -	.7889	.9400	-9070	.8211	1.1057	1.0445
1.600	.458E+08	.9975	1.6711	:7271	•1590	•4911	.3384 .3241	.7587	9367	• 90 99	.8151	1.1175	1.0519
1.850	.455E+06	9974	1.6713	7167	1479	4771		7365	.9334	- 91 34	.6093	1.1298	1.0598
1.900	.452E+08	9974	1.6715	.7065	1376		-3103	.7145	•9302	•9175	.8037	1.1429	1.0683
1.950	4505+08	9974	1.6716	• 6964		•4636	-2973	6929	•9271	. 9223	. 7983	1.1567	1.0776
2.000	.446E+08	9974	1.6716		.1281	4504	•2847	.6714	• 9240	.9274	.7930	1.1708	1.0872
~ 4 0 0 0	4 44 OF 1 R G		T 0 T 0	.6865	•1192	4377	•2727	.6503	•9211	• 9331	.7879	1.1856	1.0974

E. (CONTINUED)

14 B #11 1	1 0011 705170070		THERMAL CONDUCTIVITY	PRANDTL
MACH	LOCAL ISENTROPIC	VISCOSITY		
	EXPANSION DOEFF.	G/CM-SEC	CAL/CH-SEC-K	NUMBER
9.000	1	.75851E-04	.14507E+03	.6952
.050	1.5471	.*5832E-84	.14495E-03	•6952
.100	1.5517	.35778E-04	.14457E-03	•6953
. 150	1.5493	.35687E-04	.143955-03	.6953
.200	1.5486	.35560E-04	.14308E-73	.6953
250	1.5536	.35398E-04	.14197E-03	•6955
.300	1.5539	.35200E-#4	•14063E-03	•6956
• 350	1.5592	•34967E-04	.13922E-03	.6951
.400	1+5597	.34701E-84	•13776E-43	.6938
-450	1.5697	•34400E-04	•13612E-03	• 6924
500	1.5700	.34068E-84	.13431E-03	.6910
•550	1.5782	.33704E-04	.13234E-03	•6896
.600	1.5830	.33310E-04	.13022E-03	.6883
•650	1.5857	.32888E-04	•12796E-03	.6879
.700	1.5987	.32439E-84	.12558E-03	.6869
. 750	1.5987	.31965E -0 4	.12308E-03	.6851
.800	1.6072	•31469E+04	*12049E-03	.6845
.850	1.6141	+30952E-84	.11766E-03	.6839
•900	1.6200	.30419E-04	•11522E+03	.6834
. 951	1.6228	.29878E-84	.11253E-03	.6831
1.000	1.6386	• 29309£- 0 4	.10988E-03	.6833
1.050	1.6374	.28739E-04	.10705E-03	.6838
1.100	1.6389	.28162E+84	.10430E+03	.6847
1.150	1.6468	.27589E-04	.10155E+03	.6868
1.200	1.6471	.26996E-84	.98690E-04	.6885
1.250	1.6538	• 26412E-04	.96182E-04	.6891
1.300	1.6570	•25629E-84	.93709E-D4	.6899
1.359	1.6561	•?525AE-04	•91278E-04	. 6998
1.400	1.6614	.24676E-04	.88895E-04	.6919
1.450	1.6601	•24107E- 0 4	•86562E-04	.6931
1.500	1.6647	-23544E-04	.04273E-04	.6944
1.550	1.6613	•22990E- 0 4	.82023E+04	•6960
1.600	1.6664	.22443E-84	.79792E-04	.6978
1.650	1.6665	.21906E- 0 4	.77677E-04	•6992
1.700	1.6651	•21377E+84	.75622E-04	.7005
1.750	1.6656	.20858E-04	•73625E+04	.7016
1.699	1.6663	.20348E+84	.71666E-04	.7029
1.850	1.6670	.19849E-84	.69804E-04	.7040
1.900	1.6697	•19360E - 04	.6797CE-04	.7050
1.950	1.6660	.18880E-04	. 66191E-D4	.7060
2.000	1.6672	•16411E-D4	• 6446 9E-114	.7067

ORIGINAL PAGE IS OF POOR QUALITY ORIGINAL PAGE IS

TABLE I. REAL-GAS ISENTROPIC EXPANSIONS OF PARAHYDROGEN

		F. IT	= 100.0	K PT =	1.0 ATM	PH01 =	.246E-03	G/CM3	SVT = 772	.508 M/S	EC		
MACH	REZM	7	CP/CV	SV/SVT	P/P T	T/TT	RHO/RHOT	A*/A	SV/SVT	P/PT	1/11	RHO/RHOT	A+/A
	, , , , ,			7 7 7 7 7				.*		PELATIVE	TO IDEAL	GAS VALUES	
0.000	0.	. 9997	1.4478	1.0000	1.0000	1.0000	1.8000	0.0000	1.0000	1.0000	1.0000	1.0000	1.0000
.050	.2255+07	. 9997	1.4480	. 9999	.9982	. 9994	9987	. 11857	1.0000	. 9999	. 9999	1.0000	.9931
.100	.44BE+87	. 9997	1 -4487	.9992	.9928	.9978	•9950	.1706	1.0002	. 9998	•9998	1.0900	.9933
.150	.669E+07	. 9997	1.4489	.9982	.9838	.9950	.9888	.2540	1.0004	• 9994	. 9995	.9999	. 9934
.200	.886E+97	9997	1.4515	. 9969	.9716	.9911	.9813	.3354	1.0008	. 9991	. 9990	1.9000	.9939
.250	+1105+08	.9997	1.4536	• 9958	.9560	.9861	•9694	.4138	1.0812	. 9984	• 9985	1.0000	.9943
.300	.130E+DA	.9997	1.4562	.9928	.9372	9801	+9563	.4587	1.0017	• 9975	. 9977	•9999	.9946
•35 n	.159F+08	9997	1.4593	. 9992	.9157	.9731	9412	.5598	1.0023	. 9966	•°968	•9999	.9953
.400	1695+88	.9996	1.4629	9573	.8915	.9648	.9241	.6262	1.0029	• 9954	.9957	. 9998	.9958
450	·1865+08	, 9996	1.4671	.9839	· 86+9	• 9556	.9052	-6878	1.0037	. 9939	. 9943	•9996	. 9963
500	.2035+08	.9996	1.4717	9802	.8364	.9455	+8847	.7441	1.0044	. 9921	, 9927	.9995	.9970
550	.219E+08	9996	1.4769	9761	.8060	.934*	-8528	.7948	1.0052	.9899	. 9906	. 9992	.9975
600	.234E+98	9995	1.4827	9716	.7741	.9222	.8396	. 6399	1.0060	. 9874	. 9886	.9989	-9980
650	.247E+08	9995	1.4891	9668	.7412	.9893	.8153	. 8792	1.0068	. 9845	. 9561	.9986	.9985
.700	. 26 0E+0 8	9995	1.4960	9616	.7975	.8954	.7903	.9129	1.0076	.9813	.9831	.9984	.9991
.750	.2715+08	9994	1.5034	.9560	.6731	.8807	.7644	-9406	1.0084	. 9775	. 9798	.9979	.9993
800	.281E+08	9994	1.5114	.9511	.6385	.8653	.7382	.9628	1.0091	.9733	. 9760	9975	.9996
850	.290E+08	9994	1,5198	.9438	.60-0	.8491	.7116	.9795	1.0097	. 9687	.9718	9971	.9998
980	.297E+08	.9993	1.5288	.9371	.5698	.8323	.6849	.9912	1.0101	. 9637	.9671	. 9969	1.0000
950	.304E+08	.9993	1.5381	.9300	.5361	.8149	.65 82	.9979	1.0105	. 9583	.9620	.9966	1.0000
1.000	.310E+08	9993	1.5477	9226	.5032	7970	.6716	1.0000	1.0106	. 9525	. 9564	.9964	1.0000
1.050	*15E+98	9992	1.5575	9148	.4712	.7786	6055	.9979	1.0106	9464	.9503	.9964	1.8000
1.100	.319E+08	9992	1.5674	9066	.4404	.7600	.5799	.9923	1.0103	. 94 94	. 9439	.9969	1.0002
1.150	.3225+08	9992	1.5773	.6950	.4108	.7410	.5547	.9831	1.0008	.9341	. 9370		1.0002
1.200	.324E+08	9991	1.5670	. 8891	.3827	.7220	.5304	.9711	1.0090	.9281		.9986	1.0006
1.250	.3262+08	9991	1.5964	.8798	.3560	.7029	.5768	.9564	1.0079	.9221	.9225	1.0002	1.0011
1.300	.327E+08	9991	1.6054	.6702	.3308	.6836	4841	.9397	1.0066	9165		1.0024	1.0020
1.350	.3275+08	9990	1.6136	.8603	.3071	6649	.4622	,9212	1.8049	.9114		1.0053	1.0032
1.480	.327E+08	9990	1.6716	8501	.2850	.6462	.4413	.9013	1.0030	.9068	. 8995	1.0986	1.0049
1.450	*327E+N8	.999n	1.6288	.8393	.2643	.6278	4213	.8804	1.0019	.9839	.8918	1.0133	1.0072
1.500	.3262+08	9990	1.6352	8292	.2451	.6096	4023	. 85 66	.9985	.8998	.8842	1,0184	1.0099
1.550	*325E+08	9949	1.6408	6186	.2273	5922	.3841	.8363	.9960	.8974		1.0244	1.0133
1.600	-324E+08	9989	1.6458	.8078	2108	.5750	3669	.8138	.9933	8960		1.0315	1.0175
1.650	•322F+00	9989	1.6501	.7970	1955	.5567	₹505	.7910		8953	 *** *********************************	1.0391	1.0221
			1.6537	786?	.1814	5421	3349	.7662	.9876	8954		1.0477	1.0275
1.700	7295+08	.9989	1.6568	7754	.1684	.5263	3202	.7456	9846	8964		1.0572	1.0337
1.750	.31 RE+08	.9989	1.6594	.7647	.1563	.5111	3061	.7231	.9816	8982			1.0405
1.800	•31 6E+88	.9988		111111111111111111111111111111111111111	•1452	.4963	2926	.7010	.9786	.9009		1.0785	1.8481
1.850	.314E+08	.9988	1.6615	•7540 *i.75	1349	.4821	280?	6791	9756	.9841		1.0902	1.0562
1.900	.311E+08	.9988	1.6632	.7435	.12F4	.4683	.2691	.6577	9726	9082			1.0651
1.950	.309E+08	.9988	1.6646	.7330					,9697	+9128		1.1157	1.0744
5.000	.306E+08	.9985	1.6657	.7227	.1167	•4549	. 2567	-6367	" TO TY	4.24.60	* 07.00	101121	7.01.44

F. (CONTINUED)

0.000	MACH	LCCAL ISENTROPIC EXPANSION COEFF.	VISCOSITY G/CM-SEC	THERMAL CONDUCTIVITY GAL/CH-SEC-K	PRANDTL NUMBER
100					
100 1.4516 .42092E-B4 .1910E-03 .7063 150 1.4412 .4208E-04 .1903E-03 .7063 150 1.4412 .4208E-04 .1894E-03 .7057 250 1.4578 .4189E-04 .1894E-03 .7057 250 1.4518 .4173FE-04 .18623E-03 .7053 300 1.4508 .41552E-04 .18678E-03 .7048 350 1.4599 .41334E-04 .18509E-03 .7042 400 1.4609 .41083E-04 .18514E-03 .7035 450 1.4627 .4079E-04 .186314E-03 .7035 550 1.4729 .4013EE-04 .1753FE-03 .7020 550 1.4729 .4013EE-04 .1753FE-03 .7020 650 1.4784 .3975BE-04 .1753FE-03 .7012 650 1.4651 .39749E-04 .16989E-03 .6966 700 1.4964 .38910E-04 .16659E-03 .6996 750 1.4969 .3842E-04 .1659FE-03 .6999 750 1.4969 .3842E-04 .15964E-03 .6958 8850 1.5144 .37423E-04 .15964E-03 .6958 8850 1.5144 .37423E-04 .15964E-03 .6958 900 1.5247 .36875E-04 .15964E-03 .6958 1.5050 1.5547 .36875E-04 .15964E-03 .6956 1.000 1.55410 .3570BE-04 .14813E-03 .6946 1.050 1.5506 .35703E-04 .14813E-03 .6946 1.050 1.5634 .34461E-04 .13634E-03 .6946 1.050 1.5634 .34461E-04 .13634E-03 .6946 1.050 1.5634 .34461E-04 .13634E-03 .6959 1.500 1.5636 .37946E-04 .13985E-03 .6956 1.500 1.5649 .3570BE-04 .13985E-03 .6959 1.200 1.5820 .3315EE-04 .13985E-03 .6959 1.200 1.5820 .3315EE-04 .12928E-03 .6837 1.4000 1.5636 .7914E-04 .13634E-03 .6922 1.550 1.6649 .29191E-04 .11867E-03 .6837 1.4000 1.5635 .7912E-04 .12928E-03 .6836 1.5500 1.6499 .29191E-04 .11867E-03 .6837 1.4000 1.6493 .26539E-04 .10876E-03 .6837 1.5000 1.6493 .26539E-04 .10876E-03 .6837 1.5000 1.6493 .26539E-04 .10876E-03 .6837 1.5000 1.6493 .26539E-04 .10876E-03 .6837 1.6000 1.6493 .26539E-04 .10876E-03 .6837 1.6000 1.6493 .26539E-04 .96642E-04 .6838 1.6500 1.6649 .27120E-04 .99497E-04 .6667 1.700 1.6693 .26539E-04 .96642E-04 .6830 1.6500 1.6698 .26539E-04 .88992E-04 .6911	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		the control of the co		
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.550					
.600				그 그 그 중 경험을 하는 그 때문에 가장 그 없는 그 사람들이 되었다.	
.650					
.700	The second of th		and the first transfer of the contract of the		11 A. A. A.
.750		1.4851	• 39349E+64		
.800			.38910E-04	.16659E-03	
.850	.750	1.4969	. 38442E-84	.16317E-03	•6979
.900	.800	1.5068		.15964E-03	•6968
.950	.850	1.5144	.37423E-04	•15595E+03	.6958
1.000	:		- 36875E+84		
1.050	. 950	1:5322 master	.36302E-04	.14813E-03	•6946
1.100		1.5410	.35708E-04	•14404E-03	
1.150		1.5506	.35093E-04	•13985E-03	
1.200 1.5820 .33156E-04 .12928E-03 .6873 1.250 1.5898 .32488E-04 .12572E-03 .6856 1.300 1.5992 .31815E-04 .12218E-03 .6844 1.350 1.6000 .31140E-04 .11867E-03 .6837 1.400 1.6157 .30464E-04 .11531E-03 .6829 1.450 1.6249 .29791E-04 .11201E-03 .6827 1.500 1.6293 .29124E-04 .10876E-03 .6830 1.550 1.6360 .28463E-04 .10560E-03 .6830 1.600 1.6433 .27812E-04 .10560E-03 .6850 1.650 1.6493 .27170E-04 .99497E-04 .6867 1.750 1.6541 .25921E-04 .94009E-04 .6890 1.850 1.6604 .24719E-04 .88992E-04 .6911 1.900 1.6598 .24137E-04 .86605E-04 .6923 1.950 1.6624 .23568E-04 .84290E-04 .6937	1.100	1.5634	•34461E-84	.13634E-93	•6922
1.250 1.5898 .32488E-04 .12572E-03 .6856 1.300 1.5992 .31815E-04 .12218E-03 .6844 1.350 1.6080 .71140E-04 .11867E-03 .6837 1.400 1.6157 .30464E-84 .11531E-03 .6829 1.450 1.6249 .29791E-04 .11201E-03 .6827 1.500 1.6293 .29124E-04 .10876E-03 .6830 1.550 1.6360 .28463E-04 .10560E-03 .6830 1.600 1.6433 .27812E-04 .10250E-03 .6850 1.650 1.6449 .27170E-04 .99497E-04 .6867 1.750 1.6541 .25921E-04 .94009E-04 .6890 1.850 1.6604 .24719E-04 .80992E-04 .6911 1.900 1.6598 .24137E-04 .86605E-04 .6923 1.950 1.6624 .23568E-04 .84290E-04 .6937	1.150	1.5697	.73814E-04	.13282E-03	.6895
1.300 1.5992 .31815E-D4 .12216E-03 .6844 1.350 1.6080 .31140E-04 .11867E-03 .6837 1.400 1.6157 .30464E-84 .11531E-03 .6829 1.450 1.6249 .29791E-04 .11201E-03 .6827 1.500 1.6293 .79124E-04 .10876E-03 .6830 1.550 1.6360 .28463E-04 .10560E-03 .6830 1.650 1.6433 .27812E-04 .10250E-03 .6850 1.650 1.6449 .27170E-04 .99497E-04 .6867 1.750 1.6493 .26539E-04 .96642E-04 .6882 1.750 1.6541 .25921E-04 .94009E-04 .6890 1.850 1.6604 .24719E-04 .80992E-04 .6911 1.900 1.6598 .24137E-04 .86605E-04 .6923 1.950 1.6624 .23568E-04 .84290E-04 .6937	1.200	1.5820	.3315 EE-84	•12928E-03	.6873
1.350 1.6080 .31140004 .11867003 .6837 1.400 1.6157 .3046400000 .11531003 .6829 1.450 1.6249 .297910000 .112010003 .6827 1.500 1.6293 .291240000 .108760003 .6830 1.550 1.6360 .28463000 .10560000 .6830 1.600 1.6433 .27812000 .10250000 .6850 1.650 1.6449 .27170000 .99497000 .6867 1.700 1.6493 .26539000 .96642000 .6882 1.750 1.6541 .25921000 .94009000 .6890 1.850 1.6604 .24719000 .88992000 .6911 1.900 1.6698 .24137000 .86605000 .6923 1.950 1.6624 .23568000 .84290000 .6937	1.250	1.5898	.32488E-84	.12572E-03	.6856
1.400 1.6157 .30464E-84 .11531E-03 .6829 1.450 1.6249 .29791E-04 .11201E-03 .6827 1.500 1.6293 .79124E-04 .10876E-03 .6830 1.550 1.6360 .28463E-04 .10560E-03 .6838 1.600 1.6433 .27812E-04 .10250E-03 .6850 1.650 1.6449 .27170E-04 .99497E-04 .6867 1.700 1.6493 .26539E-04 .96642E-04 .6882 1.750 1.6541 .25921E-04 .94009E-04 .6890 1.800 1.6555 .25314E-04 .91460E-04 .6899 1.850 1.6604 .24719E-04 .88992E-04 .6911 1.900 1.6524 .23568E-04 .84290E-04 .6937	1.300	1.5992	.31815E-D4	.12216E-03	.6844
1.450 1.6249 .29791E-04 .11201E-03 .6827 1.500 1.6293 .29124E-04 .10876E-03 .6830 1.550 1.6360 .28463E-04 .10560E-03 .6838 1.600 1.6433 .27812E-04 .10250E-03 .6850 1.650 1.6449 .27170E-04 .99497E-04 .6867 1.700 1.6493 .26539E-04 .96642E-04 .6882 1.750 1.6541 .25921E-04 .94009E-04 .6890 1.800 1.6555 .25314E-04 .91460E-04 .6899 1.850 1.6604 .24719E-04 .88992E-04 .6911 1.900 1.6524 .23568E-04 .84290E-04 .6937	1.350	1.6080	.3114PE-04	.11867E-03	.6837
1.500 1.6293 .79124E-04 .10876E-03 .6830 1.550 1.6360 .28463E-04 .10560E-03 .6038 1.600 1.6433 .27812E-04 .10250E-03 .6850 1.650 1.6449 .27170E-04 .99497E-04 .6867 1.700 1.6493 .26539E-04 .96642E-04 .6882 1.750 1.6541 .25921E-04 .94009E-04 .6890 1.800 1.6555 .25314E-04 .91460E-04 .6899 1.850 1.6604 .24719E-04 .86992E-04 .6911 1.900 1.6598 .24137E-04 .86605E-04 .6923 1.950 1.6624 .23568E-04 .84290E-04 .6937	1.400	1.6157	.30464E-84	.11531E-03	.6829
1.550 1.6360 .28463E-04 .10560E-03 .6838 1.600 1.6433 .27812E-04 .10250E-03 .6850 1.650 1.6449 .27170E-04 .99497E-04 .6867 1.700 1.6493 .26539E-04 .96642E-04 .6882 1.750 1.6541 .25921E-04 .94009E-04 .6890 1.800 1.6555 .25314E-04 .91460E-04 .6899 1.850 1.6604 .24719E-04 .88992E-04 .6911 1.900 1.6598 .24137E-04 .86605E-04 .6923 1.950 1.6624 .23568E-04 .84290E-04 .6937	1.458	1.6249	.29791E-04	.11201E-03	.6827
1.600 1.6433 .27812E-04 .10250E-03 .6850 1.650 1.6493 .27170E-04 .99497E-04 .6867 1.700 1.6493 .26539E-04 .96642E-04 .6882 1.750 1.6541 .25921E-04 .94009E-04 .6890 1.800 1.6555 .25314E-04 .91460E-04 .6899 1.850 1.6604 .24719E-04 .88992E-04 .6911 1.900 1.6598 .24137E-04 .86605E-04 .6923 1.950 1.6624 .23568E-04 .84290E-04 .6937	1.500	1.6293	.79124E-84	.108765-03	.6830
1.600 1.6433 .27812E-04 .10250E-03 .6850 1.650 1.6493 .27170E-04 .99497E-04 .6867 1.700 1.6493 .26539E-04 .96642E-04 .6882 1.750 1.6541 .25921E-04 .94009E-04 .6890 1.800 1.6555 .25314E-04 .91460E-04 .6899 1.850 1.6604 .24719E-04 .88992E-04 .6911 1.900 1.6598 .24137E-04 .86605E-04 .6923 1.950 1.6624 .23568E-04 .84290E-04 .6937	1.550	1.6360	-28463E-04	.10560E-03	.6838
1.650 1.6449 .27170E-04 .99497E-04 .6667 1.700 1.6493 .26539E-04 .96642E-04 .6882 1.750 1.6541 .25921E-04 .94009E-04 .6890 1.800 1.6555 .25314E-04 .91460E-04 .6899 1.850 1.6604 .24719E-04 .88992E-04 .6911 1.900 1.6598 .24137E-04 .86605E-04 .6923 1.950 1.6624 .23568E-04 .84290E-04 .6937			-27812E-04	.10250E-03	.6850
1.700 1.6493 .26539E-04 .96642E-04 .6882 1.750 1.6541 .25921E-04 .94009E-04 .6690 1.800 1.6555 .25314E-04 .91460E-04 .6899 1.850 1.6604 .24719E-04 .88992E-04 .6911 1.900 1.6598 .24137E-04 .86605E-04 .6923 1.950 1.6624 .23568E-04 .84290E-04 .6937	1.650	1,6449	.27170E-04	.99497E-04	-6867
1.750 1.6541 .25921E-04 .94009E-04 .6890 1.800 1.6555 .25314E-04 .91460E-04 .6899 1.850 1.6604 .24719E-04 .88992E-04 .6911 1.900 1.6598 .24137E-04 .86605E-04 .6923 1.950 1.6624 .23568E-04 .84290E-04 .6937					
1.800				.94009E-04	
1.850 1.6604 .24719E-04 .80992E-04 .6911 1.900 1.6598 .24137E-04 .86605E-04 .6923 1.950 1.6624 .23568E-04 .84290E-04 .6937					
1.900 1.6598 .24137E-04 .66605E-04 .6923 1.950 1.6624 .23568E-04 .64290E-04 .6937			.24719E-04		
1.950 1.6624 .23568E-04 .84290E-04 .6937					
그렇게 다른 그는 그는 그는 그는 그는 그는 그는 그는 그는 그를 하고 있었다. 그는 그를 하는 그는 그를 하는 것이 없는 그를 하는 것이 없는 것이 없는 것이 없다.					

ORIGINAL PACTO

ORIGINAL PAGE IS OF POOR QUALITY

TAPLE II. REAL-GAS ISENTROPIC EXPANSIONS OF PARAMYDROGEN

				A	1. 1. 1. 1.		44	3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		·	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	*	
		G. TT	= 201.0	K PT =	1.0 ATM	RHOT =	.123E-03	G/CM3	SVT =1054	.285 M/Si	Ē C '		
MACH	REZM	7	CP/CV	SV/SVT	P/PT	TAIT	RHOZRHOT	A*/A	SV/SVT	P/PT	1/11	RHO/RHOT	AT/A
												GAS VALUE	
		ing the second of the second o									의 경기 기계속 기계 인접하면 경취 # 전	inger Ngjaran	* 175, 35 15 * 175, 35 15 * 175, 35 15
0.000	8.	1.0007	1.3458	1.0000	1.0000	1.0000	1.0000	0.0000		1.0000	1.0080	1.0000	1.00CO
.050	.948E+06	1.0007	1.3457	9998	• 9982	• 9996	9986	.0659		•9999	1.0001	• 9999	.9951
•100	.189E+07	1.0007	1.3456	9991	.9973	.9983	•9950	.1711	1.0901	1.0003	1.0003		.9953
-150	.2026+07	1.0007	1.7454	9979	.9650	.9961	-9866	• 2545	1.0002	1.0006	1.0006	1.5000	. 9954
-200	•373E+07	1.0007	1.3452	9963	.9735	.9931	.9803	.3359	1.0003	1.0011	1.0011	1.0000	• 9955
•250 •20	-461E+07	1.0007	1,3449	9943	.9589	.9593	.9693	.4143	1.0005	1.0015	1.0017	• 9998	. 9955
.300	-546E+07	1.0006	1.3445	.9918	-9416	-9847	•9562	.4893	1.0007	1.0022	1.0024	-9998	.9957
.359	.627E+07	1.9906	1.3440	.9889	.921E	.9793	.9413	.5603	1.0910	1.0033	1.0033	1.0000	. 9962
.400	-705E+07	1.0006	1.3435	9856	.8993	.9732	9242	.6266	1.0013	1.0042	1.0043	• 9999	. 9963
.450	•777E+07	1.0006	1.3430	.9819	.8747	9663	-9852	.6879	1.0016	1.0051	1.0055	• 9997	.9965
-500	.8455+87	1.0006	1.3424	.9779	. 8483	.9588	+6848	.7441	1.0020	1.0063	1.0068	• 9996	.9969
•550	•908E+07	1.0006	1.3416	.9735	.8204	.9587	•8631	.7947	1.0725	1.0076	1.0082	• 9996	-9973
-600	.965E+07	1.0005	1.3412	9687	.7910	.9419	.8399	.8395	1.0030	1.0089	1.0097	, 9993	.9975
-650	.102E+08	1.0005	1.3406	9637	.7607	-9326	.5158	6788		1.0104	1.0114	9993	9980
.700 .750	+1065+08 +110E+08	1.0005	1.3400 1.3395	.9584 .9527	.7294	.9227	.7907	. 91 22	1.0042	1.0118	1.0131	• 9989	.9983
1.14		and the control of the control of the		The state of the s	.6978	9124	•7650	-9401	1.0049	1.0135	1.0150	. 9987	9988
.800 .850	.114E+08	1.0005	1.3389	-9469	.6660	.9816	.7388	.9625	1.0057	1.0152	1.0170	.9984	• 9993
•900	.117E+08	1.0004	1,4384	9408	-6339	-8904	-7121	9793	1.0065	1.0166	1.0191	. 9979	9995
			1.3380	. 9345	.6020	8789	-6852	.9911	1.0074	1.0182	1.0212	9973	.9998
.950	-121E+08	1.0004	1.3377	9280	.5704	-8678	-6561	.9978	1.0063	1.0196	1.9235	9355	1.8900
1.080	•123E+08	1.0004	1.7774	9714	-5393	.8548	.6311	1.0000	1.0094	1.0209	1.0258		1.0000
1.050	-1245+08	1.0003	1.3373	.9146	.50A8	+6424	.6042	. 9978	0104	1.0219	1.0281	• 9943	•9999
1.100	.1247+08	1.0003	1.3374	9077	•4790	.8297	•5776	.9917	1.0116	1.0227	1.0305	• 9929	.9995
1.150	.1247+08	1.0003	1.3376	9007	•4502	-8168	•5514	.9822	1.0126	1.0236	1.0328	.9914	.9993
1.200	.124F+78	1.000	1.3380	8935	·4723	.8037	-5257	• 969*	1.0141	1.0241	1.0352	9897	. 9988
1.250	.124E+08	1.0903	1.3385	. 8863	.3954	.7905	•5004	. 9534	1.0154	1.0242	1.0375	•9876	.9980
1.300	·123E+08	1.0002	1.3393	.8790	• 3697	. 7771	•4759		1.0168	1.0242	1.0398	+ 9855	. 9972
1.350	.1217+05	1.0002	1.3404	.8717	3450	.7636	4520	.9147	1.0183	1.0238	1.0420	.9830	• 9962
1.400	.1205+08	1.0002	1.3417	. 8643	.3215	.7501	-4288	.8924	1.0198		1.0441	.9804	•9950
1.450	.1185+08	1.0002	1.3473	• 8569	.2991	.7364	-41164	.8684	1.0213	1.0218	1.0460	.9774	9934
1.500	.1165+08	1.0002	1.3453	. 6495	2779	.7226	.3847	.8431	1.0229	1.0201	1.0478	. 9741	•9916
1.550	-114E+D8	1.6002	1.3476	.8420	.2577	.7088	.3638	.816.	1.0246	-1.0177	1.0494	.9783	.9893
1.600	•112E+08	1.0001	1.3503	.8346	.2388	. 6949	-3438	.7894	1.0262	1.0148	1.0507	. 9664	.9869
1.650	.189E+B6	1.0701	1.3534	.8271	.2209	.6810		.7616	1.0279	1.0114	1.0518		. 9842
1.700	.107E+08	1.0001	1.3570	.5197	.2041	-6670	-3062	.7336	1.0297	1.0074	1.8526	.9577	.9813
1.750	.1045+08	1.0001	1.3611	.8122	.1884	-6531	.2856	.7055	1.0314	1.0030		. 9530	.9782
1.800	.102E+08	1.0001	1.3656	.6046	1736	6390	.2719	.6774	1.0331	• 9978	1.0531	•9480	•9747
1.850	.991E+07	1.0001	1.3707	. 7974	•1599	-6251	•2559	+649?	1.0349	.9917	1.0526	. 9425	.9707
1.901	.9645+07	1,0001	1.3764	.7900	-1470	-6189	.2408	.6216	1.0366	.9853	1.0520	.9372	49668
1.950	•937E+87	1.0001	1.3827	.7826	.1351	-5968	.2265	• 5943	1.0384	.9780	1.0507	. 9313	-9624
2.000	• 91 DE+07	1.0001	1.3896	.7752	.1240	.5827	.21? 9	.5676	1.0401	. 9701	1.0490	.9254	.9578

G. (CONTINUED)

		. (CONTINUED)		
MACH	LOCAL ISENTROPIC	VISCOSITY	THERMAL CONDUCTIVITY	
	EXPANSION COEFF.	G/CM-SEC	GAL/CH-SEC-K	NUMBER
	on a heli olare <u>y</u> e <u>silatear</u> e			
0.000		.68161E-04	.37298E-N3	.7022
.050	1.3157	.68141E-04	.37290E-03	.7022
.100	1.3601	.68081E-04	-37266E-03	.7022
.150	1.3462	.67981E-04	.37225E-03	.7022
.200	1.3+61	.67842E-04	.37169E-03	.7822
.250	1.3412	.67665E-04	.37096E-03	.7022
.300	1.3456	•67450E-04	.37009E-03	.7022
• 350	1.3498	.67199E-04	.36907E-03	.7022
.400	1.3431	.66912E-04	-36791E-03	.702?
- 450 - 500	1.3415	.66591E-04	.36662E-03	.7821
.500 550	1.3.41	.66238E+04	•36520E-03	-7019
.550	1.3436	.65853E-04	.36365E-03	.7017
.600	1.3-12	.65439E-04	•36172E-03	.7019
.650	1.3438	.64996E-04	.35894E-03	.7035
.700	1.3401	.64526E-04	.35600E-03	.7050
.750	1.3417	.64033E-04	-35293E-03	.7066
.800	1.3417	.63515E-04	.34972E-03	.7882
. 850	1.3391	.62976E-04	•34639E-03	•7096
.900	1.3400	.62416E-04	.34295E-03	.7110
.950	1.3363	.61838E-84	.33941E-03	.7123
1.000	1.3375	.61243E-04	.33579E-03	.7134
1.050	1.3373	.60631E-04	.33208E-03	.7143
1.100	1.3768	.50007E-04	.32630E-03	.7158
1.157	1.3384	•59362E-04	.32446E-03	.7154
1.200	1.3375	•5870 9E-04	.32057E+03	.7155
1.250	1.3378	.58042E-04	•31663E=03	.7152
1.300	1.3400	.57364E+04	.312€5E=83	.7146
1.350	1.3407	.56677E-04	.30863E-03	.7135
1.400	1.3415	.55980E-04	-30459E-03	.7120
1.450	1.3426	.552735-04	•30052F-03	.7100
1.500	1.3444	.54557E-04	•29642E-03	.7075
1.550	1.3456	.53837E-84	.26994E-03	.7102
1.600	1,3490 - 111 in the second	-53099E-04	-28337E-03	.7126
1 • 650	1.3518	•52357E-04	•27677E-03	.7147
1.708	1.3557	.5160BE-04	.27015E-03	.7164
1.750	1.3608	•50851E-04	.76357E-03	.7176
1.800	1.3636	.500 R EE-04	.25688E-73	.7164
1.850	1.3673	.49312E-04	-25022E-03	.7189
1.900	1.3747	.48531E-04	.24356E-03	.7188
1.950	1.3793	-47742E-84	-23688F-03	.7183
2.000	1.3860	.46945E-04	.23021E-03	.7174

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- (4) - (1) (4) (4) (4) - (4) (4) (4) (4) (4) - (4) (4)

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TABLE I. REAL-GAS ISENTROPIC EXPANSIONS OF PARAHYCROGEN

		H. 11	= 300.0	K PT =	1.0 ATM	PHOT =	.818E-04	G/CH3	SVT =1389	.789 M/S	EC		
MACH	REZM	z	CP/CV	SV/SVT	P/PT	TALL	RHOZRHOT	A#/1	SV/SVT	P/PT	7 T/TT	RHO/RHOT	A-/A
		-				,	10,000			RELATIVE		GAS VALUES	
				gart en de	1				n di kacamatan di Kabupatèn Kabupatèn Kabupatèn Kabupatèn Kabupatèn Kabupatèn Kabupatèn Kabupatèn Kabupatèn Ka Kabupatèn Kabupatèn			4-4 there.	
0.900	0.	1.0006	1.3697	1.0000	1.0000	1.0000	1.0000	9.0081	1.0000	1.0000	1.0000	1.0000	1.0000
.050	.597E+06	1.0006	1.3849	9997	9982	.9995	.9987	.0863		.9999	1.0000	9999	1.0884
.100	.119E+07	1.0006	1.3848	.9990	. 9931	. 9961	.9958	.1716		1.0290	1.0001	1.0000	1.0004
•15 D	.178E+97	1.0006	1.3846	.9977	- 9845	.9957	.9886	.2558		1.0001	1.0002	9999	1.0004
.200	-235E+07	1.0006	1.3844	• 9960	9728	.9924	.9803	.3376	.9999	1.0003	1.0003	1.0000	1.0004
.250	-290E+07	1.0006	1.3840	. 9937	.9579	-9881	9694	.4164	•9999	1.0905	1.0005	1.9000	1.0004
.300	+344E+87	1.0006	1.3837	.9911	-9411	.9830	•9564	.4915	.9999	1.0007	1.0007	1.0000	1.0993
.350	.395E+07	1.0006	1.3832	.9876	.9196	.9770	- #9413	.5626	.9998	1.0009	1.0010	1.0000	1-0002
•400	•444E+07	1.0006	1.3327	- 9842	8966	9702	•9242	.6290	.9998	1.0012	1,0013	. 9999	1.0002
•450	+490E+07	1.0006	1.3821	-9801	.8718	•9625	-9056	-6985	.9997	1.0017	1.0016	1.0081	1.0003
.500	.533E+07	1.0005	1.3814	.9756	8447	.9543	.8851	.7464	. 9997	1.0819	1.0021	1.0000	1.0001
•550	.5735+07	1.0005	1.3806	.9707	.8161	.9453	.8634	.7966	. 9996	1.0524	1.0025	. 9999	1.0000
.600	.609E+07	1,0005	1.3797	. 9654	•78E3	.9357	-8484	-8416		1.0030	1.0031	1.0000	1.0000
•650	•642E+97	1.0005	1.3788	. 9598	.7556	. 9255	.8165	.8606	.9995	1.0836	1.0037	1.0001	1.0800
.700	.671E+07	1.0005	1.3778	.9538	.7240	.9147	•7916	.9137	.9995	1.0042	1.0044	1.0000	. 9999
.751	-697E+07	1.0905	1.3767	• 9475	•6919	.9835	•7659	.9489	.9994	1.0048	1.0051	.9998	.9397
.800	.728E+07	1.0004	1,3754	.9418	6598	.8918	.7399	.9629	.9994	1.0057	1.0060	.9999	•9997
.850	•739E+07	1.0004	1.3741	. 9341	6277	,8798	-7136	.9795		1.0066	1.0069	• 9999	.9997
•900	.755E+07	1.0004	1.3727	.9270	-5959	.6674	.6872	• 9912	. 9993	1.0079	1.0079	1.0002	1.0000
.950	.767E+07	1.0084	1.3717	9197	• 5644	.8548	•6605	.9977	9993	1.0089	1.0090	1.0001	.9999
1.000	.777E+07	1.0004	1.7697	. 9123	.5337	8419	.6341	1.0000	.9993	1.0102	1.0103	1.0002	1.0000
1.050	.784E+07	1.0004	1.3680	.9046	•5037	.6288	.6078	.9981	. 9994	1.8116	1.0116	1.0003	1.0801
1.100	.788E+07	1.0003	1.3663	.8968	. 4744	*8156	.5818	. 9921	. 9994	1.0128	1.0130	1.0001	1.0000
1.150	.789E+07	1.0003	1.3645	. 5588	.4461	.6723	.5561	. 9827		1.0142	1.0145	. 9999	9999
1.200	.788E+07	1.0003	1.3627	.8808	.4188	.7890	.5310	. 9784	.9996	1.0157	1.8162	.9998	.9999
1.250	.785E+07	1.0003	1.3608	.8727	.3927	.7756	.5865	. 9552	.9998	1.0173	1.8179	. 9997	. 9999
1.300	.779E+07	1.0003	1.3589	- 8645	.3677	.7622	.4825	. 9376		1.0166	1.0196	. 9994	. 9998
1.350	.772E+07	1,0003	1.3570	.8562	-3436	.7486	-4593	.9178		1.0202	1.0217	.9989	. 9995
1.400	.763E+07	1.0002	1.3550	. 8480	.3711	.7355	. 4367	. 6963	1.0805	1.0216	1.0238	. 9984	.9993
1.450	.753E+07	1.0002	1.3531	.8397	2 995	.7222	.4148	.8732	1.0008	1.0231	1.0259	.9976	.9989
1.500	.741E+07	1.0002	1.3512	.8314	.2791	.7091	.3936	.8490	1.0012	1.0246	1.0282	. 9969	.9985
1.550	.728E+07	1,0002	1.3494	.6232	.2598	-6961	.3733	.8235	1.0016	1.0256	1.0305	. 9957	.9976
1.600	•714E+07	1.0002	1.3476	.8149	.2416	.6631	·3536	.7975	1.0021	1.8268	1.0326	. 9945	.9971
1.650	•6995+07	1.0002	1.3459	.8067	.2245	.6793	.3356	.7710	1.0026	1.0279	1.0353	• 9933	.9963
1.700	.683E+07	1.0002	1.3442	.7986	-2084	.6576	.3178	.7440	1.0032	1.0285	1.0377	•9916	.9952
1.750	.667E+07	1.0002	1.3428	.7905	.1933	.6451	-2998	.7169	1.0038	1.0291	1.0402	.9898	.9940
1.800	.650E+07	1.0091	1.3414	.7625	.1791	.6327	.2633	.6897		1.0293	1.0428	.9876	.9925
1.850	.633E+07	1.0001	1.3402	.7745	.1659	-6285	.2675	.6627		1.0294	1.0453	.9853	.9989
1.900	. 61 6E+0 7	1.0991	1.7392	. 7667	.1536	-6085	.2525	.6359	1.0861	1.0290	1.0477	.9826	-9899
1.950	•598E+07	1.0081	1.7383	.7589	•1420	.5965	-2382	.6095	1.0069	1.0283	1.0502	.9797	.9869
2.000	.561E+07	1.0001	1.3377	.7512	.1313	.5848	.2245	.5835		1.0273	1.0526	.9765	.9846

H. (CONTINUED)

MACH	LOCAL ISENTROPIC	VISCOSITY	THERMAL CONDUCTIVITY	PRANDTL
	EXPANSION COEFF.	G/CM-SEC	CAL/GM-SEC-K	NUMBER
0.000		.89603E-04	.46141E-03	.7096
.050	1.3616	.89563E-84	.46128E-03	.6893
.100	1.3898	.89496E-04	.46090E-03	.6893
.150	1.3845	.89352E-04	.46026E-113	.6893
.200	1.3865	.89151E-04	.45936E-03	6894
. 250	1.3847	.88694E-84	.45825E-03	.6895
.300	1.3839	.88583E-04	.45688E-03	.6897
.350	1.3834	.88219E-04	.45529E-03	.6898
.480	1.3830	.87805E-04	.45348E-#3	.6900
. 450	1.3868	.87342E-04	.45147E-03	.6903
. 500	1.3794	.86833E-04	•44925E-03	.6905
• 55 0	1.3808	.86280E-04	.44686E-03	-6908
.600	1.3814	.85686E-04	.44429E-83	.6911
.650	1.3806	.85053E-04	-44159F+03	.6915
.700	1.3774	.84385E-84	. 43886E-03	.6.916
.750	1.3756	.83684E-04	.43602E-03	.6919
. 800	1.3775	.82954E-04	.43307E-D3	.6921
.850	1.3753	.82196E-0+	.43002E-03	. 6924
. 900	1.3762	.81414E-04	.42689E-03	.6928
.950	1.3715	.80611E-04	.42368E-03	.5931
1.000	1.3721	.79790E-04	.42042E-03	.6935
1.050	1.3705	.78957E-84	.41712E-03	.6939
1.100	1.3665	.78100E-04	.41377E-83	.6943
1.150	1.3651	.77238E-04	.41041E-03	-6948
1.200	1.3644	.76366E-04	.40702E-03	-6952
1.250	1.3627	.75487E-D4	.40356E-03	-6957
1.300	1.7683	.74603E-04	.39978E-03	-6968
1.350	1.3574	.73715E-04	.39599E-03	• 69 79
1.400	1.3568	•72825E-04	.39223E-03	-6988
1.450	1.3535	.71934E-04	.38848E-83	.6997
1.500	1.3531	.71044E-84	.38476E-03	.7005
1.550	1.3492	.70154E-04	.36107E-03	.7011
1.600	1.3467	-69268E-84	.37741E-03	.7016
1.650	1.3477	.68384E-04	.37379E-03	.7020
1.700	1.3445	.67504E-04	.37021E-03	.7021
1.750	1.3443	.66628E-04	.36665E-03	.7020
1.800	1.3418	.65756E-04	.36316E-03	.7015
1.850	1.3420	.64888E-04	.35822E-03	.7037
1.900	1.3402	.6402EE-04	-35284E-03	.7965
1.950	1.3396	.63168E-04	.34752E-03	.7090
2.000	1.3394	.62314E-84	.34227E-03	.7112

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TABLE II. REAL-GAS ISENTROPIC EXPANSIONS OF PARAHYDROGEN

1		and the second second			•			•				
	A. TT	= 30.0 K	PT =	3.0 ATM	RHOT =	.275E-02	G/CH3	SVT = 433	165 H/SE	C		
RE/M	, ,	CP/CV	SV/SVT	P/PT	1/11	RHOZRHOT	A*/A	SV/SVT	P/PT	T/TT	PHO/RHOT	A*/I
					24 C	in a second			CENTAL	IO TOWN	AND ANTOES	,
0.	.8930	1.9215	1.0000	1.0000	1.0000	1.0000	0.0000	1.0000	1.0000	1.0860	4 2000	
.3575+08	8929	1.9215	• 9995	9979	.9991							1.0000
.712E+96	.8929	1.9714	. 9982	. 9915								1.0341
.106E+09	.8928	1.9214	.9960									1.0334
.141E+09	.8927	1.9214	.9928	9670								1.0311
.175E+09	.8926	1.9213	. 9889	9489								1.0293
.208E+89	.8925	1.9711	.9841	.9276			and the second second					1.0272
.240E+09	.8923	1.9210	.9786	9833	The second secon							
.270E+09	.8921	1.9208	9723									1.8250
.300E+09	8919	1.9205	-9653									1.0226
.328E+09	.8917	1.9202	.9577									1.0200
.3555+09	.1915	1.9198	9495		N							1.8174
.380E+09	.8913	1.9193	. 9408	.7509								1.0146
.404E+09	.8911	1.9187	. 9316	7168		' .	and the second second					
.427E+89	.8979	1.9180	.9220				* *					1.0096
.448E+09	.8907	1.9171	.9119			at the second of						
.467E+09	8905	1.9161	and the second s									1.0052
.485E+09	.8903	1.9151										1.0035
·502E+09	.8902					The second secon						1.0020
.517E+09	.8900		and the second second				the state of the s					1.0009
.531E+09	.8899	1.9113	44.									1.0003
.543E+09	. 8897		the state of the s									1.0000
.555E+D9	. 6896	1.9087	.8353	4285	-7111	-6048	.9932	.9309	9149	.8632	1.0390	1.0003
	0. 357E+08 -712E+08 -712E+09 -106E+09 -141E+09 -175E+09 -206E+09 -270E+09 -308E+09 -358E+09 -407E+09 -408E+09 -408E+09 -408E+09 -408E+09 -517E+09 -517E+09 -513E+09	RE/M Z 08930 .3575+08 .8929 .712E+08 .8929 .712E+08 .8929 .106E+09 .8927 .175E+09 .8926 .20E+09 .8925 .240E+09 .8921 .300E+09 .8919 .378E+09 .8917 .355E+09 .8917 .355E+09 .8913 .404E+09 .8913 .404E+09 .8907 .467E+09 .8907	RE/M Z CP/CV 08930 1.9215 .3575+08 .8929 1.9215 .712E+08 .8929 1.9214 .106E+09 .8928 1.9214 .106E+09 .8926 1.9214 .175E+09 .8926 1.9213 .208E+09 .8925 1.9211 .240E+09 .8923 1.9210 .270E+09 .8921 1.9208 .308E+09 .8919 1.9205 .328E+09 .8919 1.9205 .328E+09 .8919 1.9205 .388E+09 .8917 1.9202 .380E+09 .8913 1.9193 .404E+09 .8913 1.9193 .404E+09 .8911 1.9187 .427E+09 .8909 1.9180 .448E+09 .8907 1.9171 .467E+09 .8905 1.9161 .485E+09 .8903 1.9151 .502E+09 .8903 1.9153 .502E+09 .8909 1.9139 .517E+09 .8909 1.9139 .517E+09 .8909 1.9113	RE/M Z CP/CV SV/SVT 0	RE/M Z CP/CV SV/SVT P/PT 0.	RE/M Z CP/CV SV/SVT P/PT T/TT 0	RE/M Z CP/CV SV/SVT P/PT T/TT RHO/RHOT 08930 1.9215 1.0000 1.0000 1.0000 1.0000 .3575+08 .8929 1.9215 .9995 .9979 .9991 .9988 .712E+08 .8929 1.9214 .9982 .915 .9966 .9950 .106E+09 .8928 1.9214 .9960 .9811 .9924 .9888 .141E+09 .8927 1.9214 .9928 .9670 .9865 .9804 .775E+09 .8926 1.9213 .9889 .9489 .9791 .9695 .240E+09 .8925 1.9211 .9841 .9276 .9702 .9566 .240E+09 .8923 1.9210 .9786 .9833 .9599 .9418 .270E+09 .8921 1.9208 .9723 .8765 .9482 .9252 .300E+09 .8919 1.9205 .9653 .8474 .9354 .9069 .378E+09 .8917 1.9202 .9577 .8164 .9215 .8872 .355E+09 .8917 1.9202 .9577 .8164 .9215 .8872 .355E+09 .8917 1.9193 .9495 .7841 .9066 .6662 .380E+09 .8913 1.9193 .9408 .7509 .8909 .8444 .404E+09 .8911 1.9187 .9316 .7168 .8744 .8215 .427E+09 .8909 1.9180 .9220 .6827 .8574 .7981 .448E+09 .8907 1.9171 .9119 .6483 .8398 .7740 .467E+09 .8907 1.9171 .9119 .6483 .8398 .7740 .467E+09 .8907 1.9171 .9119 .6483 .8398 .7740 .465E+09 .8907 1.9139 .8801 .5485 .7851 .7808 .517E+09 .8907 1.9139 .8801 .5169 .7666 .7253	RE/M Z CP/CV SV/SVT P/PT T/TT RHG/RHOT A=/A 0.	RE/M Z CP/CV SV/SVT P/PT T/TT RHO/RHOT A*/A SV/SVT	RE/M	RE/M 7 CP/CV SV/SVT P/PT T/TT RHO/RHOT A*/A SV/SVT P/PT T/TT T/TT	RE/M 7 CP/CV SV/SVT P/PT T/TT RHO/RHOT A=/A SV/SVT P/PT T/TT PAO/RHOT TPELATIVE TO IDEAL FAS VALUES 08930 1.9215 1.0000 1.0000 1.0000 0.0000 1.00000 1.00000 1.00000 1.0000 1.00000 1.00000 1.00000 1.00000 1.00000 1.000

SATURATION SOUNDARY REACHED.

TABLE II. PEAL-GAS ISENTPOPIC EXPANSIONS OF PARAHYDROGEN

A. COUNTINUEDS

MACH	LOCAL ISENTROPIC EXPANSION COEFF.	VISCOSITY G/CH-SEC	THERMAL CONDUCTIVITY CAL/GN-SEC-K	PRANDTL NUMBER
0.000	1	.16676E-04	-61100E-04	.8029
•050	1.6971	.16662E-04	.61049E-04	.8029
. 100	1.6918	.16622E-04	.60897E-04	.8030
•150	1.6954	•16555E-04	.60644E-04	.8031
. 200	1.7087	.164635-04	•60295E-04	.8832
•250	1.6890	.16345E-04	.59847E-04	.8034
.300	1.6941	.16203E-04	.59306E-04	.8037
.350	1.6978	.16038E-04	.58680E-04	.8041
.400	1.6965	. 15653E-04	.57988E-04	.8043
.450	1.6929	-15647E-04	.57215E-84	.8946
•500	1.6927	.15423E-04	.56369E-04	.8051
•550	1.6887	.15163E-04	.55453E-04	.8058
.600	1.6947	.14928E-04	.54476E-04	.8066
. 650	1.6872	.14659E-04	.53442E-84	.8077
.700	1.6903	.14380E-04	.52455E-04	.8076
.750	1,6822	.14091E-04	.51429E-84	.8976
.800	1.6863	.13794E-84	.50340E-04	.8084
. 850	1.6833	-13491E-04	.49191E-04	.8099
.900	1.6805	.13183E-04	.47990E-04	.8123
950	1.6805	.12872E-04	.46745E-84	. 8155
1.000	1.6757	12558E-84	.45468E-04	.8197
1.050	1.6762	.12244E-04	.44147E-04	.8249
1.100	1.6738	.11931E-04	.42977E-04	.8288

SATURATION BOUNDARY REACHED.

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TABLE II. REAL-GAS ISENTROPIC EXPANSIONS OF PARAHYDROGEN

MACH RE/N Z CP/CV SV/SWT P/PT T/TT RHO/RHOT A*/A SV/SWT P/PT T	ang mang
.050	
.056 .284E+08 .9310 1.8248 .9996 .9979 .9991 .9987 .0891 .9998 .9996 .9996 .000 .567E+08 .9310 1.8248 .9982 .9917 .9966 .9951 .1773 .9992 .9987 .9986 .9981 .000 .200 .847E+08 .9309 1.6247 .9960 .9813 .9924 .9889 .2638 .9982 .9968 .9968 .9968 .9968 .200 .200 .112E+09 .9308 1.8245 .9929 .9670 .9866 .9804 .3475 .9969 .9943 .9944 1.000 .2550 .139E+09 .9377 1.8743 .9891 .9491 .9792 .9596 .4280 .9351 .9912 .9914 1.000 .3500 .1655E+09 .9306 1.8249 .9484 .9277 .9703 .9566 .5043 .9931 .9875 .9877 1.000 .3550 .191E+09 .9304 1.8237 .9787 .9035 .9600 .9417 .5759 .9907 .9834 .9835 1.000 .400 .215E+09 .9303 1.8234 .9725 .8758 .9484 .9253 .6426 .9880 .9790 .9787 1.000 .5500 .238E+09 .9301 1.6233 .9657 .8477 .9356 .9069 .7036 .9860 .9790 .9787 1.000 .5500 .261E+09 .9299 1.8230 .9562 .8168 .9217 .8872 .7588 .9819 .9889 .9678 1.000 .5500 .262E+09 .9297 1.8228 .9552 .7844 .9068 .9611 .8080 .9785 .9684 .9617 1.000 .5500 .328E+09 .9296 1.8225 .9416 .7510 .8914 .8441 .8514 .9749 .9579 .9553 1.000 .6600 .328E+09 .9296 1.8225 .9416 .7510 .8914 .8441 .8514 .9749 .9579 .9553 1.000 .6600 .328E+09 .9296 1.8222 .9325 .7170 .8746 .8212 .8887 .9711 .9524 .9486 1.000 .7500 .338E+09 .9297 1.8219 .9231 .6828 .8576 .7978 .9283 .9662 .9472 .9466 .9271 .001 .8000 .336E+09 .9296 1.8210 .9321 .6828 .8576 .7978 .9283 .9662 .9472 .9466 .9271 .001 .8000 .336E+09 .9296 1.8210 .9321 .6828 .8576 .7978 .9283 .9664 .9591 .9366 .9271 1.001 .8000 .336E+09 .9287 1.8210 .9321 .6828 .8576 .7978 .9283 .9664 .9591 .9366 .9271 1.001 .8000 .4000 .9283 1.8190 .8599 .4885 .7268 .7662 .6757 .9981 .9463 .9228 .9985 .9000 .	0 1.0800
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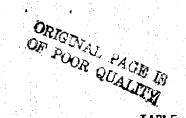
*210	
.250 .1396+09 .9307 1.8247 .9891 .9491 .9792 .9696 .4280 .9951 .9912 .9914 1.00 .350 .1655+09 .9306 1.8240 .9842 .9277 .9703 .9566 .5043 .9931 .9875 .9877 1.00 .350 .1916+09 .9304 1.8237 .9787 .9035 .9600 .9417 .5759 .9907 .9834 .9835 1.00 .400 .2156+09 .9303 1.8234 .9725 .8758 .9484 .9253 .6426 .9880 .9790 .9787 1.00 .450 .2386+09 .9301 1.8233 .9657 .8477 .9356 .9069 .7036 .9851 .9740 .9735 1.00 .5500 .2616+09 .9299 1.8230 .9582 .8168 .9217 .8872 .7588 .9819 .9689 .9678 1.00 .5500 .2616+09 .9297 1.8228 .9502 .7844 .9068 .9661 .8080 .9765 .9634 .9617 1.00 .5500 .3026+09 .9296 1.8228 .9502 .7844 .9068 .9661 .8080 .9765 .9634 .9617 1.00 .5500 .3026+09 .9296 1.8225 .9416 .7510 .8911 .8441 .8514 .9749 .9579 .9553 1.00 .6500 .3286+09 .9294 1.8222 .9325 .7170 .8746 .8212 .8887 .9711 .9524 .9486 1.00 .7500 .3386+09 .9294 1.8222 .9325 .7170 .8746 .8212 .8887 .9711 .9524 .9486 1.00 .750 .3366+09 .9297 1.8216 .9132 .6485 .8399 .7738 .9461 .9632 .9418 .9344 1.01 .8500 .3696+09 .9288 1.8211 .9030 .6144 .8219 .7493 .9461 .9632 .9418 .9344 1.01 .8500 .3836+09 .9287 1.8207 .8926 .5809 .8035 .7248 .9816 .9549 .9316 .9366 .9271 1.01 .8500 .3966+09 .9285 1.8202 .8819 .6485 .8399 .7738 .9461 .9632 .9418 .9344 1.01 .8500 .3966+09 .9285 1.8202 .8819 .6481 .7649 .7002 .9920 .9506 .9270 .9121 1.01 .8500 .4086+09 .9283 1.8190 .8599 .4855 .7475 .6514 1.0000 .9420 .9189 .8945 1.02 1.000 .4196+09 .9283 1.8190 .8599 .4855 .7475 .6514 1.0000 .9420 .9189 .8945 1.02 1.000 .4286+09 .9281 1.8163 .8488 .4558 .7287 .6627 .9981 .9334 .9126 .8819 1.03	
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.450 .238E+09 .9301 1.8233 .9657 .8477 .9356 .9069 .7035 .9851 .9740 .9735 1.00 .500 .261E+09 .9299 1.8230 .9562 .6168 .9217 .8672 .7588 .9819 .9689 .9678 1.00 .550 .282E+09 .9297 1.8228 .9502 .7844 .9068 .5661 .8080 .9785 .9634 .9617 1.00 .660 .302E+09 .9296 1.8225 .9416 .7510 .8911 .8441 .8514 .9749 .9579 .9553 1.00 .650 .320E+09 .9294 1.8222 .9325 .7170 .8746 .8212 .8887 .9711 .9524 .9486 1.00 .700 .338E+09 .9292 1.8219 .9231 .6828 .8576 .7978 .9283 .9672 .9472 .9416 1.00 .750 .354E+09 .9290 1.8216 .9132 .6485 .8399 .7738 .9461 .9632 .9418 .9344 1.01 .800 .369E+09 .9288 1.8211 .9030 .6144 .8219 .7493 .9664 .9591 .9366 .9271 1.01 .800 .369E+09 .9287 1.8207 .8926 .5809 .8035 .7248 .9816 .9549 .9316 .9196 1.01 .900 .396E+09 .9287 1.8202 .8819 .5481 .7649 .7002 .9920 .9506 .9270 .9121 1.01 .950 .408E+09 .9283 1.8190 .8599 .4855 .7662 .6757 .9981 .9463 .9226 .9045 1.02 1.000 .419E+09 .9281 1.8190 .8599 .4855 .7475 .6514 1.000 .9420 .9189 .9186 .8890 1.02 1.050 .428E+09 .9280 1.8176 .8376 .4274 .7101 .6039 .9932 .9334 .9126 .8619 1.03	
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.550 .282E+09 .9297 1.8228 .9502 .7844 .9068 .9661 .8080 .9785 .9634 .9617 1.00 .600 .302E+09 .9296 1.8225 .9416 .7510 .8911 .8441 .8514 .9749 .9579 .9553 1.00 .650 .320E+09 .9294 1.8222 .9325 .7170 .8746 .8212 .8087 .9711 .9524 .9486 1.00 .700 .378E+09 .9297 1.8219 .9231 .6828 .0576 .7978 .9203 .9672 .9472 .9416 1.00 .750 .354E+09 .9290 1.8216 .9132 .6485 .8399 .7738 .9461 .9632 .9418 .9344 1.01 .800 .369E+09 .9288 1.8211 .9030 .6144 .8219 .7493 .9664 .9591 .9366 .9271 1.01 .850 .363E+09 .9287 1.8207 .8926 .5809 .8035 .7248 .9816 .9549 .9316 .9196 1.01 .900 .396E+09 .9275 1.8202 .8819 .5481 .7849 .7002 .9920 .9586 .9278 .9121 1.01 .950 .408E+09 .9283 1.8190 .8599 .4855 .7662 .6757 .9981 .9463 .9228 .9045 1.02 1.000 .419E+09 .9283 1.8190 .8599 .4855 .7475 .6514 1.0000 .9420 .9189 .8970 1.02 1.050 .428E+09 .9281 1.8183 .8488 .4558 .7287 .6274 .9983 .9377 .9156 .8894 1.03	
.690 .302E+09 .9296 1.8225 .9416 .7510 .8911 .8441 .8514 .9749 .9579 .9553 1.00 .650 .320E+09 .9294 1.8222 .9325 .7170 .8746 .8212 .8887 .9711 .9524 .9486 1.00 .780 .338E+09 .9297 1.8219 .9231 .6828 .8576 .7978 .9283 .9672 .9472 .9416 1.00 .750 .354E+09 .9290 1.8216 .9137 .6485 .8399 .7738 .9461 .9632 .9418 .9344 1.01 .800 .369E+09 .9288 1.8211 .9030 .6144 .8219 .7493 .9664 .9591 .9366 .9271 1.01 .850 .383E+09 .9287 1.8207 .8926 .5809 .8035 .7248 .9816 .9549 .9316 .9196 1.01 .900 .396E+09 .9275 1.8202 .8819 .5481 .7849 .7002 .9920 .9506 .9270 .9121 1.01 .950 .408E+09 .9234 1.8196 .8710 .5163 .7662 .6757 .9981 .9463 .9226 .9045 1.02 1.000 .419E+09 .9283 1.8190 .8599 .4855 .7475 .6514 1.8000 .9420 .9189 .8970 1.02 1.050 .428E+09 .9281 1.6183 .8488 .4558 .7287 .6274 .9983 .9377 .9156 .8894 1.03 1.100 .437E+09 .9280 1.8176 .8376 .4274 .7101 .6039 .9932 .9334 .9126 .8819 1.03	
.650	
.750 .354E+09 .9290 1.8216 .913? .6485 .8399 .7738 .9461 .9632 .9418 .9344 1.01 .800 .369E+09 .9288 1.8211 .9030 .6144 .8219 .7493 .9664 .9591 .9366 .9271 1.01 .850 .383E+09 .9287 1.8207 .8926 .5809 .8035 .7248 .9816 .9549 .9316 .9196 1.01 .900 .396E+09 .9285 1.8202 .8819 .5481 .7849 .7002 .9920 .9506 .9270 .9121 1.01 .950 .408E+09 .9284 1.8196 .8710 .5163 .7662 .6757 .9981 .9463 .9228 .9045 1.02 1.000 .419E+09 .9283 1.8190 .8599 .4855 .7475 .6514 1.8080 .9428 .9189 .8970 1.02 1.050 .428E+09 .9281 1.8183 .8488 .4558 .7287 .6274 .9983 .9377 .9156 .8894 1.03 1.100 .437E+09 .9280 1.8176 .8376 .4274 .7101 .6039 .9932 .9334 .9126 .8819 1.03	
.750 .354E+09 .9280 1.8216 .9132 .6485 .8399 .7738 .9461 .9632 .9418 .9344 1.01 .800 .369E+09 .9288 1.8211 .9030 .6144 .8219 .7493 .9664 .9591 .9366 .9271 1.01 .850 .383E+09 .9287 1.8207 .8926 .5809 .8035 .7248 .9816 .9549 .9316 .9196 1.01 .900 .396E+09 .9255 1.8202 .8819 .5481 .7849 .7002 .9920 .9506 .9270 .9121 1.01 .950 .408E+09 .9284 1.8196 .8710 .5163 .7662 .6757 .9981 .9463 .9226 .9045 1.02 1.000 .419E+09 .9283 1.8190 .8599 .4855 .7475 .6514 1.8000 .9420 .9189 .8970 1.02 1.050 .428E+09 .9281 1.6183 .8488 .4558 .7287 .6274 .9983 .9377 .9156 .8894 1.03 1.100 .437E+09 .9280 1.8176 .8376 .4274 .7101 .6039 .9932 .9334 .9126 .8819 1.03	
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.850 .3835+09 .9287 1.8207 .8926 .5809 .8035 .7248 .9816 .9549 .9316 .9196 1.01 .900 .3965+09 .9285 1.8202 .8819 .5481 .7849 .7002 .9920 .9506 .9270 .9121 1.01 .950 .4085+09 .9284 1.8196 .8710 .5163 .7662 .6757 .9981 .9463 .9226 .9045 1.02 1.000 .4195+09 .9283 1.8190 .8599 .4855 .7475 .6514 1.8000 .9428 .9189 .8970 1.02 1.050 .4285+09 .9281 1.8183 .8488 .4558 .7287 .6274 .9983 .9377 .9156 .8894 1.03 1.100 .4375+09 .9280 1.8176 .8376 .4274 .7101 .6039 .9932 .9334 .9126 .8819 1.03	
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1.100 .4375+09 .9280 1.8176 .8376 .4274 .7101 .6039 .9932 .9334 .9126 .8619 1.03	
1.160 AASELITA AAAA AAAA AAAA AAAA	
TARE TO THE STUDY OF THE STUDY	
1.280 1.452E+09 1.9279 1.8159 .8150 .3745 1.65733 .5580 .9743 1.9249 .9081 .8672 1.05	
1.250 .4585+09 .9278 1.8151 .8037 .3501 .6553 .5360 .9614 .9207 .9068 .8601 1.05	
1.300 .4635+09 .9778 1.8142 .7924 .3270 .6375 .5146 .9464 .9166 .9859 .26538 .1.06	
1.3504685+099278 1.613376133051620149389298917690566661 1.07	
1.400 44725+09 9278 1.8124 .7781 .2846	
1.475 +475E+U9 -49277 1.8116 -7591 -2653 -58637 -4542 -8924 -9046 -9064 -8328 1.09	1, -, -
1.500 .4785.09 .9277 1.8105 .7482 .2472 .5699 .4353 .8722 .9810 .9076 .6264 1.10	
1.550 .480E+09 .9277 1.8101 .7374 .2303 .5540 .4173 .8514 .8973 .9095 .8201 1.11	,

SATURATION BOUNDARY REACHED.

TABLE II. PEAL-GAS ISENTROPIC EXPANSIONS OF PARAHYDROGEN

B. (CONTINUED)

MACH	LOCAL ISENTROPIC	VISCOSITY	THERMAL CONDUCTIVITY	PRANDIL
	EXPANSION COEFF.	G/CH-SEC	CAL/CH-SEC-K	NUMBER
0.000		.18949E-04	.68541E-N4	.7620
• 850	1.6895	.18934E-84	-68483E-94	.7620
.100	1.7153	.18891E-04	.68314E-04	.7621
• 150	1,6882	.18618E-84	.68030E-04	.7624
. 200	1.6879	.18718E-04	.67637E-04	.7627
.250	1.6922	-1859RE-04	.67136E-04	.7631
. 300	1.6874	.18437E-84	.66537E-04	.7636
• 3 50	1.6902	.18258E-04	-65842E-04	.7641
• 40 G	1.6976	.16057E-04	.65080E-04	.7646
•450	1.6868	.17833E-84	.64236E-84	.7650
•50 0	1.6556	.17590E-04	.63318E-04	.7653
₹550	1.6857	.17328E-04	.62367E-04	.7653
• 500	1.6873	.17949E-04	.61349E-04	.7653
•650	1.6864	.16756E-04	•60267E-04	.7655
.700	1.6904	-16450E-84	.59130E-04	.7659
.751	1.6846	.16132E-8+	-57938E-04	.7664
.509	1.6822	.15806E-04	.56703E-04	.7670
. 550	1.6828	.15471E-04	.55438E-04	.7679
- 900	1.6817	.15130E-04	.54127E-04	.7689
• 950	1.6830	-14786E-84	.52601E-04	.7701
1.000	1.6795	.14437E-84	.51457E-04	.7716
1 - 050	1.6810	.14887E-04	.50130E-04	.7728
1.100	1.6790	-13737E-04	.48861E-04	.7732
1.150	1.6752	.13386E-84	.47594E-04	.7737
1.209	1.6763	.13038E-04	.46329E-04	.7744
1.250	1.6773	.12692E-84	.45871E-04	.7753
1.300	1.6747	.12349E-04	.43823E-04	.7763
1.350	1.6733	.12011E-04	.42588E-04	.7776
1.480	1.6684	.11676E-84	.41370E-84	.7790
1.450	1.6724	.11348E-04	.48172E-04	.7806
1.580	1.6676	.11025E-04	-39021E-04	.7819
1.550	1.6702	-10708E-04	.38143E-04	.7783



TAPLE II. PEAL-GAS ISENTROPIC EXPANSIONS OF PARAHYDROGEN

		C. TT	= 40.00	< PT =	3.N ATM	PHOT =	.193E-02	G/CH3	SVT = 515	.384 H/S	EC		
MACH	RE/M	Z	CP/CV	SV/SVT	P/PT	T/TT	RHOZRHOT	A*/A	SV/SVT	P/PT	1/11	RHO/RHOT	A*/A
										RELATIVE		GAS VALUES	
0.000	0.	.9528	1.7759	1.0000	1.0000	1.0000	1.0000	0.6000	1.5000	1.0000	1.0000	1.0000	1.0900
.050	.236E+88	• 9528	1.7759	• 9996	9979	.999?	.9987	.0896	.9998	- 9996	.9997	1.0000	1.0323
.100	.470E+08	• 9527	1.7759	.9982	.9917	.9966	.9951	-1772	9992	9967	9986	1.0001	1,0318
.150	.701E+08	.9527	1.7758	. 9960	.9813	9924	.9889	.2636		9968	9969	1.0001	1.0308
.200	• 92 9E+08	.9526	1.7758	.9930	• 9670	.9866	.9883	.3474	.9970	.9943	. 9945	1.0000	1.0294
.250	·115E+09	. 9525	1.7757	.9891	9491	. 97 92	.9695	.4277	.9953	.9912	9915	1.0001	1.0277
.300	.137E+09	- 9524	1.7756	. 9845	.9279	.9784	.9567	.5041	9933	.9877	9878	1.0003	1.0259
.350	.158E+09	.9522	1.7754	. 9791	• 9037	.9601	-9418	.5758	+9910	9836	. 9836	1.0005	1.0237
.400	.178E+09	• 95 21	1.7752	.9729	¥8768	. • 9485	.9251	.6423	.9884	9790	.9789	1.0009	1.0214
.450	•197E+09	•9519	1.7750	9661	.8478	.9358	•9069	.7034	.9855	.9742	9736	1.0015	1.0190
.500	.215E+09	.9517	1.7748	9586	•8169	.9219	.8371	.7587	.9623	. 96 91	. 9680	1.0022	1.0165
.550	.233E+09	.9516	1,7745	.9506	.7645	.9070	.8661	.8879	.9789	. 9636	9519	1.0031	1.0138
600	.249£+09	. 9514	1.7742	.9421	.7513	+8913	.8442	.0513	. 9754	. 9583	9555	1.8044	1.0116
-650	.264E+59	.9512	1.7738	.9330	.7173	6749	.8213	.8886	9717	. 9529	. 94 88	1.0059	1.0092
.700	.279E+09	. 9518	1.7734	.9236	-6830	.8578	•7977	9201	.9678	.9474	9419	1.0077	1.0069
.750	.292E+09	.9508	1.7730	.9137	.6487	.8482	.7736	.9459	.9638	9420	9347	1.0099	1.0049
. 890	.384E+89	.9507	1.7727	.9035	.6147	.6222	.7492	9663	9597	9369	9274	1.0125	1.0033
. 550	.315E+09	• 95 05	1.7723	.8932	.5811	.8839	.7247	.9816	.955€	. 9320	.9200	1.0155	1.0019
.900	.326E+D9	.9503	1.7720	.8326	-5483	.7853	.7000	.9920	.9514	9273	.9125	1.0186	1.0808
•95 C	•335E+119	9502	1.7716	.6718	.5164	.7666	-6754	.9988	.9472	.9230	9049	1.0227	1.0002
. 1.000	.343E+R9	. 95 00	1.7713	.860A	4855	.7478	.6511	1.0000	.9429	• 91 91	.8974	1.0271	1.0000
1.050	.351E+09	, 9499	1.7759	-8497	• 4558	.7290	.6271	-9982	.9387	•9156	. 6896	1.0321	1.0003
1.100	.358E+09	.9495	1.7704	.8385	.4274	.7184	- 69 35	.9931	.9345	. 91 25	.8823	1.0374	1.0010
1.150	.364F+09	. 94 97	1.7700	.8273	.4002	.6918	-5893	9850	9303	90 99	. 6748	1.0434	1.0022
1.200	.369E+09	.9496	1.7695	8160	. 7743	.6735	.5576	9742	9261	.9077	.8674	1.0499	1.0039
1.250	.374E+09	• 94 95	1.7690	.8848	.3498	. 6554	-5356	9613	-9220	9861	. 86 02	1.0570	1.0062
1.300	.378E+09	.9495	1.7685	.7936	. 3266	.6375	-5141	.9462	.9179	9050	. 8530	1.0646	1.0090
1.350	.381E+09	.9495	1.7679	.7824	.3047	.6200	.4932	9295	.9139	.9844	.8460	1.0727	1.0122
1.400	.364E+09	.9494	1.7673	.7713	.2842	.6028	4730	9113	9100	9043	. 83 91	1.0614	1.0161
1.450	.387E+09	. 9494	1.7568	.7603	.2649	.5860	4536	. 8922	9062	9849	.8324	1.0909	1.0206
1.500	·389E+09	. 9494	1.7662	7494	.2468	.5696	-4348	8720	.9024	.9859	.8259	1.1008	1.0256
1.551	.390E+09	.9494	1.7656	.7386	.2298	.5535	-4166	.6511	. 8987	.9874	8195	1.1112	1.0311
1.600	.392E+09	.9494	1.7650	.7280	.2140	.5379	. 1992	8297	. 8951	9095	. 61 33	1.1223	1.0373
1.650	.393E+09	.9494	1.7644	7175	.1992	.522€	.3625	.8079	8916	9122	.8072	1.1348	1.0440
1.700	.393E+09	.9495	1.7638	.7071	.1855	-5078	3665	7860	.8882	9154	.8014	1.1464	1.0513
1.750	.3935+09	9495	1.7633	6969	.1726	.4934	-3510	7634	.8849	9190	.7956	1.1590	1.0590
1.800	.393E+89	9495	1.7628	.6868	-1607	4794	.3363	.7418	.8817	9233	.7901	1.1725	1.0674
1.850	-397E+09	•9496	1.7623	.6769	.1496	4659	.32??	.7198	.8786	.9279	.7848	1.1865	1.0763
1.900	.3935+09	. 94 96	1.7620	.6672	.1393	4527	3087	6981	.6755	.9332	.7796	1.2010	1.0857
1.950	.392E+09	•9496	1.7616	6576	-1297	-44 Off	2958	-6767	8726	.9389	.7746	1.2162	1.0957

C. (CONTINUED)

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MACH	LOCAL ISENTROPIC	VISCOSITY	THERMAL CONDUCTIVITY	PRANDTL
	EXPANSION COEFF.	G/CM-SEC	CAL/CH-SEC-K	NUMBER
		04475	767707 64	7704
0.000	I	.21135E-04	.76359E-114	.7381
.050	1.6841	.71119E-04	.76296E-04	.7382
.100	1.7097	.21072E-04	.76109E-04	.7383 .7386
.150	1.6833	.28995E-84	.75797E-04	
. 200	1.6834	.20867E-04	.75365E-04	.7389 .7393
• 250	1.6877	.20750E-04	.74817E-04	
.300	1.6925	.28585E-84	.74159E-04	.7399
• 350	1.6871	.20393E-04	.73397E-04	.7405
. 400	1.6873	-20176E-04	.72560E-04	.7489
•450	1.6908	.19936E-84	.71638E-84	-7414
.500	1.6857	.19674E-04	.70633E-04	.7419
.550	1.6831	•19392E-04	.69555E-04	.7424
.600	1.6901	•19092E-04	.68414E-04	.7438
.650	1.6839	.18776E-84	.67215E-04	.7436
.700	1.6830	.18446E-84	.65966E-84	.7443
.750	1.6823	.18103E-04	.64678E-84	.7449
. 600	1.6833	.17751E-04	.63356E-04	.7455
.850	1.6821	.17389E-84	.62003E-04	.7460
. 900	1.6785	.17920E-84	.60623E-04	.7466
. 950	1.6806	.16545E=84	.59208E-04	.7474
1.000	1.6896	.16267E- 8 4	.57769E-84	.7484
1.050	1.6797	.15886E-04	.56314E-04	.7496
1.100	1.6778	.15584E-84	•54896E-04	.7502
1.150	1.6762	.15127E-04	.53487E-84	.7588
1,200	1.6761	.14741E-04	.52089E-04	.7514
1.250	1.6775	.14363E-04	.50706E+04	.7519
1.300	1.6752	.13987E-04	.49341E-04	.7523
1.350	1.6735	.13615E-04	.47987E-04	.7529
1.400	1.6733	.13247E-84	.46649E-04	.7535
1.450	1.6749	-12885E-04	.45330E-04	.7542
1.500	1.6727	.12528E-04	.44831E-84	.7550
1.550	1.6704	.12178E-04	.42756E+04	.7559
1.698	1.6713	-11834E-84	-41507E-04	.7568
1.650	1.6709	.11497E-84	.40286E-04	.7578
1.700	1.6715	.11167E-04	.39894E-04	.7589
1.750	1.6667	10845E-04	.38877E-04	.7570
1.800	1.6701	.1053RE-04	.37265E-04	.7516
1.850	1.6677	.10222E-04	.36488E-84	.7458
1.900	1.6680	.99226E-05	.35745E+04	.7397
1.950	1.6682	.96307E-05	.35033E-04	.7333
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TABLE II. REAL-GAS ISENTROPIC EXPANSIONS OF PARAHYDROGEN

TT: = 60.0 K PT = 3.0 ATM RHOT = .125E-02 G/CH3 SVT = 634.987 M/SEC . 2 MACH RE/M CP/CV SV/SVT P/PT T/TT RHO/RHOT A+/A SV/SVT P/PT T/TT RHO/RHOT AT/A -----PELATIVE TO IDEAL GAS VALUES-----0.000 .9864 1.6746 1.0000 1.0000 1,5600 1.0000 0.0000 1.0000 1.0000 1.0000 1.0000 1.0000 .050 .136E+08 1.6748 .9979 .9854 .9996 .9992 .9987 .0883 .9999 . 9996 . 9997 .9999 1.0239 .100 .9863 1.6752 .271E+08 .9985 .9917 .9968 •9949 .1758 . 9995 .9987 . 9988 .9999 1.0235 .150 .404E+08 1.6760 •9563 .9967 9516 .9928 .9888 .2616 .9989 .997? .9973 1.0000 1.0230 .201 .5365+06 1.6770 .9862 . 9941 .9676 .9872 .9803 .3449 .9981 . 9950 . 9951 1.0000 1.0221 .250 .664E+08 1.6783 .9861 .9909 .9500 • 96 95 .9802 . 4258 .9978 . 9923 . 9924 1.0000 1.8211 .300 .768E+08 .9860 1.6797 .9292 9169 .9717 •9566 .5012 .9957 . 9891 9892 1.0002 1.0200 .350 .908E+08 .9859 1.6814 .9822 .9053 .9618 .9417 .5729 .9942 • 9853 . 9854 1.0094 1.0186 .400 .102E+09 .9858 1.6837 .9769 .8786 .9506 .9248 .6395 .9924 .9810 .9810 1.0086 1.8169 .459 .113E+09 .9857 1.6850 .97119 .8498 .9382 .9864 .7006 .9903 .9765 . 9762 1.0010 1.0152 .500 .124F+09 .9855 1.6869 .9642 .8190 .9246 . 5566 .7564 .9880 .9716 .9709 1.0016 1.0134 **.**550 .134E+09 .9854 1.6888 .9570 .7867 .9101 .8653 .8069 .9855 **.**9662 .9651 1.0021 1.0114 .600 .143E+09 .9852 1.6907 .9492 .7533 .8946 . 64 10 .8496 .9828 .9608 .9590 1.0031 1.0095 -650 .151E+119 .9850 1.6925 .9489 .7193 .8783 .8201 .8874 .9798 . 9554 . 9526 1.0044 1.0878 .700 .159E+09 1.6941 .9849 .9320 .6848 .8614 .7962 +9192 .9766 . 94 99 .9458 1.0058 1.0060 .75 B .167E+89 .9847 1.6957 .9227 .6583 .8439 .7719 . 9454 .9733 .9444 1.0077 . 9388 1.0044 .800 ·173E+09 .9845 1.6970 .9130 .6161 .8259 .7474 .9661 9697 .9392 .9316 1.0190 1.0030 . 85 D .179E+09 .9844 1.698? .9030 .5823 .0075 .7225 .9814 .9339 .9661 .9242 1.0125 1.0017 .900 .185E+09 .9842 1.6992 .8927 .5492 .6977 .7889 . 9919 .9623 .9289 .9167 1.0155 1.0007 .950 .1985+09 .9840 1.7001 .5172 .8821 .7702 .6731 .9981 ,9584 . 9244 .9092 1.0191 1.0003 1.000 .194E+09 .9839 1.7008 .8712 .4861 .7514 .6436 1.0000 .9016 .9544 .9201 1.0231 1.0000 1.050 +198E+89 .9437 1.7013 . 4562 .8603 .7325 .6245 .9982 .9504 1,0903 . 9164 . 8941 1.0277 1.100 .2015+09 .9876 1.7017 .8492 .4276 .7136 .5008 .9930 .9463 .9130 . 88 65 1.0328 1.0009 1.150 .204E+09 .9835 1.7020 .8380 .4003 .6952 .5776 . 9850 .9423 .9102 .8790 1.0385 1.0022 1.200 .206E+09 .9833 1.7021 .8267 .3743 .6767 .5548 .9740 .9382 .9077 .8716 1.0446 1.0036 1.250 .209E+09 .9832 1.7022 .8154 .3497 .6585 .5326 .9610 .9342 .9059 .6643 1.0515 1.0059 1.300 ·217E+09 .9831 1.7822 .8042 .3265 .6466 .5113 .9459 .9302 . 9045 .8572 1.0588 1.0186 1.350 .212E+D9 1.7022 .9830 .7929 .3045 .6230 .4905 .9291 • 9263 .9037 .8501 1.0667 1.6119 1.400 .2135+09 .9829 1.7821 .7515 .2839 .6057 .4703 .9110 .9224 .9035 . 6432 1.0753 1.0157 1.450 .2135+09 .9828 1.7819 .7707 .2645 .5888 .4509 .8917 .9185 .9038 . 8364 1.0843 1.0200 1.500 -2145+09 .9828 1.7018 .7597 . 2464 .5723 .4321 .8714 .9148 .9846 . 8298 1.8940 1.0249 1.550 ·214E+09 .9827 1.7016 .7488 .2794 .5562 .4141 .9111 . 8505 .9059 .8234 1.1044 1.0305 1.600 .214E+09 1.7014 . 9826 .7361 .2136 .5404 .3967 .8290 .9075 .9078 . 6171 1.1152 1.6364 1.650 .214E+09 .9826 1.7013 .7274 .1988 .5251 .3801 .6073 .9040 .9103 .8110 1.1268 1.0432 1.700 .2145+09 .9825 1.7011 .7169 .1850 .5102 .3640 .7851 .9006 .9130 .8050 1.1366 1.0501 1.750 .2136+09 .9375 1.7009 .71166 .172? .4957 .3487 .7631 .8973 .9166 .7993 1.1513 1,0580 1.800 .213E+09 .9825 1.7707 .6964 .1602 .4615 .3340 .7409 .8941 .9205 .7936 1-1644 1.0661 1.850 .212E+09 .9824 1.7095 .6864 .1491 .4679 .3199 .7189 .8909 .9249 1.0749 .7882 1.1781 1.900 .211E+09 .9824 1.7003 .6766 .1388 .4546 .3865 .6973 .8876 .9300 .7829 1.1927 1.0845 1.950 .21 NE+09 .9824 1.7991 .6669 .1292 .4418 .2936 •6757 .8849 . 9354 .7778 1.2075 1.0942 2.000 .2092+09 .9824 1.6999 .6574 .1203 .4293 .2814 . 6547 .8620 . 9415 .7728 1.2232 1.1048

D. (CONTINUED)

MACH	LOCAL ISENTROPIC	VISCOSITY	THERNAL CONDUCTIVITY	PRANDTL
TI.RQII	E PANSION COEFF.	G/CH-SEC	CAL/CH-SEC-K	NUMBER
•	2 1 111022011 0021 1	41 411 524		
0.000	I	.29071E-84	.11020E-03	.6885
.050	1.6234	.29052E-84	.11011E-03	.6885
.100	1.6467	.28997E-04	.10984E-03	.6886
. 150	1.6585	.28905E-04	.10940E-03	.6887
. 200	1.6520	.28776E-04	.10879E-03	.6888
. 250	1.6546	.28613E-04	.10801E-03	.6890
.300	1.6601	.28415E-84	.10706E-03	.6892
.350	1.6575	.28184E-84	.10597E-03	.6896
.400	1.6547	.27922E-04	.10472E-03	.6901
.450	1.6629	.27629E-#4	.18334E-03	.6907
-500	1.6626	.27309E-04	•10099E-03	.6972
.550	1.6592	.26962E-#4	.99487E-84	.6975
.600	1.6650	.26591E-84	.97885E-04	•6979
.65D	1.6693	.26199E-04	.96200E-04	.6983
.700	1.6667	.25787E-04	.94455E-04	.6989
.750	1.6697	.25358E-04	.92647E-74	.6995
.800	1.6727	.24914E-14	.98796E-04	.7003
.850	1.6678	.24457E-04	.88912E+04	.7011
.900	1.6714	.23990E-04	.86998E+04	.7020
• 950	1.6745	.23515E-84	.85020E+04	.7033
1.000	1.6718	.23834E-84	.83029E-84	.7048
1.050	1.6742	.22548E-04	.80774E-04	.7086
1.100	1.6727	.22059E-04	.78828E-04	.7099
1.150	1.6758	.21569E-04	.76897E-N4	.7112
1.200	1.6705	.21089E-04	.74984E-04	.7124
1.250	1.6754	.20591E-04	.73097E-04	.7136
1.300	1.6727	.20106E-04	.71239E-04	.7147
1.350	1.6731	.19624E-84	.69413E-04	.7157
1.400	1.6731	.19146E-04	.67620E-04	.7166
1.450	1.6721	.18674E-84	.65864E-84	.7174
1.500	1.6720	.18208E-84	.64147E-04	.7161
1.550	1.6724	.17748E-04	.62469E-04	.7186
1.600	1.6709	.17295E-04	-60833E-114	.7190
1.650	1.6735	.16851E-04	.59171E-04	.7200
1.700	1.6677	.16413E-04	.57531E-04	.7212
1.750	1.6729	.15985E-84	.55934E-84	.7223
1.800	1.6686	.15564E+04	.54382E-04	.7232
1.650	1.6798	.15153E-84	.52872E-04	.7241
1.900	1.6729	.14750E-84	.51406E-04	.7248
1.950	1.6676	.14356E-84	.49983E-04	.7254
2.000	1.6727	.13972E-04	.48560E-04	.7263
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OF MOOR QUALITY

TABLE II. REAL+GAS ISENTROPIC EXPANSIONS OF PARAHYDROGEN

		E. T1	r = 80.0 K	PT =	.3.0 ATH	RHOT =	.925E-03	G/CM3	SVT = 714	.525 M/S	C		
MACH	PE/H	?	CP/CV	SV/SVT	F/PT	IVII	RHOZRHOT	A*/A	SV/SVT	P/PT	T/TT	RHO/RHOT	A+/A
	•					e de la companya de					10 TOTAL	AND AMERIC	,
0.800	0.	.9957	1.5608	1.0000	1.0000	1.0000	1.0000	0.0000	1.0000	1.0000	1.0000	1.0000	1.0000
•050	·917E+07	9957	1.5611	. 9997	• 9980	.9993	.9987	.0868	1.0000	.9998	. 1998	1.0000	1.0059
.100	·1835+08	9956	1.5619	9990	•9923	.9973	•9951	.1728	1.0000	. 9993	• 9993	1.0001	1.0059
.150	.273E+08	9956	1.5634	9977	9826	-9938	9887	.2572	.9999	. 9981	• 9983	. 9999	1.0057
.200	.361E+88	• 9956	1.5655	.9959	• 9696	9891	9804	. 3394	.9999	.9970	.9970	1.6001	1.0059
.250	.448E+08	9955	1.5681	• 9936	• 9528	•9830	•9694	•4186	. 9998	• 9951	• 9953	1.0000	1.0057
.300	.531E+08	.9954	1.5713	9908	9328	• 9756	.9563	• 4941	.9997	.9929	• 993 <i>?</i>	1.0000	1.0955
.350	.612E+08	.9954	1.5750	• 9875	9100	•9669	9414	•5655	• 9995	•9905	• 9906	1.0001	1.0055
-486	•690E+08	.9953	1.5792	9836	. 8843	.9570	.9243	.6322	•9993	. 9874	.9877	1.0001	1.0052
.450	•764E+08	. 9952	1.5839	9793	8563	•9460	.9057	.6937	.9989	• 9840	• 9843	1.0305	1.0050
-500	.834E+08	.9951	1.5890	-9744	.8262	.9338	.8853	.7498	.9985	- 98 91	. 9805	1.8002	1.0045
•550	.899E+08	9950	1.5945	•9690	.7945	•9205	.8637	.8001	•9979	.9758	.9762	1.0003	1.0041
-600	.961E+08	.9948	1.6003	.9631	.7614	•9762	.5409	. 8447	•9972	.9712	.9715	1.0006	1.8836
.651	.102E+09	.9947	1.6764	.9567	.7274	.8910	.8172	.8833	.9963	• 9663.	. 9563	1.0009	1.0031
•700	.1075+09	9946	1.6127	• 9+98	•6929	.8750	.7928	•9162	•9952	•9612	.9607	1.0015	1.0026
.750	•112E+09	9945	1.6190	+9423	.6581	.8582	.7678	9432	9939	.9558	.9548	1.0023	1.0020
.800	·116E+09	.9943	1.6253	. 9344	.6233	-8408	.7423	• 9645	.9924	•9501	. 9464	1.0031	1.0014
•850	.1205+09	.9942	1.6316	.9261	•588B	.8228	.7165	.9805	.9987	.9443	.9417	1.0042	1.0007
.900	.1245+09	.9941	1.6376	.9172	• 5 5 5 0	.6044	-6911	.9915	.9887	-9387	. 9347	1.0059	1.0003
95 0	.127E+09	.9939	1.6434	.9079	•5221	.7857	•6656	• 9979	-9865	.9332	.9275	1.9678	1.0000
1.000	.129F+09	9938	1.6488	.8983	-4902	-7668	-6405	1.6000	-9640	.9279	. 9201	1.0103	1.0000
1.050	.132E+09	.9937	1.6538	.5883	•4594	•7477	6157	•9961	.9813	.9228	.9126	1.0132	1.0081
1.100	.1345+09	9975	1.6584	.6780	• 4300	.7286	•5914	.9927	.9784	.9180	.9050	1.0166	1.0006
1.150	.135E+09	.9934	1.6625	.8674	•4019	•7096	•5676	. 9842	•9754	9138	• 897 3	1.0207	1.8614
1.200	.137E+09	.9933	1.6662	.8566	.3753	6907	-5446	. 9731	9722	• 91 0 1	. 8897	1.0254	1.0027
1.250	+138E+09	• 9932	1.6693	. 6456	.3501	.6721	•52?2	• 3594	•9688	.9068	.8821	1.0396	1.0043
1.300	•139E+09	.9931	1.672	.8346	.3264	.6576	.5006	. 9441	.9654	, 90 43	. 8746	1.0367	1.0067
1.350	.139E+89	.9930	1.6743	.8234	.3041	.6355	.4798	.9270	-9618	.9824	. 6672	1.0434	1.0095
1.400	·140E+09	9929	1.6762	.8122	.2832	•617R	•4597	.9085	.9583	.9011	.8600	1.0508	1.0129
1.450	•148£+09	-9928	1.6778	• 8 010	.2636	.6004	•4483	8888	.9547	.9004	.8529	1.0588	1.0167
1.500	•140E+09	.9927	1.6790	•7898	. 2453	•5835	•4216	.8682	.9511	. 9004	.8460	1.0674	1.0212
1.550	.140E+09	. 9926	1.6807	.7787	.2282	•5669	-4036	.6472	.9475	.9811	.6393	1.0770	1.0264
1.600	•1405+89	. 9925	1.6807	• 7677	.2123	•5508	*3867	. 8255	9439	. 9024	. 8328	1.0870	1.0321
1.650	.139E+89	.9925	1.6813	• 7567	.1975	.5351	.3703	.8036	.9484	.9843	. 8265	1.0978	1.0385
1.700	.139E+09	.9924	1.6817	.7459	-1637	-5198	.3546	.7815	.9378	.9068	.8203	1.1091	1.0453
1.750	•138E+09	.9923	1.6820	.7352	.1709	.5050	.3395	.7593	. 9336	90 99	. 81 44	1.1210	1.0520
1.800	.138E+89	.9923	1.6822	.7247	.1590	.4907	.3252	.7373	.9303	-9137	. 80 86	1.1336	1.0610
1.850	.137E+09	.9922	1.6823	.7143	.1488	+4767	.3114	.7153	.9271	9179	.8030	1.1470	1.0696
1.900	.1365+09	.9922	1.6824	.7041	.1377	.4632	.2983	.6937	.9239	.9227	.7976	1.1609	1.0789
1.950	.135E+09	.9922	1.6824	•6941	.1282	.4501	.2858	.6722	.9209	.9278	.7924	1.1751	1.0685
2.000	.134E+89	.9971	1.6824	.6841	•1193	.4374	.2738	.6511	.9179	. 9336	.7873	1.1900	1.0987

E. (CONTINUED)

MACH	LOCAL ISENTROPIC EXPANSION COEFF.	VISCOSITY G/CM-SEC	THERNAL CONDUCTIVITY CAL/CH-SEC-K	PRANDTL NU MB ER
0.000	Ţ	.36024E-04	.14648E-03	.6980
.050	1.5471	-36006E-84	.14635E-03	.6980
.100	1,5699	.35950E-04	.14597E-03	.6980
.150	1.5390	.35857E-04	.14533E-03	.6981
. 208	1.5708	.35728E-94	-14445E-03	.6981
. 250	1.5563	.35563E-04	.14331E-03	.6982
.300	1.5594	.35361E-84	.14194E-03	-6984
.350	1.5715	.35124E-04	.14052E-03	.6978
.400	1.5671	.34653E-04	•13903E-03	.6964
.450	1.5745	.34547E-04	.13737E-03	.6958
.500	1.5769	. \$4209E-04	.13553E-03	.6935
.550	1.5833	.33840E-84	.13354E-03	.6921
-600	1.5896	.33440E-64	.13139E-03	.6907
.6:0	1.5944	.33011E-04	.12910E-03	.6894
.700	1.6037	.32556E-04	•12668E-03	.6883
.750	1.6079	.32076E-04	.12415E-03	.6874
.600	1.6122	.31574E-04	•12152E-03	-6868
.850	1.6173	.31852E-84	.11888E-03	.685û
.900	1.6263	.30513E-84	.11622E-03	-6853
• 950	1.6311	.29959E-64	.11352E-03	.6858
1.000	1.6372	.29393E-84	.11077E-03	.6850
1.050	1.6488	.28817E-84	.10000E-03	.6854
1.100	1.6450	.28235E-04	.10523E-03	-6862
1.150	1.6493	.27649E-84	.17246E-03	.6874
1.200	1.6540	.27861E-84	.99325E-04	-6916
1.250	1.6543	.26474E-04	.96793E-04	•6921
1.300	1.6616	.25888E-04	.94298E-04	.6929
1.350	1.6519	.25305E-04	•91850E-04	.6938
1.400	1.6635	.24728E-84	.89458E-84	•6949
1.450	1.6633	• 2415 €E-04	.87102E-04	.6960
1.500	1.6650	• 23592E- 8 4	.84790E-04	.6974
1.550	1.6685	. 23035E-04	.82513E-04	•6 990
1.680	1.6678	•22486E-04	.80172E-04	.7016
1.659	1.6665	.21946E-04	.78040E-04	.7030
1.700	1.6678	• 21416E-04	•75966E-04	.7044
1.750	1.6665	• 20895E-84	•73953E-04	.7056
1.800	1.6714	.20384E-04	.71995E-04	.7068
1.850	1.668₹	·19882E-04	.70101E-04	.7079
1.900	1.6703	.19392E-04	.68256E-84	.7089
1.950	1.6671	-18911E-04	-66468E-04	.7098
2.000	1.6679	-1644DE-04	-64734E-04	.7196

DRUGINAL PAGE L

ORIGINAL PAGE IS
OF POOR QUALITY TABLE II.

TABLE II. REAL-GAS ISENTROPIC EXPANSIONS OF PARAHYDROGEN

		F. IT	= 100.0	K PT =	3.0 ATM	RHOT =	.738E-03	G/CM3	SVT = 773	711 H/S	EC		
MACH	RE/M	Z	CP/CV	SV/SVT	P/FT	T/TI	RHOZRHOT	A*/A	SV/SVT	P/PT	1/11	RHO/RHGT	ATZA
- 1												GAS VALUES	ntan: Seereesis
											TO: TOURE	OND TAROE.	7 37 8
0.000	0.	. 9992	1.4538	1.0000	1.0000	1.0000	1.0000	0.0000	1.0900	1.0000	1.0000	1.0900	1.0000
•050	•6745+07	. 9992	1.4540	.9994	9982	9994	- 9988	.0857	1.0000	1.0000	. 9999	1.0000	9940
-100	.1345+86	.9992	1.4547	9992	. 9927	.9978	.9949	.1707	1.0802	.9996	9998	•9999	9940
•150	.200E+08	9992	1.4559	.998?	.9879	.99511	.9889	.2543		9995	9994	1.0001	9944
.200	.2655+08	. 9991	1.4575	.9967	.9715	.9911	.9804	.3357	1.0007	. 9998	9990	1.0001	9947
•250	•3295+08	.9991	1.4596	9949	9557	-9861	.9694	-4141	1.0011	.9982	. 9984	.9999	9950
•300	.390E+08	.9990	1.4622	9926	.9370	.9800	•9563	. 4891	1.0015	. 9974	9976	1.0000	9954
-350	•449E+D8	•9990	1.4653	.9900	• 9154	.9728	.9412	.5691	1.0021	.9963	9967	.9999	.9959
•480	.5055+08	.9989	1.4690	.9870	.8911	•9646	. 9241	6266	1.0026	.9950	.9955	.9998	.9964
•45 D	•559F+0B	.9988	1.4731	. 9836	. 8646	.9554	•9053	.6852	1.0033	. 9935	9941	9998	.9970
•500	•609E+08	.9987	1.4778	9798	8358	.9452	.8847	.7444	1.0040	9914	9924	9994	.9973
•55 D	.657E+BR	.9987	1.4830	.9756	.8055	.9340	+8629	.7953	1.0047	9894	9905	9994	9980
•600	.7005+08	• 9986	1.4668	9719	·7736	.9219	.8397	.8403		. 9868	. 9882	9992	. 9984
•650	.741E+08	.998=	1.4952	.9661	.7486	.9088	-8155	.8796	1.0061	-9838	9856	9988	9988
-700	•778E+08	.9974	1.5021	.9508	.7068	.8949	. 7904	.9130	1.0068	9804	9526	.9985	9992
.750	.811E+08	.9983	1.5096	.9552	.6724	-8502	.7646	. 9408	1.0074	. 9765	. 97 93	.9982	. 9995
.800	.841E+08	.9982	1.5176	. 9491	· 6379	.8547	.7*85	.9630	1.0080	.9724	9754	. 9979	. 9999
. 850	.868E+08	9981	1.5761	.9427	.6073	.8485	.7118	.9797	1.0085	9677	9712	.9975	9999
.900	.891E+08	.9980	1.5351	.9359	•5691	.6317	•6551	.9912	1.0989	-9625	9664	9972	1.0000
• 950	.912E+08	.9979	1.5444	. 9288	-5355	-8143	•6585	. 9980	1.0091	9572	.9512	. 9971	1.0001
1.000	.929E+08	.9974	1 • 5540	.9213	.5025	.7953	-6328	1.0000	1.0092	.9513	9556	9969	1.0000
1.050	.943E+08	• 9977	1.5639	. 91 34	•4706	.7780	-6059	.9980	1.0091	9453	94.95	.9971	1.0001
1.100	•955E+08	.9976	1.5734	.9051	. 4399	.7593	.5803	.9923	1.0087	.9392	-9430	.9976	1.0002
1.150	.965E+08	.9975	1.5837	8965	• 4104	.7493	•5552	.9631	1.0081	9330	. 9362	.9983	1.0803
1.200	-972E+08	9974	1.5934	.8875	.3823	.7213	.5310	.9712	1.0072	9270	• 92 90	9997	1.0006
1.250	.977E+118	.9973	1.6028	.8781	.3556	.7022	-5074	9566	1.0060	9211	.9216	1.0014	1.0013
1.300	.980E+08	.9972	1.6117	.8685	.3305	.6831	-4847	9399	1.0046	9156	. 9140	1.0038	1.0022
1.350	.982E+08	.9971	1.6201	+8585	.3068	+6642	•4629	.9215	1.0029	9105	-9864	1.0067	1.0035
1.400	.982E+08	.9971	1.6279	.8483	-2847	.6456	.4420	.9017		9061	.8986	1.0105	1.0053
1.450	.981E+08	.9969	1.6350	.8379	-2641	.6277	.4221	.8808	.9987	9024	.8919	1.0151	1.0076
1.500	.979E+08	•9968	1.6414	. 8274	.2449	.6092	. 4030	.8591	.9963	8992	-8834	1.0203	1.0104
1.550	.976E+08	.9968	1.6470	.8167	-2272	.5916	.3849	.8368	.9937	8969	.8759	1.0265	1.0139
1.600	•972E+08	•9967	1.6519	8059	-2107	.5745	.3677	.8143	9909	.8955	.8686	1.0336	1.0180
1.650	. 967E+08	.9966	1.6562	.7951	•1955	.5578	•3513	.7916	.9881	.8950	.8615	1.0416	1.0230
1.700	.962E+08	•9966	1.6598	. 7842	•1814	.5416	.3356	.7690	.9851	. 8954	. 8546	1.0504	1.0286
1.750	.9562+88	9965	1.6628	.7734	.1684	•5259	.3210	.7463	.9821	.8964	.8480	1.0600	1.0348
1.800	+9495+08	• 9964	1.6653	•7627	•1563	•5107	.3070	.7238	•9791	.8983	.8416	1.0703	1.0416
1.850	.9425+08	.996+	1.6674	.7520	.1452	.4959	.2937	.7817	.9761	9010	.8354	1.0815	1.0492
1.900	.935E+08	• 9963	1.6690	.7415	1350	.4817	.2818	.6888	9730	9044	8295	1.0935	1.0576
1.950	+927E+08	.9963	1.6784	.7311	.1255	.4679	.2689	.6585	9700	9084	. 82 38	1.1060	1.0663
2.000	.920E+08	.9953	1.6714	.7208	.1167	.4546	.2575	.6375	9671	91 32	-8183	1.1193	1.0758

F. (CONTINUED)

MACH	LCCAL ISENTROPIC	VISCOSITY	THERMAL CONDUCTIVITY	PRANDTL
	EXPANSION COEFF.	G/CM-SEC	CAL/CH-SEC-K	NUMBER
30. T		57 011 520	ONE ON DEO K	KONGER
0.000	The state of the s	-42301E-04	•19268E-03	.7079
.050	1.4600	. 42284E-04	.19254E-03	.7079
.100	1.4398	.42232E-04	.19213E-03	.7077
•150	1.4669	.4214EE-84	.19146E-03	.7075
.200	1.4566	.42026E-84	•19052E-03	.7071
• 250	1.4522	-41871E-04	.18931E-03	.7067
.300	1.4611	-41683E-84	.18785E-03	.7062
. 350	1.4616	-41462E-84	.18612E-03	.7056
.400	1.4657	.41207E-04	-16415E-03	.7049
•450	1.4711	-40919E-114	•18193E-03	.7842
•500	1.4703	.40599E-04	.17947E-03	.7034
.550	1.4820	•40247E-04	•17677E-03	.7026
•600	1.4832	•39864E-84	.17365E-03	.7018
.650	1.4891	•39450E~84	•17071E-03	.7010
.700	1,4958	.39075E+04	.16737E-03	.7003
.750	1.5034	.38532E-04	.163926-03	•6993
.800	1.5127	.38031E-84	.16035E-03	-6981
.850	1.5180	•37503E-04	.15662E-03	-6972
• 900	1.5266	• 76949E+B4	•15274E-03	•6964
• 95 0	1.5379	.36372E-04	.14873E-03	.6960
1.000	1.5442	•35773E- 0 4	-14468E-03	•6960
1.050	1.5560	.35154E-04	.14037E-03	•6965
1.100	1.5659	•34517E-04	.13667E+03	-6934
1.150	1.5741	.33866E-84	.13334E-03	.6907
1.200	1.5861	.33204E-84	.12976E-03	.6884
1.250	1.5929	.32533E+04	•12621E-03	.6867
1.308	1.6032	.31857E-84	•12264E-D3	.6855
1.350	1.6108	•31178E-04	•11912E-03	.6848
1.400	1.61.95	.30500E-04	.11577E-03	.6839
1.450	1.6275	•29826E-04	•11246E-03	•6836
1.500	1.6313	.29156E-04	•10921E+03	.6838
1.550	1.6387	• 28494E-04	•10683E-03	.6846
1.600	1.6436	.27840E-84	.10293E-03	.6858
1.650	1.6501	• 271 97E-#4	• 99915E-04	-6874
1.700	1.6535	• 26565E+04	•96930E+04	.6897
1.750	1.6553	•25945E-04	•94289E-04	.6905
1.800	1.6570	•25337E-04	•91732E-04	• 6915
1.650	1.6605	.24742E-84	.69257E-04	•6926
1.900	1.6634	• 24159E-04	•86865E-04	+6938
1.950	1.6615	.23589E-04	.84541E-04	.6951
2.000	1.6643	-230325-04	.82274E-114	•6967
		and the second s		

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OF IGINAL PAGE IS SE POOR QUALITY 00

TABLE II. PEAL-GAS ISENTROPIC EXPANSIONS OF PARAHYDROGEN

			TABLE	11.	CAL-GAS I	SENIKUPIG	EXPANSION	VS OF PAR	KAHTUROGEN			F.3.3	
		G. TT	= 200.0	C PT =	3.0 ATM	RHOT =	.368E-03	G/CH3	SVT =1056	.041 H/S	EC	1 .	
MACH	PE/M	7	CP/CV	SVIST	P/FT	T/TT	RHOZRHOT	A*/A	SV/SVI	P/PT		RHOZRHOT	A*/A:
									++	RELATIVE	TO IDEAL	GAS, VALUE	\$
0.000	0	1.0020	1.3467	1.0000	1.0000	1.0000	1.0000	0.0000	1.0000	1.0000	1.0000	1.0000	1.0000
.050	-284E+07	1.0028	1.3466	9998	9982	.999€	9986	.0859	1.0000	1.0000	1.0001	.9999	.9957
-100	.566E+07	1.0020	1.3465	. 9991	9973	.9983	9951	.1710	1.0001	1.0003	1.0083		.9956
.150	.845E+07		1.3463	. 9979	. 9849	.9961	-9887	.2547	1.0001	1.0005	1.0006	.9999	9958
.200	*115E+08	1.0020	1.3461	9963	9735	.9931	9503	.3361	1.0003	1.9010	1.0011	1.0000	.9960
•250	·138E+08	1.0019	1.3458	. 9942	9588	.9893	.9693	-4145	1.0004	1.0014	1.0017	.9999	.9960
•300	•164E+B8	1.0019	1.3454	• 9917	9416	.9847	•9563	-4896	1.0006	1.0022	1.0024	1.0000	.9963
.350	•188E+08	1.0008	1.3449	.9888	9216	.9793	•9412	.5604	1.0008	1.0039	1.0033	9999	.9965
.400	.2115+08	1,0018	1.3444	9854	.8991	.9731	•9241	• 62 6 8.	1.0811	1.0039	1,0043	. 9998	• 9967
•450	•233E+08	1.0917	1.3439	9817	.8745	• 9663	.9953	.6861	1.0014	1.8049	1.0054	- 9998	. 9969
.500	•253E+08	1.0017	1.3433	.9776	.8482	.9587	.8859	.7443	1.0018	1.0061	1.0067	. 9997	• 9972
•550	.272E+08	1.0716	1.3427	9732	8202	•9506	.8632	.7949	1.0022	1.0074	1.0061	.9997	.9976
.600	.289E+08	1.0716	1.3421	9684	.7907	-9418	.8400	.8396	1.0026	1.0086	1.0096	. 9994	.9978
•650	-305E+08	1.0015	1.3415	• 9633	.7603	•9324	.8158	.8789	1.0031	1.0099	1.0112	• 9992	.9981
.700	.319E+88	1.0014	1.3408	9579	.7292	.922€	.7909	.9124	1.0037	1.0115	1.0130	• 9991	. 9986
.750	•331E+08	1.0014	1.3403	9522	•6975	.9122	.7651	.9401	1.0044	1.0129	1.0149	•9987	. 9988
.600	-342E+98	1.0713	1.3397	9463	.6656	9014	.7369	.9625	1.0051	1.0146	1.0168	.9985	.9993
.850	.351E+08	1.0012	1.3392	• 9+02	.6335	.8902	.7122	9793	1.0058	1.0161	1.0189	. 9950	. 9995
.900	-358E+08	1.0012	1.3388	+9338	.6016	.8787	.6853	•9910	1.0067	1.0176	1.0210	.9974	-9998
.950	.364E+08	1.0011	1.3384	• 9273	5701	.8668	•65 83	.9978	1.0075	1.8190	1.0233	.9967	1.0000
1.000	•36 6E+0 8	1.0019	1.3382	9206	•5390	.8546	-6313	1.0000	1.9985	1.0203	1.0256	.9958	1.0000
1.050	-371E+00	1.0010	1.3380	. 9138	*5086	.8422	-6045	.9960	1.0095	1.0215	1.0279	. 9948	1.0008
1.100	•373E+08	1.0009	1.3380	•9068	.47RB	.8295	•5778	- 9918	1.0106	1.0223	1.0302	.9933	9996
1.150	.373E+08	1.0008	1.3382	. 6998	.4500	.616€	-5517	.9622	1.0118	1.0231	i.0326	.9919	.9993
1.200	•373E+08	1.0008	1.3386	8926	.4221	.8036	-5260	• 9695	1.0130	1.0237	1.0350	. 9903	.9990
1.750	.3715+08	1.0007	1.3392	.8854	.3953	.7903	.5016	. 9537	1.0143	1.0239	1.0373	.9884	.9983
1.300	*368E+08	1.0007	1.3400	.8781	3695	.7769	•4762	. 9354	1.0157	1.0238	1.0396	.9862	• 9974
1.350 1.400	.364E+08	1.0006	1.3410	.8707	.3449	.7635	• 4524	.9151	1.0171	1.0236	1.0418	.9840	• 9965
1.450	•355E+08	1.0006 1.0005	1.3423	. 8633	.3214	.7499	•4292	6927	1.0186	1.0229	1.0439	. 9813	•9953
1.500	•349E+08		1.3439	8559	.2990	. 7362	-4868	.8687	1.0201	1.0216	1.0458	.9783	.9937
1.550		1.0005	1.3458	. 84 84	.2778	,7225	.3651	.8433	1.0216	1.0198	1.0476	.9750	• 199•
1.600	•342E+08	1.0004	1.3481	-8409	•2577	-7087	.3642	.8169	1.0232	1.0176	1.0492	.9714	-9897
1.650	.336E+08	1.0004	1.3568	.8335	.2388	-6948	-3442	.7898	1.0249	1.0148	1.0595	.9676	- 9874
1.700	.321E+08	1.0003	1.3540	8260	.2209	.680.9	-3249	.7619	1.0265	1.0113	1.0516	.9632	- 9846
1.750	.313E+08	1.0002		.8185	.2941	.6669	.3066	.7340	1.0282	1.0074	1.0524	9589	-9818
1.800	•305E+08	1.0002	1.3616	.8111 .8036	•1884 •777	6529	•2690 2327	.7059	1.0299	1.0030	1.0529	9543	•9787
1.850	•297E+08	1.0002	1.3712	.7962	•1737	-5389	.2723	.6777	1.0317	9978	1.0529	-9494	.9753
1.900	•289E+08	1.0001	1.3712	• 7 9 8 5	.1599 .1471	.6249	•2563	-6497	1.0334	.9919	1.0526	.9441	-9714
1.950	.261E+08	1.0001	1.3832	.7814	.1351	.6108 .5968	.241?	.6228	1.0351	. 9854	1.0518	.9386	.9674
2.000	.273E+88	1.0001	1.3981	7741	.1240	-5827	•2268 2177	5948	1.0368	• 97 82	1.0506	.9329	.9631
		20001	193701	611-47	4 T C # fi	. 2061	-2133	.5681	1.0385	.9705	1.0488	.9271	e 95 8 7

G. (CONTINUED)

MACH	LOCAL ISENTROPIC	VISCOSITY	THERMAL CONDUCTIVITY	PRANDTL
	EXPANSION COEFF.	G/CM-SEC	CAL/CH-SEC-K	NUMBER
0.900	I	.68237E-04	.37355E-03	.7025
.050	1.3223	.682136-84	.37347E-03	.7025
.100	1.3638	.68153E-04	.37322E-03	.7025
• 150	1.34.10	.68052E-04	.37281E-03	.7025
.200	1.3530	.67913E-04	.37224E-03	. 7025
.258	1 - 3445	.67734E-04	.37151E-03	.7025
.300	1.3514	.67518E-04	.37063E-03	.7025
.350	1.3472	.67265E-04	.36961E-03	.7025
• 400	1.3461	.66976E-04	.36844E-03	.7024
45 0	1.3460	.66653E-04	.36713E-03	.7023
•500	1.3470	.66298E-04	.36570E+03	.7021
•550	1.3458	.65911E-04	.36414E-03	.7019
•600	1.3432	.65494E-84	-36218E-03	.7021
•651	1.3436	.65049E-04	.35939E+03	.7037
.700	1.3447	.54577E-04	.35644E+D3	.7053
•750	1.3421	.64081E-04	.35335E-03	.7068
.600	1.3431	.63561E-04	•35013E-D3	.7084
. 850	1.3415	.63028E-04	.34678E-03	.7098
<u>. 900</u>	1.3410	.62458E-84	.34333E-03	.7112
• 950	1.3403	.618775-04	.33978E-03	.7125
1.000	1.3393	.51280E-04	.33614E-03	.7136
1.050	1.3399	.60665E-04	•33242E-03	.7145
1.100	1.3360	.60036E-84	.32662E-03	.7151
1.150	1.3393	.59393E-04	.32477E-03	.7155
1.200	1.3397	•5873 8E-04	.32067E-03	.7156
1.250	1,3397	.58069E+04	.31691E-03	.7153
1.300	1.3401	.5739NE+04	•31291E-03	.7147
1.350	1.3424	.56781E-04	.30889E-N3	.7136
1.400	1.3420	.56002E-04	.30483E-03	.7121
1.450	1.3436	.552946-84	.30074E-03	.7181
1.500	1.3449	•54577E-04	•29664E-D3	.7076
1.550	1.3472	.53651E-04	.29012E-03	.7103
1.600	1.3501	.53116E-04	.28353E+03	.7128
1.650	1.3516	. 52374E-04	.27693E-03	.7148
1.700	1.3568	.51623E-04	.27030E-03	.7164
1.750	1.3698	.50865E-04	.26366E-03	.7177
1.000	1.3642	.50099E-04	.25700E-03	.7185
1.850	1.3686	.49325E-04	.25034E-03	.7189
1.900	1.3741	.48543E-04	.24367E-03	.7189
1.958	1.3894	.47753E-94	.23699E-03	.7184
2.000	1.3875	•46956E-04	.23031 <u>5</u> -03	.7175

ORIGINAL PAGE IS OF POOR QUALITY



TABLE II. REAL-GAS ISENTROPIC EXPANSIONS OF PARAHYDROGEN

		•	1 8 34 6 6	11. 4	EAC-GAS I	SENIKOPIO	EXPANSION	AS OF PA	KAHYURUGEN				
		н. Т	T = 300.0 K	PT =	3.0 ATM	RHOT =	.245E-03	G/CM3	SVT =1311	.496 H/SI	EC		
MACH	RE/M	Z	CPZCV	SV/SVT	P/PT	T/TT	RHO/RHOT	A+/A	SV/SVT	P/PT	T/TT	RHO/RHOT	A*/A
								,, + ,,				GAS VALUES	
0.000	0.	1.0018	1.3699	1.0000	1.0000	1.0000	1.0000	0.0000	1.0000	1.0000	1.0000	1.0800	1.0000
.050	-179E+07	1.0018	1.3852	9997	,9982	•9995	•9987	.0863	1.0000	1.0000	1.0000	•9999	1.0008
100	.357E+07	1.0018	1.3851	.9990	9930	,9981	9949	.1719	1.0000	1.0000	1.0001	•9999	1.0007
-150	.532E+07	1.0018	1.3850	9977	9845	.9957	9888	2559	.9999	1.0001	1.0002	1.0000	1.0000
-200	.704E+07	1.0717	1.3847	9959	.9727	.9924	9802	.3377	.9999	1.0002	1.0003	.9999	1.0007
.250	.871E+07	1.0017	1.3844	.9937	.9578	.9881	9694	•4165	.9999	1.0004	1.1005	1.0000	1.0007
.300	.103E+98	1.0017	1.3849	.9909	.9399	.9837	-9563	.4916	.9998	1.0005	1.0007	.9999	1.0006
.350	.119E+D8	1.0017	1.3836	.9877	9194	.9770	9412	.5627	.9997	1.0007	1.0009	9999	1.0005
.480	•133E+08	1.0016	1.3830	9840	.8967	.9702	.9244	-6293	.9996	1.0012	1.0012	1.0001	1.0006
.450	-147E+08	1.0016	1.3824	.9799	.8716	.9626	-9056	.6907	.9996	1.0015	1.0016	1.8001	1.0006
•500	.160E+08	1.0016	1.3817	.9754	8446	9543	.8853	.7467	9995	1.0019	1.0020	1.0001	1.0004
.550	.172E+08	1.0715	1.3409	.9705	.8160	9453	8634	.7970	9994	1.0022	1.0025	1.0000	1.0002
.600	.183E+08	1.0015	1.3801	.9651	7862	9356	8405	.8418	.9993	1.0028	1.0030	1.0001	1.0002
-650	-192E+08	1.0014	1.3791	. 95 95	.7553	. 9254	-8164	.6806	.9992	1.0032	1.0036	1.0000	1.0081
.700	.201E+08	1.0014	1.3781	. 9535	7237	-9146	.7916	.9137	9991	1.0038	1.0043	1.0000	9999
.750	.289E+08	1.0013	1.3770	9472	6916	9834	.7660	9410	.9990	1.0044	1.0050	. 9999	.9998
.800	.216E+08	1.0013	1.3757	.9406	.6596	.8917	.7401	9631	9989	1.0054	1.0059	1.0001	9999
.850	.222E+08	1.0012	1.3744	.9337	6275	.8797	.7138	9797	9989	1.0064	1.0068	1.0002	9999
.900	.226E+08	1.0012	1.3730	.9266	5957	.8673	-6873	9912	.9988	1.0075	1.0078	1.0003	1.0000
•95 D	.230E+08	1.0011	1.3715	• 91 92	.5643	-8547	.6617	.9979	.9988	1.0086	1.0089	1.0004	1.0000
1.000	.233E+08	1.0010	1.3699	.9117	.5335	.8418	.6342	1.0000	9987	1.0098	1.0101	1.0004	1.0000
1.050	.235E+08	1.0010	1.3583	.9040	.5034	· 82 87	•6888	.9981	.9987	1.0112	1.0114	1.0005	1.0001
1.100	•236E+08	1.0009	1.3666	.8962	.4742	.8155	.5620	9923	.9988	1.0125	1.0129	1.0005	1.0001
1.150	·237E+08	1.0009	1.3648	.8882	•4459	.8022	•5563	-9828	.9988	1.0138	1.0144	1.0003	1.0000
1.200	•236E+98	1.0008	1.3629	.8802	.4187	.7889	.5312	.9783	,9989	1.0152	1.0161	1.0001	.9999
1.250	.235E+08	1.0006	i.3611	.8720	.3925	.7755	.5067	• 9552	.9990	1.0168	1.0178	1.0000	.9998
1.300	.234E+08	1.0007	1.3591	•8638	. 3676	.7621	.4829	.9379	•9992	1.0186	1.0197	1.0000	1.0000
1.350	.232E+08	1.0007	1.3572	.8555	.3437	•7487	•4596	.9180	•9994	1.0200	1.0216	• 9995	.9997
1.400	.229E+08	1.0007	1.3553	.8473	.3210	.7354	-437f	.8965	•9996	1.0215	1.0237	. 9998	. 9995
1.450	•226£+B8	1.0006	1.3533	• 839T	. 2995	.7222	•4151	.8734	•9999	1.0230	1.0258	9984	. 9992
1.500	-222E+08	1.0006	1.3515	.8307	.2790	.7090	•3940	.8491	1.0003	1.0243	1.0281	.9976	-9987
1.558	•21 8 E+08	1.0005	1.3496	.8224	.2597	•696 0	.3737	.8236	1.0007	1.0256	1.0304	9966	.9981
1.600	+214E+08	1.0005	1.3478	.6142	.2416	•6830	.3541	.7978	1.0011	1.0267	1.0328	• 9955	.9974
1.650	•210E+08	1.0005	1.3461	.8060	.2245	.6783	.3354	.7713	1.0016	1.0278	1.0352	. 9942	.9967
1.700	•205E+08	1.0004	1.3444	.7978	.2084	•6576	.3173	.7444	1.0022	1.0287	1.0377	• 9927	.9957
1.750	·2002+08	1.0004	1.3429	+7897	. 1 933	•6451	.3010	.7171	1.0028	1.8290	1.0402	9906	. 9943
1.800	•195E+08	1.0004	1.3416	.7817	.1792	•6327	.2836	•6900	1.0035	1.0294	1.0427	9886	.9929
1.850	•190E+08	1.0004	1.3484	•7737	•1559	-6285	•2678	.6630	1.0042	1.0294	1.0452	.9863	.9913
1.900	.185E+08	1.0003	1,3393	.7659	.1536	.6084	.2528	.6363	1.0050	1.0293	1.8477	9838	.9896
1.950	•179E+08	1.0003	1.3385	.7581	.1421	•5965	•2 3 85	-6098	1.0058	1.0286	1.0502	•9809	.9875
5.000	·174E+08	1.0003	1.3378	.7504	.1313	5648	•2249	.5837	1.0067	1.0275	1.0526	•9776	.9850

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H. (CONTINUED)

MACH	LOCAL ISENTROPIC	VISCOSITY	THERMAL CONDUCTIVITY	PRANDTL
	EXPANSION COSFF.	G/CM-SEC	CAL/CM-SEC-K	NUMBER
0.000	I	.89634E-84	.46160E-03	.7098
.050	1.3681	.89632E-04	.46147E-03	.6896
.100	1.3842	.89545E+04	.46109E-03	.6896
. 150	1.3923	.89410E-84	.46045E-83	.6897
.200	1.3838	.89198E-04	.45956E-113	.6898
.250	1.3903	.88948E-84	.45843E-03	.6899
.300	1.3638	.88628E-04	.45706E-03	.6900
.350	1.3860	.86263E-04	.45547E-03	•6902
.481	1.3891	.87847E-04	.45365E-03	-6904
.450	1.3855	.87383E-04	.45163E-03	•6906
•500	1.3833	.86872E-04	•44941E-03	.6908
•550	1.3814	.86318E-04	.44701E-03	.6911
•600	1.3834	.85727E-84	.44444E-113	•6914
•65D	1.3797	.85088E-04	.44174E-03	-6917
.700	1.3797	.84418E-04	.43902E-03	•6919
.750	1.3777	.83716E-04	.43617E-03	.6921
.800	1.3797	.929845+04	-43322E-03	.6924
850	1.3775	.82225E-04	.43017E-73	.6927
.900	1.3761	.81442E-D4	.42704E-03	.6930
• 950	1.3740	•80637E-04	•42363E-03	•6 933
1.000	1.3721	.79814E-04	.42057E-03	•6 9 37
1.050	1.3715	.78974E-04	•41726E-03	.6941
1.100	1.3686	.781??E-04	.41392E-03	.6945
1.150	1.3660	.77255E-04	•41054E-03	•6949
1.280	1.3643	.76385E-04	.40716E-83	.6953
1.250	1.3633	.75505E -0 4	•40369E-03	•6959
1.300	1 + 3633	•74620E-04	-39991E-03	.6970
1.350	1.3567	.73732E-04	.39612E-03	.6980
1.400	1.3571	.72841E-04	.39235E-03	•6990
1.450	1.3549	•71949E-04	.3886DE-D3	•6998
1.500	1.3527	•71058E-04	.36488E-03	.7006
1.550	1.3511	.70168E-04	.38119E-93	.7012
1.600	1.3491	.69281E-04	.37752E-03	.7817
1.650	1.3479	.68397E-04	.37390E+03	.7021
1.700	1.3461	•67517E-04	•37032E-03	.7922
1.750	1.3428	•66640E-84	.36677E-03	.7020
1.600	1.3432	.65768E-84	.36327E-03	.7016
1.850	1.3419	•64900E-04	.35832E-03	.7037
1.900	1.3416	.64037E-04	•35293E-D3	.7065
1.950	1.3397	•631.79E-94	.34762E-03	.7090
2.000	1.3390	.62325E-04	.34236E-83	.7112

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TABLE III. REAL-GAS ISENTROPIC EXPANSIONS OF PARAHYDPOGEN

		4 TT	= 35.0	K PT =	5.0 ATM	= 10H¢	.398F=92	G/CM3	SVT = 467	.465 H/S	EC		
MACH	주도 / M	Z	CP/CV	SV/SVT	P/PT	7/17	RHOZRHOT	A*/A	SV/SVT	P/PT RELATIVE	T/TT TO IDEAL	RHD/RHOT GAS VALUES	A*/A
0.000	0.	. 58119	1.9733	1.0000	1.0000	1.0000	1.0000	0.0000	1.0000	1.0000	1.0000	1.0000	1.0000
• 05 8	.480E+08	.8808	1.973?	•9995	.9979	.9991	9948	.0895	.9996	• 9996	9996	1.0000	1.0372
•100	.957E+08	.8897	1.9730	.9981	9914	.9955	9950	.1780	9991	9984	9985	1.0000	1.0364
.150	.143E+99	.8936	1.9729	. 9957	• 9809	.9923	.9888	.2547	9979	9964	9967	1.0000	1.0352
.200	.1895+09	.8804	1.9727	.9924	.9564	.9864	9803	.3488	•9963	. 9938	9942	1.0000	1.0336
.250	.235F+09	.9991	1.0724	.9882	. 9485	.9789	9697	.4294	•99+3	9906	9911	1.0003	1.0318
•309	•279E+09	, 9799	1.9721	.9431	.9268	9699	9566	.5058	9919	9865	.9873	1.0003	1.0293
•35N	.321E+09	.8795	1.9715	.9772	9024	9595	9419	•5775	9891	9822	.9830	1.0006	1.0258
• 400	.363:+09	.8792	1.9712	9706	. 9754	.9478	9254	-6441	9860	•9775	9781	1.0012	1.0242
•450	.402E+09	.8788	1.9716	.9535	-8-59	9349	.9079	.7049	9828	.9721	9728	1.0016	1.0212
•500	*##UE+U3	.8784	1.9717	.9557	-8149	9209	.8874	.7681	.9793	.9666	• 9670	1.0025	1.0164
•550	.475E+09	.8779	1.9719	.9473	.7825	9061	.8665	.8894	9755	.9611	9608	1.0036	1.0157
•608	.509E+09	.8775	1.9719	.9384	.7489	.8902	.8445	8524	.9715	.9552	9542	1.0048	1.0128
-65 0	.541E+09	.8770	1.9721	.9298	.7149	.8736	.8219	.8896	.9674	9496	.9474	1.0067	1.0103
.700	.570E+09	.8766	1.9721	. 91 91	•€805	•856 5	.7985	.9209	9631	.9440	9494	1.0087	1.0079
•75 d	.598E+09	.8767	1.9721	.9989	.6462	.8388	.7745	. 9465	.9587	9384	. 9332	1.0110	1.0056
.800	.624F+09	.8757	1.9729	.8984	.6122	.8207	7583	.9667	9542	9332	.9258	1.0139	1.0037
•850	.6475+00	• ዓንም ፕ	1.9717	.8876	-5788	8024	.7259	.9819	9496	9283	9183	1.0173	1.0022
-900	.669£+09	.8749	1.9712	.8766	.5462	.7839	.7016	.9922	9450	.9238	.9108	1.0711	1.0010
•950	•6895+09	8745	1.9706	.8654	-51-6	7652	-6773	9983	9403	.9198	.9033	1.9756	1.0004
1.000	.707E+09	,9741	1.9698	.6541	. 4 BLB	7466	.6533	1.0002	9356	.9162	.8959	1.0305	1.0002
1.050	.724E+09	.9738	1.9687	.8426	. 4545	.7281	6294	9982	9309	9129	.8885	1.0358	1.0002
1.100	.739F+09	.8735	1.9674	.8311	.4264	.7095	•6060	.9932	•9252	9184	.8812	1.0418	1.0003
1.150	.7525+09	.8732	1.9660	.8196	.3996	.6912	+5832	.9853	•9216	9885	.8740	1.0416	1.0025
1.290	.7645+09	• R 7 ኛ ŋ	1.9645	.8080	. 3741	.6732	.5608	9747	.9170	.9072	.8670	1.0556	1.0044
1.250	.774E+09	.8727	1.9628	.7965	.3500	.6554	.5389	9619	9125	9865	.8602	1.0636	1.0068
1.390	.783E+09	.8725	1.9611	.7951	.3271	.6379	-5176	.9471	9081	.9063	. 8536	1.0720	1.8099

A. ICONTINUEDI

MACH	LOCAL ISENTROPIC	VISCOSITY	THERMAL CONDUCTIVITY	PRANDTL
	EXPANSION COEFF.	G/CM-SEC	CAL/CM-SEC-K	NUMBER
0.000	I	.194425-04	.72465E-04	.8131
.050	1.7253	.19381E-84	.72223E-04	.6133
.100	1.7089	•19335E-84	.72035E-04	.8135
.150	1.7153	.19258E-04	.71725E-04	.8139
.200	1.7171	.19152E-04	•71293E-04	.8144
.250	1.7271	.19017E-04	.70745E-04	.8152
.300	1.7043	.18854E-04	.70075E-04	.8161
.350	1.7170	.18666E-04	.69297E-04	.8174
400	1.7175	.16454E-04	.68414E-04	.8189
450	1.7817	.18219E-04	.67423E-04	.8206
.500	1.7119	.17963E-84	.66344E+04	.8223
.550	1.7112	.17689E-04	.65364E-04	.8221
600	1.7031	.17397E-04	.64307E-04	.8219
•550	1.7096	.17091E-04	.63183E-04	.8219
.700	1.7040	.16772E-04	.61994E+04	.8221
.750	1.7005	.16441E-84	.61748E-04	.8226
.800	1.7010	.16101E-04	.59454E-84	.6233
.850	1.6998	.15755E-04	•58118E-04	. 8244
.900	1.6975	.15402E-04	.56750E-04	.8258
.950	1.6971	.15046E-84	.55390E-04	.8270
1.000	1.6942	.14688E-B4	.54018E-94	.8286
1.050	1.6871	.14328E-04	.52803E-04	.8276
1.100	1.6890	.13969E-04	.51551E+04	.8277
1.150	1.6869	.13611E-04	.50239E-04	.8290
1.200	1.6835	.13256E-04	.48883E-84	.8316
1.250	1.6799	.12905E-04	.47492E-04	.8354
1.300	1.6766	12557E-04	.46076E-04	.8405

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TABLE III. REAL-GAS ISENTROPIC EXPANSIONS OF PARAHYDROGEN

		e. T	T = 40.0	K PT =	5.0 ATM	RHOT =	.334E-02	G/CM3	SVT = 509	.634 M/S	C		
MACH	RE/H	Ż	CP/CV	SV/SVT	P/PT	T/TT	RHO/RHOT	A+/A	SV/SVT	P/PT RELATIVE	T/TT TO IDEAL	RHO/RHOT GAS VALUES	A*/A
0.000	0.	. 91 99	1.8676	1.0000	1.0000	1.0000	1.0009	0.0000	1.0000	1.0000	1.0000	1.0000	1.0000
.050	.395E+0 6	. 91 98	1.8676	•9995	•9979	.9991	• 9985	.0894	.9998	.9996	.9996	1.0000	1.0360
.100	.700F+08	•9198	1.8675		• 9914	.9966	.9951	.1778	.9991	. 9984	9986	9999	1.0352
.150	1165+69	.91 96	1.8674		.9811	.9923	.9889	.2645	• 998 t	. 9966	. 9968	1.0001	1.0343
.200	.156E+09	•9195	1.8673		•9656	•9864	-9884	.3485	• 9966	. 9948	9943	1.0001	1.0327
.250	•193E+09	•9193	1.8671		.9485	• 97 B P	• 96 95	.4290	.9947	. 9986	.9912	1.0001	1.0386
.300	.229E+09	.9190	1.8679		•9272	. 9781	9568	•5055	. 9924	. 9869	.9874	1.9334	1.0288
.350	265E+09	.9187	1.0667	9779	.9028	•9596	.9420	.5773	•9898	.9826	. 98 31	1.0007	1.0264
-400	,298E+09	.9184	1.8664	•9714	.87F6	.9479	•9252	•6437	.9869	. 9777	. 97 62	1.0010	1.0236
• 45 0	.331E+09	.9181	1.8660	. 9643	• 846 3	.9350	-90 69	.7047	.9836	.9725	.9729	1.0016	1.0208
.500	.361E+09	. 9177	1.8656	• 9565	.8154	•9219	.8874	.7599	.9801	.9672	.9671	1.0025	1.0181
•550	.390E+09	•9174	1.8651	. 9481	.7829	.9061	•85 6 4	. 8090	9764	.9616	.9609	1.0034	1.0152
.600	.418E+89	.9170	1.8646	.9792	.7495	.8983	. 5445	.8521	.9725	• 9560	. 9544	1.0048	1.0125
•65£	.444E+09	• 91 66	1.8641	• 9299	.7155	.873 B	.8218	.8893	.9684	.9504	.9476	1.0065	1.0100
.700	.468E+09	•9162	1.8634	.9201	.6811	.8567	7983	.9286	.9641	.9448	94.06	1.0085	1.0074
.750	.498E+09	.9158	1.8628	• 90.99	•6470	.8391	•7745	. 9464	.9598	. 93.96	.9334	1.0110	1.0055
. 500	.510E+09	.9155	1.8624	. 8996	.6129	.8210	.7501	• 9666	.9554	.9342	.9261	1.0137	1.0035
•85 D	.529E+09	.9151	1.8621	.8889	.5794	.8026	•7256	.9817	.9510	. 92 92	- 91 86	1.0168	1.0020
-900	•547E+09	.9148	1.8618	.8781	5467	.7840	.7012	• 9922	. 9465	.9246	.9110	1.0206	1.0010
• 9 50	•563F+09	.9144	1.8614	.8671	.5149	•7653	.676 7	.9981	.9421	.9203	. 99 34	1.0247	1.0002
1.000	.577E+09	• 91 4 1	1.8611	• 8559	.4841	.7465	6575	1.0000	.9376	. 91 64	. 8959	1.0293	1.0000
1.050	.5905+09	. 91 18	1.8606	.8446	.4545	.7278	.6286	• 9982	.9331	.9129	.8883	1.0345	1.0802
1.100	•602E+09	•9136	1.8601	.8333	• 4262	.7092	.6051	.9932	.9287	.9100	.8806	1.0403	1.0010
1.150	.612E+09	.9133	1.6595	.8219	•3992	6907	•5820	• 9851	.9243	.9075	.8734	1.0465	1.0023
1.200	.621F+09	•9131	1.8589	-6106	.3735	.6724	•5596	.9745	.9199	.9057	.8661	1.0535	1.0942
1.250	.629E+09	.9179	1.8581	.7992	.3491	-6544	•5876	.9516	.9156	.9043	.8589	1.0609	1.0065
1.300	.636E+09	.9127	1.8572	.7879	.3261	•6367	.5163	• 9468	.9113	• 9 0 3 6	8518	1.0691	1.0096
1.350	, S42E+09	•9126	1.4562	.7766	.30-4	.6192	•4955	.9302	.9072	. 90 34	.8449	1.0777	1.0130
1.400	.648E+89	• 9124	1.8552	.7654	.2840	-6822	4755	•9123	. 90 31	- 90 38	. 6382	1.0870	1.0171
1.458	•65?E+89	•9123	1.8541	.7543	.2648	•585F	•4560	.8931	.6991	9047	.0317	1.0967	1.0217
1.500	.655E+09	.9122	1.8530	.7434	.2469	•5692	.4374	.8733	.8951	9064	8253	1.1074	1.0271
1.550	.658E+09	.9172	1.8518	.7325	.2301	-5533	•4193	.8525	.8913	-9083	. 8191	1.1183	1.0328
1.600	.661E+09	.9121	1.8507	.7219	.21-4	.5376	•4020	.8313	.8876	.9111	. 61 32	1,1300	1.0393
1.650	·662E+89	.9120	1.8496	.7113	.1997	•5227	.7857	.8097	.8541	91 43	.8074	1.1422	1.0462
1.700	•663F+09	.9121	1.8485	.7009	• 18€®	.5081	.3693	.7879	.6805	. 91 82	.8018	1.1551	1.0538

B. (CONTINUED)

MACH	LOCAL ISENTROPIC	VISCOSITY	THERMAL CONDUCTIVITY	PRANDTL
	EXPANSION COEFF.	G/CM-SEC	CAL/CH-SEC-K	NUMBER
0.000	I	-21553E-04	.79421E-94	.7683
.050	1.7137	.21489E-04	.79158E-04	.7685
.100	1.6975	.21440E-04	.78955E+04	.7687
.150	1.7263	.21359E-84	.78623E-N4	.7690
.200	1.7068	.21246E-84	.78159E-04	.7694
.250	1.7045	.21102E-04	.77570E-04	.7699
.300	1.7170	.20930E-04	.76864E+04	.7706
.350	1.7093	.20730E-04	.76043E-04	.7714
•400	1.7028	.20504E-04	.75158E+ti4	.7718
.450	1.7039	.20253E-84	.74174E-84	.7725
•500	1.7080	•19981E-Q4	•73093E-04	.7733
•550	1.7904	.19688E+04	.71953E-04	.7740
•600	1.7023	.19377E-04	-70742E-04	.7748
•657	1.7025	.19050E-04	.69464E-114	.7757
.700	1.6965	.18709E-04	.68127E-04	.7768
•750	1.7010	.18355E-04	•66743E-04	.7780
.800	1.6924	•17992E-04	.65315E-04	.7793
• 85 n	1.6939	.17619E-04	.63869E-04	.7803
• 900	1.6941	.17239E-N4	.62466E-04	.7605
• 950	1.6913	•16855E-04	•61072E+04	.7603
1.000	1.6904	.16466E-04	.59646E-04	.7804
1.050	1.6892	.16076E-04	.58194E-84	.7808
1.100	1.6891	.15685E-84	.56723E-84	.7814
1.150	1.6862	.15295E-04	.55238E-04	.7824
1.200	1+6869	.14906E-04	•53749E-04	.7836
1.250	1.6838	.14520E-04	-52260E-04	.7851
1.308	1.6840	•14137E-04	。J0657E-04	.7857
1.350	1.6799	.13759E-04	.49427E-04	.7871
1.400	1.6799	•13386E-04	•47973E-84	.7895
1 - 450	1.6767	.13019E+04	•46559E-04	.7917
1.500	1.6791	.12658E-04	.45248E-84	.7930
1.550	1.6722	.12304E-04	.43955E-04	.7945
1.600	1.6741	.11957E-04	.42687E-04	.7963
1.650	1.6714	.11617E-04	•4144E-04	.7984
1.700	1.6707	·11285E-04	.40226E-04	.6836

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TABLE TIL. REAL-GAS ISENTROPIC EXPANSIONS OF PARAHYCROGEN

		C. TT	= 60.0 *	(PT =	5.0 ATM	PHOT =	.209E-02	G/CH3	SVT = 634	.456 M/SI	EC		
MACH	RE/M	7.	CP/EV	SV/SVT	P/PT	T/T T	RHOZEHOT	A*/A	SV/SVT	P/PT ELATIVE	T/TT TO IDEAL	RHO/RHOT GAS VALUES	A+/A
0.000	0.	.9774	1.7017	1.0000	1.0000	1.0000	1.0090	0.0000	1.0000	1.0000	1.0000	1.0000	1.0000
•050	*226E+08	.9774	1.7023	•9996	9979	.9992	.9987	.0885	9999	.9996	.9997	.9999	1.0259
.100	.452F+88	.9773	1.7028	.9985	•9916	•9968	9949	.1761	9995	9986	9987	.9999	1.0254
.150	.674E+08	.9773	1.7035	• 9966	.9815	.9927	. 9885	.2621	.9988	.9970	. 9972	1.0000	1.0248
.200	.8935+08	.9771	1.7946	.9948	•9674	.9871	.9883	.3455	.9979	.9948	. 9950	1.0000	1.0239
.250	•1115+09	•9770	1.7059	• 9906	.9498	, 980 u	• 9696	•4258	•9967	.9920	+9973	1.0002	1.0229
.300	.131E+09	.9769	1.7974	• 9865	.9287	.9714	. 9566	.5020	.9953	. 9886	.9889	1.0003	1.0215
.350	.151E+89	•9766	1.7098	-9817	.9947	.9615	.9417	.5737	•9936	.9847	.9850	1.0005	1.0200
. 400	.171E+09	•9764	1.7198	9762	.8780	. 95 02	.9249	.6404	.9917	.9803	. 9806	1.0007	1.0163
.450	.189E+89	• 9762	1.7126	.9700	.8489	.9377	• 9064	.7015	•98 9 4	• 9754	.9757	1.0010	1.0163
.500	.206E+09	.9759	1.7145	•9632	.8180	.9241	.8866	.7571	9870	.9703	.9703	1.0016	1.0143
.550	•223E+D9	.9756	1.7165	.9559	.7856	.9094	.8654	.8066	.9842	. 9649	. 9644	1.0023	1.0123
-600	.2385+09	.9753	1.7183	.9478	•7572	.6939	.8433	.8503	.9813	• 95 95	. 95 82	1.0034	1.0103
-650	.2528+09	•9750	1.7201	•9392	.7189	.8775	.8202	.8879	.9781	.9538	• 95 17	1.0046	1.0083
.700	•266€ + 09	- 9747	1.7217	•9302	.€83E	-8695	.7965	•9196	.9747	. 9462	.9449	1.0053	1.0064
.750	.2785+119	+9744	1.7232	.9209	•6491	.5438	.7724	.9457	.9712	.9427	.9378	1.0083	1.0047
.890	.289E+09	.97-1	1.7245	.9109	.E148	.8249	•7478	.9662	• 9674	•9372	-9305	1.0186	1.0032
.850	•299E+09	9738	1.7256	.9007	.5812	.806F	•7232	9817	•9636	.9321	. 9231	1.0134	1.0019
900	•308E+09	.9735	1.7265	.8902	*5*P2	•7881	•698 +	• 9921	∗ 959€	9271	•9156	1.0166	1.0009
• 95 0	• 31 6ë +0 9	.9732	1.7272	.8794	•F161	.7692	•67₹9	• 9982	•9555	• 9225	. 9080	1.0203	1.0004
1.000	.324 <u>5</u> +09	97.44	1.7278	.8685	. 4851	.7504	.E494	1.0000	.9514	•9182	.9004	1-0244	1.0000
1.050	•33NE+09	•9727	1.7282	.8574	• 4553	.7315	+6254	.9982	.9472	• 91 45	. 8929	1.0292	1.0003
1.100	.3365+09	.9774	1.7285	.8462	• 4268	.7128	.6018	•9931	.9430	. 9112	.8853	1.8345	1.0010
1.150	.341E+89	•9722	1.7286	.8349	. 3995	•6942	•5786	- 9850	.9488	• 90 84	.8778	1.0404	1.0022
1.200	•3455+NG	• 9779	1.7286	. 82 35	.3737	.675 A	•556N	.9742	.9346	• 9062	.8705	1.0468	1.0039
1.250	.348F+09	.9718	1.7286	.8122	.3492	.6577	-5348	•9612	.9305	.9044	8632	1.0539	1.0062
1.300	• 3512+09	•9716	1.7284	.9008	.3260	.6398	• 5127	. 9463	• 9264	.9033	.8560	1.0616	1.0091
1.350	*353E+09	.9714	1.7282	.7596	.3042	•6222	• 4919	• 9296	•9223	• 90 26	.8490	1.0697	1.0123
1.400	• ₹55E+09	.9712	1.7280	.7784	-2836	.6050	.4718	.9115	.9183	. 9025	.8421	1.0765	1.0163
1.450	.3575+09	.9711	1.7277	.7672	.2643	.5851	. 4524	.8923	.9144	.9838	.8354	1.0879	1.0208
1.500	.3585+09	•97119	1.7274	•7562	•2462	.5716	·4336	- 6721	.9106	.9038	.8286	1.0978	1.0257
1.550	4358E+09	.9708	1.7270	.7453	.2293	-5555	•4156	.8513	•9069	•9055	.8224	1.1084	1.0314
1.600	.358E+B9	.9707	1.7268	.7345	-2135	•5 ₹ 98	.3983	.8299	.9832	. 90 75	.8162	1.1195	1.0376
1.650	.758E+R9	.9796	1.7765	.7239	.1988	.5245	.3816	.6162	.8997	.9101	.8101	1.1313	1.0443
1.700	.358E+09	•9705	1.7262	.7134	.1850	.5096	.3656	.7862	.8962	. 91 31	.8042	1.1435	1.0516
1.750	•357E+D9	.9794	1.7259	.7031	.1722	•4951	.3503	.7642	.8928	•9168	.7984	1.1565	1.0595
1.800	.3565+09	.970⊶	1.7256	•6929	•1603	.4811	.3355	.7421	.8896	.9208	.7928	1.1699	1.0678
1.850	•355E+N9	•97113	1 • 725 र	6929	. 1492	.4674	• 3715	.7202	.8664	. 9255	.7674	1.1839	1.0768
1.900	.3545+09	9793	1.7749	.6731	.1389	.4542	.3080	.6984	+8533	•9306	.7821	1.1985	1.0563
1.950	•352E+09	• 9793	1.7246	• 6535	.1293	.4414	-2952	.6771	.8803	. 9364	.7771	1.2139	1.0965
5.000	•351F+09	•9792	1.7243	.6548	.1205	.4290	.2829	•6560	.8774	.9425	.7721	1.2297	1.1070

C. (CONTINUED)

MACH	LOCAL ISENTROPIC	VISCOSITY	THERMAL CONDUCTIVITY	PRANDTL
	EXPANSION COEFF.	G/CM-SEC	CAL/CM-SEC-K	NUMBER
0.000	I	-29364E+94	•11279E-03	•6931
.050	1.6368	.29287E-04	.11242E+03	.6931
.100	1.6554	.29230E-04	.11214E-03	•6931
.150	1.6718	.29135E-04	.11169E-03	.6932
.201	1.6664	. 2900 4E-04	.11106E+03	.6933
.250	1.6740	.28836E+04	.11026E+03	.6934
.300	1.6651	.28633E-04	•10929E+03	6936
.350	1.6705	.28397E-64	.10817E-03	.6939
.4BN	1.6692	.28128E-04	.10689E-03	.6943
•45D	1.6679	.27829E-04	.10547E-03	.6949
•500	1.6738	.27501E-04	.10254E-03	.7050
•55D	1.6718	.27147E-04	.10100E-03	.7052
•600	1.6774	.26769E-04	.99351£-04	.7056
.650	1.6758	.26369E+04	•97622E-04	.7060
.700	1.6786	.25949E-04	.95839E-04	.7065
.758	1.6800	.25513E-0+	.93993E+04	.7071
.800	1.6786	.25061E-04	.92104E-04	.7078
•85n	1.6808	.24598E-84	.90185E-04	.7085
. 900	1.6793	.24124E-04	.88234E+04	.7893
• 950	1.6812	·23642E-84	.86195E-04	.7109
1.000	1.6781	.23154E-84	.84145E-04	.7124
1.050	1.6818	.72662E-04	.81713E-84	.7175
1.109	1.6811	.22168E-94	.79727E-04	.7188
1.150	1.6795	.21672E-04	.77752E-04	.7201
1.200	1.6797	.21177E-04	•75795E-04	.7214
1.250	1.6800	·20684E-04	.73862E=04	.7227
1.300	1.6807	.20194E-04	.71958E-04	.7240
1.350	1.6769	•1970AE-04	•70095E+04	.7251
1.400	1.6778	.1922FE-04	.68264E+94	.7261
1.450	1.6775	.18750E-04	.66474E-04	.7270
1.500	1.6742	.18281E-84	.64730E-04	.7277
1.550	1.6777	.17817E-84	.63027E-04	.7282
1.600	1.6749	•17361E-04	.61365E-04	.7286
1.650	1.6757	•16913E-0↔	•59688E-04	.7296
1.700	1.6733	•16473E-04	.58739E-04	.7306
1.750	1.6753	.16041E-94	.56438E-04	.7316
1.400	1.6717	•15618E=84	.54864E-04	•7324
1.850	1.6733	•15203E-04	•53339E-04	.7332
1.900	1.6771	.14798E-Ø→	•51858E-04	.7338
1.951	1.6743	•14402Ē-04	.50421E-84	.7344
2.000	1.6715	.14015E-04	.49018E-04	.7351

ORIGINAL PAGE OF POOR QUALITY

OFFICE ALL STAPLE I

OFFICE OF

TAPLE III. PEAL-GAS ISENTROPIC EXPANSIONS OF PARAHYCROGEN

		D. TT	= 80.0 K	PT =	5.8 ATM	RHOT =	.155E-02	G/CM3	SVT = 71	5.337 H/S	EC		
MACH	PE/M	7	CP/CV	SV/SVT	P/PT	TZTT	RHOZRHOT	A-/A	SV/SVT	P/PT	7/17	RHO/RHOT	A*/A
						,						GAS VALUES	
0.000	0.	.9929	1.5716	1.0000	1.0000	1.0000	1.0000	0.0000	1.0000	1.0000	1.0000	1.0000	1.0000
.050	.153E+08	.9929	1.5739	.9997	.9981	.9993	.9988	.8869	1.0000	.9998	.9998	1.0000	1.0071
.100	.304F+08	.9929	1.5739	.9989	9922	,9972	9950	.1730	.9999	. 9992	9992	1.0000	1.0070
•150	.454E+08	.9928	1.5754	.9975	• 9826	.9938	9889	. 2575	9999	9982	.9983	1.0000	1.0070
.200	.602f+09	.9927	1.5774	• 9958	.9694	.9890	.98n3	.3398	.9998	• 9968	9969	1.0000	1.0069
.250	.745E+D8	.9926	1.5901	.9934	•9526	.9829	• 9694	.4190	.9996	. 9949	.9952	1.0000	1.0067
.300	.885E+08	.9925	1.5833	, 9906	.9326	.9754	.9565	.4947	.9994	• 9927	.9930	1.0001	1.0067
.350	·1025+09	.9924	1.5970	.9871	• 90 96	.9667	.9414	.5661	9992	.9900	.9904	1.0001	1.0064
•400	.115E+09	•9922	1.5913	.9832	.8838	9568	.9244	.6327	.9988	.9868	9874	1.0001	1.0060
-450	.1275+09	.9921	1.5960	.9789	8557	•9456	.9057	.6942	.9984	.9833	.9839	1.0002	1.0057
.500	.139E+89	.9919	1.6912	.9738	.8256	.9334	8855	.7503	9978	. 9794	.9800	1.0004	1.0053
.550	.1505+09	.9917	1.6068	•968₹	.7938	.9200	.8639	8006	.9971	9750		1.0005	1.0047
•600	.1605+09	.9915	1.6126	.9622	.7507	.9057	.9411	.8451	.9963	.9703	. 97 89	1.0008	1.0042
•650	.169E+09	.9913	1.6188	. 9557	.7266	8904	8174	.8837	.9953	.965?	.9657	1.0012	1.0035
.700	.178E+09	.9918	1.6251	.9486	.£921	.8747	.7938	.9164	9940	9600	.9600	1.0018	1.0029
.750	.186E+09	.9908	1.6314	.9411	.6571	.8575	.7679	9432	9926	9543	•9540	1.0025	1.0021
.800	.194E+09	.9906	1.6378	.9330	.6224	.8401	.7426	964	.9910	. 9487	.9476	1.0035	1.0015
.850	.2005+09	9903	1.5440	9245	.5880	.8221	.7171	9807	.9891	9430	9489	1.0049	1.0010
.900	.206E+09	.9901	1.6501	.9156	.5542	.8936	6916	.9917	9869	9373	.9338	1.0066	1.0005
.950	.211E+R9	.9899	1.6559	.9062	.5212	.7849	.6661	9979	.9846	.9316	.9266	1.0085	1.0000
1.000	.216E+09	.9896	1.6613	8964	. 4894	7660	6410	1.0000	.9820	• 9264	.9191	1.0112	1.0000
1.050	.2285+89	. 9894	1.6663	.8863	.4587	.7469	-6163	9982	.9792	.9214	.9116	1.0143	1.0002
1.100	.223E+09	.9892	1.6708	.8759	293	.7278	-5921	9928	9762	9167	.984D	1.0179	1.0007
1.150	.226E+89	.9890	1.6749	.8653	.4013	.7088	.5694	9843	.9731	9124	.6963	1.0220	1.0015
1.200	.2285+09	.9888	1.6785	. 8544	.3747	.6899	.5454	.9732	•9697	9088	.8887	1.0269	1.0028
1.250	.230E+09	-9886	1.6816	8434	3497	.6713	.5231	9598	.9662	.9057	.8811	1.0325	1.0047
1.300	.231E+09	.9884	1.6842	.8322	.3260	-6529	.5015	9443	9627	9032	.8736	1.0386	1.0069
1.350	*535E+09	9882	1.6864	.8210	.3038	6349	.4698	.9273	-9591	.9015	.8663	1.0456	1.0099
1.400	.2335+09	.9880	1.6882	.8098	.2829	.6171	4696	9088	9554	.9002	8591	1.0530	1.0132
1.450	.233E+09	.9879	1.6897	.7986	.2633	-5998	.4413	8892	.9518	.8996	.8529	1.0613	1.0172
1.509	.234E+09	.9877	1.6909	.7873	. 2451	.5829	4227	.8687	.9481	8997	.8452	1.0701	1.0218
1.550	+233E+09	.9876	1.6918	.7762	.2281	-566₹	4049	.8478	9445	•9006	8385	1.0799	1.0272
1.600	.2335+09	9875	1,6925	.7652	2122	5503	.3878	.8263	.9409	.9021	.8320	1.0902	1.0330
1.650	.232E+09	.9874	1.6929	.7542	.1974	.5346	3714	.8043	9373	.9041	.8257	1.1011	1.0394
1.700	.2325+09	9872	1.6933	7434	.1837	.5194	.3557	.7822	.9338	9866			
1.750	.231E+89	.9871	1.6935	7327	•1709	.5846	•3407	.7602	9304	• 90 99	.8196 .8137	1.1125 1.1249	1.0463 1.0540
1.800	.2305+09	9971	1.6936	7222	.1590	.4982	•3263	.7381	.9271	.9137	.8079		
1.850	.2295+09	9870	1.6917	7118	.1480	.4763	• 3126	7162	.9238	.9137		1.1376	1.0622
1.900	•227E+09	9869	1.6937	.7016	.1377	4628	•3176 •2994	•6946	•9206		.8024	1.1511	1.0709
1.950	.226E+09	.9868	1.6936	6915	1282	4497	• 2869	.6733		.9229	.7970	1.1651	1.0802
2.000	.2245+09	.9868	1.6935	.6817	1194	.4371	•2749		9175	4 92 84	.7918	1.1798	1.0902
		4,000	240774	1001	# 4 4 7 **	44311	ac 7 47	• 6522	•9145	9343	.7867	1.1949	1.1005

		p. toom inces.		
MACH	LCCAL ISENTROPIC	VISCOSITY	THERMAL CONDUCTIVITY	PRANDTL
	EXPANCION COEFF.	G/CM-SEC	CAL/GM-SEC-K	NUMBER
0.000	I	•36269F- 0 4	.14635E-03	.7009
.050	1.5689	.36182E-04	.14775E-03	.7099
.100	1.5576	• 36125E-04	.14736E-03	.7009
.150	1.5683	.360302-04	.14671E-03	.7009
.200	1.5654	•35899E÷04	•14581E-03	.7010
. 250	1.5663	.35730E-04	•14465E-03	.7011
•30D	1.5749	•35525E-84	•14325E-03	.7013
.350	1.5729	• 352 84E− 1 4	.14181E-03	.7006
-400	1.5753	.35007E-84	•14030E-03	•6992
•450	1.5898	.34697E-04	.13862E-03	.6977
•500	1.5876	•34353E+04	.13676E-03	.6961
• 550	1.5903	.33977E-04	.13473E-03	. 6946
.600	1.5965	.33572E-04	.13255E-03	•6932
•650	1.6010	• 331 37E-04	•13023E-03	•6919
.700	1.6097	.32676E-04	.12778E-03	.6907
• 750	1.6113	•32190E÷04	•12522E-03	.6898
. 800	1.6204	.31681E-84	.12255E-03	.6891
•85D	1.6272	.31153E-04	•1: 990E+03	.6883
• 900	1.6312	.30608E-04	1::/ *23E=03	•6874
• 95 O	1.6344	.30049E-04	.11/251E-03	.6870
1.000	1.6435	•29478E-84	•11174E-03	.6869
1.050	1.6477	.28897E-04	.10895E-03	•6872
1.100	1.6502	.28311E-04	.10616E-03	.6879
1.150	1.6536	.27721E-04	•10336E+03	.6891
1.200	1.6583	•27129E-04	•99962E-04	•6948
1.250	1.6620	.26537E-04	.97407E-04	•6954
1.300	1.6628	.25948E-04	• 94892E-04	•6961
1.350	1.6671	.25363E-04	•92425E-04	.6970
1.400	1.6652	.24782E-04	•90009E-04	•6980
1 • 450	1.6684	.24208E-04	.87646E-04	.6991
1.500	1.6685	.23641E-04	+65312E-04	.7005
1.550	1.6727	.23081E-04	•83097E-04	.7021
1.600	1.6713	•22531E-04	-80556E-04	.70 56
1.650	1.6699	•21989E-04	.78406E-04	.7070
1.700	1.6698	.21456E-04	.76316E-04	.7884
1.750	1.6732	·20934E-04	•74286E-04	•7096
1.800	1.6708	.20421E-04	•72315E-04	.7108
1.850	1.6717	•19918E-04	•70484E+84	.7119
1.900	1.6706	.19425E-04	.68548E-84	.7129
1.957	1.6728	•16943E-114	.66749E-04	.7138
2.000	1.6694	•18472E-04	•65005E-04	.7146

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POOR QUALITY

TABLE III. REAL-GAS ISENTROPIC EXPANSIONS OF PARAHYDROGEN

E. IT = 100.0 K PT = 5.0 ATM RHOT = .1235-02 G/CM3 SVT = 774.990 M/SEC

MACH			₹. ₹	T = 100.0 K	PT =	5.8 ATM	RHOT =	.1235-02	G/CM3	SVT = 774	.990 M/S	EC		
. 1125-08	MACH	REZM	Z	CP/CV	SV/SVT	P/PT	7/11	RHOZRHOT	A*/A			T/TT TO IDEAL	RHO/PHOT GAS VALUES	
. #850	ស.សភភ	0.	.9987	1.4584	1.0900	1.0000	1.0000	1.0000	0.0000	1.0000	1.0000	1 . 0000	-1.0000	1.0000
100 274_6406	.850	·112E+88	.9987	1.4600										
150	.100	.224E+86	.9987	1.4607	.9992									
.280	•15:D	.334E+08	.9987	1.4618		.9838								
.250	•200	-442E+88	. 9986	1.4635	• 9966	.9713	.9911							
.300	·250	.5475+88	.9985	1.4656	9947	.9557								
.350 .7777408 .9983 1.4773 .9898 .9151 .9727 .9411 .5604 1.0018 .9965 .9999 .9966 .400 .81616 .9887 1.4750 .9867 .8999 .9644 .424 .626 1.0023 .9947 .9955 .9999 .9969 .9869 .4980 .9316408 .9381 1.4792 .9872 .8661 .9552 .0852 .6884 1.0029 .9929 .9939 .9997 .9972 .550 .1016109 .9978 1.4891 .9750 .880-9 .9337 .8629 .7954 1.0041 .5887 .9910 .9994 .9982 .600 .1176409 .9977 1.4950 .9704 .7731 .9215 .8399 .8405 1.0041 .5887 .9912 .9994 .9982 .600 .1176409 .9977 1.4950 .9704 .7731 .9215 .8399 .8405 1.0041 .9887 .9912 .9994 .9982 .7700 .1296409 .9973 1.51083 .5500 .7061 .6945 .7700 .9841 .0055 .9930 .9996 .700 .1296409 .9973 1.51083 .5500 .7061 .6945 .7700 .9131 .0055 .9363 .9552 .9990 .9996 .700 .1356409 .9975 .15154 .9544 .6372 .8624 .7386 .9630 1.0070 .9735 .9736 .9821 .9987 .9993 .9996 .8000 .1466409 .9976 .15574 .9416 .6072 .8880 .7706 .9630 .0070 .9736 .9736 .9737 .9984 .9998 .9990 .9990 .1466409 .9976 .15584 .9946 .6072 .8880 .7706 .9630 .0070 .9736 .9736 .9737 .9984 .9998 .9990 .9900 .1466409 .9966 .1.5514 .9348 .5665 .8880 .7736 .9630 1.0070 .9713 .9746 .9982 .9990 .9900 .1676409 .9964 1.5514 .9348 .5665 .8810 .6859 .9979 1.0076 .9614 .9665 .9705 .9977 .9984 .9996 .9900 .1572409 .9964 1.5514 .9348 .5665 .8880 .9712 .9766 .9077 .9066 .9077 .9077 .9071 .1000 .1576409 .9961 1.5504 .9199 .5070 .8136 .6659 .9979 1.0076 .9614 .9667 .9977 1.0000 .1576409 .9961 1.5704 .9060 .9060 .7733 .6669 .9979 1.0076 .9614 .9667 .9977 1.0000 .1576409 .9961 1.5704 .9060 .9060 .7733 .6669 .9979 1.0070 .9960 .9960 .9961 1.5704 .9060 .9	.300	.649±+DR	. 9984	1.468?	•9925	.9367	.9799							9959
.400 .8-15-08 .9987 1.4-750 .9867 .8919 .9644 .9242 .6769 1.0023 .9947 .9957 .9959 .9956 .950 .930E-08 .9981 1.4-792 .9832 .86-1 .9552 .684 1.0029 .9929 .9939 .9937 .9937 .5500 .101E-09 .9930 1.4-839 .9937 .8354 .9449 .8848 .7447 1.0035 .9910 .9922 .9996 .9977 .5500 .101E-09 .9978 1.4-991 .9750 .80-9 .9337 .8548 .9449 .8848 .7447 1.0035 .9910 .9922 .9996 .9977 .5500 .101E-09 .9978 1.4-991 .9750 .80-9 .9337 .8354 .9449 .8848 .7447 1.0035 .9910 .9822 .9996 .9977 .9500 .117E-09 .9978 1.4-9910 .9750 .80-9 .9337 .8354 .8399 .8405 1.0047 .9867 .9902 .9994 .9987 .9987 .9987 .9987 .9987 .9987 .9987 .9987 .9987 .9987 .9988 .9998 .9988 .9998 .9	•350°	.7475+08	.9983	1.4713	•9898	•9151	.9727							
.450 .930E+98 .9981 1.4792 .9872 .8661 .9552 .985 .6884 1.0029 .9929 .9939 .9937 .9972 .5550 .100E+99 .9940 1.4839 .9753 .8354 .9449 .9327 .8629 .7954 1.0035 .9910 .9922 .9996 .9977 .5550 .100E+99 .9977 1.9E10 .9775 .888.9 .9337 .8629 .7954 1.0041 .9887 .9902 .9994 .9982 .9966 .117F+99 .9977 1.9E10 .9774 .9215 .8399 .8405 1.0047 .9861 .9876 .9993 .9987 .700 .127E+99 .9973 1.5883 .9500 .70E1 .8945 .7905 .9131 1.0059 .9795 .9821 .9987 .9993 .9990 .9990 .9990 .179E+09 .9973 1.5883 .9560 .70E1 .8945 .7905 .9131 1.0059 .9795 .9821 .9987 .9993 .8888 .100E4 .9976 .9976 .9978 .9993 .8888 .100E4 .9976 .9976 .9978 .9998 .8888 .100E4 .9976 .9978 .9998 .8888 .100E4 .9976 .9976 .9978 .9998 .8888 .100E4 .9976 .9976 .9978 .9998 .9996 .9997 .9998 .99	•40 N	·8+1E+08	.9982	1.4750	.9867	.8909		.9242						
.5500	•450	.930E+98	.9981	1.479?	.9832	.8641	.9552							
.550 .106+09 .9978	.500	.1015+09	. 99 1 0	1.4839	.9793	·8354								9977
.600 .1177+09 .9977 1.9950 .9704 .7731 .9215 .8399 .8405 1.00.7 9861 .9878 .9993 .9987 .700 .1298+09 .9973 1.5114 .9554 .7400 .9845 .8797 1.0053 .9830 .9552 .9990 .9990 .750 .1357+09 .9972 1.5154 .9542 .6718 .8797 .7005 .9131 1.0059 .9795 .9821 .9997 .9993 .9993 .800 .1402+09 .9970 1.5239 .9481 .8372 .6642 .7386 .9630 1.0070 .9713 .9748 .9982 .9998 .8500 .1402+09 .9970 1.5239 .9481 .8372 .6642 .7386 .9630 1.0070 .9713 .9748 .9982 .9998 .8500 .1402+09 .9963 1.5744 .9416 .6072 .6448 .8797 .7648 .9982 1.0076 .9665 .9705 .9978 .9998 .9998 .8500 .1402+09 .9964 1.5414 .9348 .6645 .8311 .6854 .9912 1.0076 .9665 .9705 .9978 .9998 .9998 .1572*09 .9964 1.5514 .9346 .6572 .6349 .8114 .6854 .9912 1.0076 .9614 .9657 .9977 1.0000 .9513 .9986 .1572*09 .9963 1.5504 .9199 .6324 .7975 .6324 1.0000 1.0077 .9502 .9546 .9977 1.0001 .055149 .9963 1.5704 .9964 .9968 .9977 1.0001 .1059 .1572*09 .9963 1.5704 .9964 .9978 .9999 .8136 .6589 .9979 1.0078 .9560 .9606 .9977 1.0001 .1059 .1572*09 .9963 1.5704 .9199 .5020 .7975 .6324 1.0000 1.0077 .9502 .9546 .9978 .9999 .11500 .1572*09 .9961 .9977 .9001 .9773 .5063 .9979 1.0078 .9560 .9606 .9978 .9999 .9999 .1572*09 .9965 1.5704 .9961 .9978 .9999 .9999 .1572*09 .9965 1.5704 .9965 .9978 .9999 .9999 .10078 .9968 .9977 1.0001 .00078 .9560 .9977 1.0001 .00078 .9966 .9978 .9999 .9999 .10078 .9969 .9969 .9977 1.0001 .00078 .9969 .996	•550	.109E+09	.9978	1.4891	.9750									9982
*650 *12724-09 *9975 1.5014 *9654 7.400 *9084 *8156 8797 1.0053 .0830 9852 9990 9990 7750 12984-09 9973 1.5083 9860 7061 88797 7648 9408 1.0065 9776 9787 9821 9987 9993 7550 13564-09 9970 1.5289 9461 6.672 *662 77866 9630 1.0070 9713 9748 9992 9996 9996 1.5274 9416 60726 8480 7121 9776 1.0076 9614 9665 97705 9978 9998 9990 9900 1.4852409 9966 1.5414 9348 5668 87121 9776 1.0076 9614 9665 97705 9977 1.0000 1.528240 9966 1.5414 9348 5668 87121 98766 9912 1.0076 9614 9667 9977 1.0000 1.0000 1.552409 9966 1.5414 9348 5668 87121 98766 9912 1.0076 9614 9657 9977 1.0000 1.0000 1.552409 9963 1.5500 9919 5020 7957 6324 1.0000 1.0077 9502 9548 9976 1.0000 1.576409 9963 1.5703 9919 5020 7957 6324 1.0000 1.0077 9502 9548 9976 1.0000 1.576409 9961 1.5703 9919 4.700 7773 6603 9979 1.0077 9502 9548 9976 1.0000 1.576409 9950 1.5802 9936 4.494 7586 5809 9927 1.0077 99502 9548 9976 1.0000 1.526409 9950 1.5802 9936 4.494 7586 5809 9927 1.0007 9950 1.5000 9950 1.5802 9956 1.5902 9956 1.5902 9956 1.5903 8000 9977 1.0000 1.0077 99502 9548 9976 1.0000 1.5007 9950 9950 1.5000 9950 1.0000 1.2000 1.3000 9950 1.5000 9950 1.5000 9950 1.5000 9950 1.0000 1.3000 9950 1.0000 1.3000 9950 1.0000 1.3000 9950 1.0000 9950 1.0000 9950 1.0000 9950 1.0000 9950 1.0000 9950 1.5000 9950 1.5000 9950 1.5000 9950 1.0000 9950 9950 9950 9950 9950 9950 9950	.600	•117F+D9	. 9977	1.4950	.9704	.7731								
.700 .1278E+09 .9973 1.5183 .9500 .7061 .8945 .7005 .9131 1.0059 .9705 .9821 .9907 .9908 .750 .115E+09 .9972 1.5158 .9542 .6718 .8797 .7648 .9408 1.0065 .9756 .9787 .9984 .9998 .800 .140E+09 .9970 1.5239 .9481 .6372 .7836 .9630 1.0070 .9713 .9748 .9982 .9998 .850 .140E+09 .9968 1.5774 .9416 .6076 .8481 .7121 .9796 1.0070 .9713 .9748 .9982 .9998 .800 .140E+09 .9966 1.5744 .9416 .6076 .8481 .7121 .9796 1.0076 .9614 .9657 .9977 1.0000 .950 .157E+09 .9964 1.5507 .9275 .5349 .8136 .6589 .9912 1.0076 .9614 .9657 .9977 1.0001 .0556 .9978 .9998 .157E+09 .9961 1.5703 .9119 .4700 .7773 .6063 .9979 1.0078 .9560 .9657 .9978 .9998 .157E+09 .9961 1.5703 .9119 .4700 .7773 .6063 .9979 1.0077 .9502 .9946 .9976 1.0001 .155E+09 .9959 1.5802 .9936 .4374 .7586 .5809 .9973 1.0077 .9502 .9946 .9978 .9999 1.150 .161E+09 .9959 1.5802 .9936 .4374 .7586 .5809 .9973 1.0077 .9381 .9422 .9985 1.0001 .250 .161E+09 .9956 1.5902 .9353 .9994 .0004 .250 .161E+09 .9956 1.5902 .8764 .3352 .7006 .5315 .9711 1.0053 .9320 .9353 .9994 1.0004 .250 .163E+09 .9956 1.5902 .8764 .3352 .7006 .5315 .9711 1.0053 .9320 .9353 .9994 1.0006 .250 .163E+09 .9951 1.6022 .8764 .3552 .7015 .5081 .9567 1.0040 .9221 .9207 1.0027 1.0016 .250 .163E+09 .9951 1.6022 .8667 .3301 .8625 .4636 .9215 1.0007 .9996 .9055 1.0027 1.0016 .250 .163E+09 .9951 1.6022 .8667 .3301 .663E-0 .9951 1.6022 .8667 .3301 .865E-0 .4636 .9215 1.0007 .9996 .9055 1.0032 1.0035 1.400 .164E-0 .9951 1.6533 .8147 .2221 .5910 .8659 .4636 .9215 1.0007 .9996 .9055 1.0032 1.0055 1.400 .164E-0 .9948 1.6044 .8360 .2639 .6636 .4636 .9215 1.0007 .9996 .9055 1.0032 1.0035 1.400 .164E-0 .9948 1.6644 .9948 1.6644 .9048 .8594 .9939 .8897 .8895 1.0022 1.0055 1.400 .164E-0 .9944 1.6533 .8147 .2221 .5911 .3866 .8574 .9988 .8594 .9939 .8896 .8593 .8996 .8055 1.0028 1.0055 1.0055 1.0056 .8947 .8668 1.0044 1.0235 1.6600 .162E-0 .9944 1.6659 .7702 .8163 .8949 .9940 1.6673 .7701 1.6673 .7701 .16673 .7701 .16673 .7701 .1658 .99	•650	•123E+09	.9975	1.5014	• 9654	.7+08								
.750 .1356.09 .9972 1.5158 .9942 .6718 .8797 .7648 .9408 1.0065 .9756 .9787 .9964 .9995 .800 .1405409 .9970 1.5573 .9810 .6372 .6642 .7386 .9630 1.0070 .9713 .9748 .9982 .9998 .850 .1455409 .9968 1.5774 .9416 .6372 .8642 .7386 .9630 1.0070 .9713 .9748 .9982 .9998 .900 .1485409 .9968 1.5774 .9416 .6575 .8311 .6854 .9912 1.0076 .9614 .9657 .9977 1.0000 .1575409 .9963 1.5504 .9199 .5026 .7957 .6324 1.0000 1.0077 .9560 .9605 .9977 1.0001 .0000 .1575409 .9963 1.5504 .9199 .5026 .7957 .6324 1.0000 1.0077 .9562 .9548 .9976 1.0000 1.0077 .9562 .9548 .9976 1.0000 1.0077 .9562 .9548 .9976 1.0000 1.0077 .9562 .9548 .9976 1.0000 1.0077 .9562 .9548 .9976 1.0000 1.0077 .9562 .9548 .9976 1.0000 1.0077 .9562 .9548 .9976 1.0000 1.0077 .9562 .9548 .9978 .9999 1.1500 .1575409 .9951 1.5802 .9159 .4700 .7773 .6053 .9979 1.0075 .9441 .9487 .9978 .9999 1.1500 .15615409 .9955 1.5802 .9136 .4304 .7586 .5809 .9923 1.0071 .9381 .9422 .9985 1.0002 1.250 .1552409 .9956 1.5994 .8859 .4304 .7586 .5809 .9923 1.0073 .9320 .9353 .9994 1.0002 1.250 .1552409 .9956 1.5994 .8859 .4809 .7397 .5558 .9832 1.0063 .9320 .9353 .9994 1.0004 1.250 .15615409 .9956 1.5994 .8859 .4866 .3562 .4848 .9401 1.0053 .9258 .9281 1.0007 1.0066 1.250 .15616409 .9956 1.5994 .88567 .3858 .8859 .9832 1.0053 .9320 .9353 .9994 1.0006 1.250 .1652409 .9956 1.5802 .8764 .3552 .7015 .5081 .9567 1.0040 .9221 .9207 1.0027 1.0014 1.300 .1632409 .9951 1.6092 .8764 .3552 .7015 .5081 .9567 1.0040 .9221 .9207 1.0027 1.0014 1.300 .1632409 .9951 1.6092 .8667 .3858 .6636 .4636 .9215 1.0007 .9906 .9055 1.0022 1.0056 1.400 .1642409 .9950 1.6343 .8465 .2845 .66450 .4428 .9016 .9916 .9957 1.0027 .9016 .9055 1.0024 1.0056			.9973	1.5083	.9500									
*800					• 9542	.6718	.8797	.76+8						
.850 .145E+09 .9968 1.5714 .9416 .6076 .8480 .7121 .9796 1.0076 .9614 .9665 .9705 .9978 .9998 .900 .145E+09 .9966 1.5814 .9348 .5685 .8311 .6854 .9912 1.0076 .9614 .9657 .9977 1.0000 .155E+09 .9963 1.5504 .9199 .5020 .7957 .6324 1.0000 1.0077 .9502 .9958 .9976 1.0000 .155E+09 .9963 1.5504 .9199 .5020 .7957 .6324 1.0000 1.0077 .9502 .9986 .9976 1.0000 .157E+09 .9961 1.5703 .9119 .4700 .7773 .6063 .9979 1.0077 .9502 .9986 .9976 1.0000 .157E+09 .9951 1.5802 .9936 .4394 .7586 .5809 .9923 1.0076 .9441 .9457 .9978 .9999 1.200 .157E+09 .9957 1.5901 .8949 .4909 .7787 .5558 .9032 1.0075 .9441 .9457 .9978 .9999 1.200 .157E+09 .9957 1.5901 .8949 .4909 .7787 .5558 .9032 1.0075 .9441 .9457 .9978 .9999 1.200 .157E+09 .9957 1.5901 .8949 .4909 .7397 .5558 .9032 1.0063 .9320 .9353 .9994 1.0002 1.200 .162E+09 .9956 1.599 .8858 .3818 .7206 .5315 .9711 1.0053 .9320 .9353 .9994 1.0004 1.200 .162E+09 .9956 1.509 .8858 .3818 .7206 .5315 .9711 1.0053 .9328 .9281 1.0007 1.0006 1.350 .163E+09 .9951 1.6092 .8764 .3552 .7015 .5081 .9567 1.8040 .9261 .9207 1.0027 1.0014 1.350 .164E+09 .9953 1.6182 .8667 .3881 .5626 .4854 .9401 1.0025 .9147 .9131 1.0052 1.0024 1.350 .164E+09 .9951 1.6265 .8667 .3865 .2865 .6636 .4858 .9215 1.0007 .9996 .9055 1.0002 1.0036 1.460 .9987 .9987 .9987 .9983 .9978 1.0024 1.400 .164E+09 .9948 1.6265 .2865 .2865 .6650 .4428 .9010 .9987 .9987 .9053 .9978 1.0122 1.0035 1.450 .164E+09 .9948 1.6543 .8465 .2865 .6650 .4428 .9010 .9987 .9987 .9053 .9978 1.0122 1.0035 1.450 .164E+09 .9948 1.6544 .8360 .2639 .6266 .4229 .8811 .9964 .9916 .9955 1.0022 1.0036 1.550 .164E+09 .9948 1.6573 .8147 .2711 .5911 .3858 .8373 .9913 .8966 .8751 1.0289 1.0185 1.500 .164E+09 .9948 1.6582 .8039 .2106 .5740 .3685 .8148 .9885 .8985 .8985 .8985 .8085 .8085 .10224 1.0188 1.550 .164E+09 .9944 1.6582 .8039 .2106 .5740 .3685 .8148 .9885 .8985 .8985 .8985 .8083 1.0285 .10285 .10285 .10285 .10285 .10289 .10285 .10286					• 9481	.6372	·#642	.7386	.9630					
900					• 9416	.6026	•8487	.7171		1.0074				
.950			.9966	1.5414	. 9348	-5685	.8311	+6854	.9912	1.0076				
1.000					•9275	•5349	.8136							
1.050			-		. 9199	•5020	.7957	. 6324		1.0077				
1.100 .1595+09 .9959 1.580? .9036 .4394 .7586 .5809 .9923 1.8070 .9381 .9422 .9985 1.0002 1.250 .1615+09 .9956 1.5994 .8850 .3818 .7206 .5515 .98132 1.0063 .9258 .9281 1.8007 1.0006 1.250 .1635+09 .9954 1.6092 .8764 .3552 .7015 .5081 .9567 1.8004 .9201 .9207 1.0027 1.0007 1.3500 .1635+09 .9953 1.6182 .8667 .3301 .6825 .4854 .9401 1.0025 .9147 .9131 1.0052 1.0024 1.350 .1645+09 .9951 1.6726 .8567 .3865 .6450 .4458 .9215 1.8007 .9096 .9055 1.8002 1.0036 1.480 .1645+09 .9950 1.6343 .8465 .2845 .6650 .4428 .9016 .9987 .9053 .8978 1.0122 1.0036 1.450 .1645+09 .9948 1.6414 .8360 .2639 .6266 .4229 .8811 .9964 .9016 .8901 1.0169 1.0079 1.550 .1635+09 .9947 1.6477 .8254 .2448 .6086 .4038 .8594 .9939 .8967 .8825 1.0224 1.0188 1.550 .1635+09 .9946 1.6533 .8147 .2271 .5911 .3858 .8373 .9913 .8966 .8751 1.0289 1.0145 1.550 .1615+09 .9944 1.6582 .8039 .2106 .5740 .3685 .8148 .9985 .8992 .6678 1.0289 1.0167 1.700 .1605-09 .9942 1.6669 .7822 .8133 .9456 .8574 .9856 .8947 .8608 1.0440 1.0235 1.750 .1615+09 .9942 1.6669 .7822 .1813 .5941 .3366 .7694 .9826 .8950 .8539 1.0529 1.0733 1.0029 1.750 .1566+09 .9940 1.6714 .7607 .1563 .5103 .3078 .7245 .9765 .8963 .8473 1.0627 1.0355 1.000 .1566+09 .9940 1.6714 .7607 .1563 .5103 .3078 .7245 .9765 .8983 .8409 1.0733 1.0425 1.900 .1566+09 .9938 1.6734 .7500 .1455 .9940 .9939 .16774 .7807 .1563 .5103 .3078 .7245 .9765 .8983 .8409 1.0733 1.0425 1.900 .1566+09 .9938 1.6734 .7500 .1455 .9940 1.6714 .7607 .1563 .5103 .3078 .7245 .9765 .8983 .8409 1.0733 1.0425 1.900 .1566+09 .9938 1.6734 .7500 .1455 .9940 1.6714 .7607 .1563 .5103 .3078 .7245 .9765 .8983 .8409 1.0733 1.0425 1.900 .1566+09 .9938 1.6763 .7291 1.155 .48676 .2945 .7024 .9735 .9011 .8348 1.00846 1.0580 1.0580 .1556+09 .9938 1.6763 .7291 1.155 .48676 .2945 .7024 .9735 .9011 .8348 1.0084 1.0580 1.0580 .1566+09 .9938 1.6763 .7291 1.1555 .48676 .2945 .7024 .9735 .9011 .8348 1.00846 1.0580 1.0580 .1556+09 .9938 1.6763 .7291 1.1555 .48676 .2945 .7024 .9735 .9011 .8348 1.00846 1.0580 1.0580 .1556+09 .9938 1.6763 .7291 1.1555 .48676 .2945 .			.9961	1.5703	•9119	.4700	.7773		.9979	1.0075				
1.250		.159E+N9	•9953	1.5802	•9736	·4394	.7586	.5809						1.0002
1.250			.9957	1.5901	.8949	•+899	.7397	.5558						
1.250			• 9956	1.5094	• 885A	.381R	.7206							
1.350			.9954	1.6092	.8764									
1.350			.9953	1.6182	.8667	. Z Z N 1	6825							
1.400			.9951	1.6265	.8557									
1.458					.8465	. 2845								
1.500		.1645+09	.9948	1.6414	•836D	• 2639	.6266	.4229						
1.550			.9947	1.6477	.8254	.2 +4 8	.6086							
1.600			. 9946	1.6533	-8147	.2271	.5911	.3658						
1.650		.162F+09	. 9944	1.6582	.8039	.2106								
1.700		•161E+09	.9943	1.6624	.7931									
1.750 .159E+09 .9941 1.6689 .7714 .1683 .5255 .7219 .7469 .9796 .8963 .8473 1.0627 1.0355 1.800 .158E+09 .9940 1.6714 .7607 .1563 .5103 .3078 .7245 .9765 .8983 .8409 1.0733 1.0425 1.850 .157E+09 .9940 1.6734 .7500 .1453 .4956 .2945 .7024 .9735 .9011 .8348 1.0846 1.0502 1.900 .156E+09 .9939 1.6750 .7395 .1350 .4813 .2818 .6806 .9704 .9046 .8289 1.0967 1.0586 1.950 .1555+09 .9938 1.6763 .7291 .1255 .4676 .2698 .6593 .9674 .9088 .8232 1.1095 1.0676		.160E+09	. 9942	1.6659	.7822	-1813	.5411							
1.800		.159E+09	.9941	1.6689										
1.850		.158E+69	. 9948	1.6714										
1.900 .156E+09 .9939 1.6750 .7395 .1350 .4813 .2818 .6806 .9704 .9046 .8289 1.0967 1.0586 1.950 .1555+09 .9938 1.6763 .7291 .1255 .4676 .2698 .6593 .9674 .9088 .8232 1.1095 1.0676		•157E+09	.9941	1.6734	.7500									
1.950 .1555+09 .9938 1.6763 .7291 .1255 .4676 .2698 .6593 .9674 .9088 .6232 1.1095 1.0676		.156E+09												
0 000 10 mon 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1.950	.1555+09	.9938	1.6763										
	5.100	·154E+09	.9977	1.6773	.7188	.11£8								

TABLE III. REAL-GAS ISENTROPIC EXPANSIONS OF PARAHYDROGEN

E. (CONTINUED)

MACH	LOCAL ISENTROPIC EXPANSION COEFF.	VISCOSITY G/CM~SEC	THERMAL CONDUCTIVITY CAL/CH-SEC-K	PRANDTL NUMBER
		3. 01. 000	ones on See R	MOTION EN
0.000	Ī	.42520E-04	.19456E+D3	.7892
• 950	1.4886	•424256-84	.19368E+03	.7093
.109	1.4553	.42373E-04	.19327E-03	.7092
.150	1.4603	• 422 55E=04	•19258E-03	.7089
.200	1,4573	.+2163E+04	.19162E+03	.7086
.250	1.4667	.42006E-04	.19040E-03	.7082
.300	1.4603	.41815E-84	.18891E-93	.7076
•350	1.4681	.4159DE+04	.18716E-B3	.7070
•400	1.4737	.41332E-04	.18516E-03	.7064
• 450	1.4720	.41040E-O+	•18290E-03	.7056
.500	1 • 4791	.40715E-04	•18049E-83	.7048
•550	1.4835	.40358E-04	•17767E-03	.7840
•600	1.4909	.3997NE-04	•17471E-03	.7032
•659	1.4932	.39551E-04	•17153E-03	.7024
.700	1.5005	.39102E-04	•16815E-03	.7017
.751	1.5079	. 38 62 3E-114	-16466E-13	.7007
• ៩៦០	1.5162	.38117E-04	.16106E-03	-6995
.850	1.5224	.375842-84	.15729E-03	.6985
•900	1.5328	.37029E-04	•15337E-03	.6978
- 95 0	1.5+20	.36443E+04	-14932E-03	.6974
1.000	1.5489	.35839E-04	•14516E-03	•6974
1.050	1.5584	• 3521 52 -0 4	•14092E-03	.6978
1.100	1.5715	• 34574E-04	·13741E-03	•6946
1.150	1.5782	"3 3919 E-84	•13386E-03	•6919
1.200	1.5867	. 33253E-04	.13028E-03	.6896
1.250	1.5992	.325795-04	.12669E-03	.6878
1.390	1.6065	•31900E-04	•12311E-03	.6866
1.350	1.6122	•31218E-84	•11958E-03	•6859
1 + 400	1.6248	.30539E-04	-11623E-03	•6849
1.450	1.6299	.29861E-04	•11291E-03	•6845
1.500	1.6354	.29169E-04	•10966E-03	-6847
1.550	1.6427	.285255-04	.10648E-03	.6854
1.600	1.6.57	.2787DE-D4	.10337E-03	-6866
1.650	1.6493	.27225E-04	.10034E-03	.6861
1.700	1.6549	• 26 592E+114	•97222E-04	•6913
1.750	1.6584	.25971E+04	.94571E-04	.6921
1.600	1.6601	•25361E-04	•92007E-04	.6930
1.850	1.6630	·24765E-N4	•89527E-04	.6941
1.900	1.6638	.?4181E+04	.87129E-04	•6953
1.950	1.6652	•23611E-04	-84796E-04	•6966
5 • 000	1.6655	.23052E-04	.82516E-84	•6982

MANAGE ROLL OF THE PARTY HAVE BEEN AND THE PARTY HAVE

MALITANCE TO SUMPLIES

TABLE III. REAL+GAS ISENTROPIC EXPANSIONS OF PARAHYDROGEN

		F. TT	= 200.9 K	PT =	5.0 ATM	유 버 0▼ =	.617E-03	S/CH3	SVT =1057	.808 M/S	EC		
MACH	PE/M	7	CP/CV	SV/SVT	P/FT	7/11	RHO/RHOT	A*/A	TVZVZ	P/PT FELATIVE	TO IDEAL	RHO/RHOT	A*/£
0.000	θ.	1.0033	1.3478	1.0000	1.0000	1.0000	1.0000	0.0000	1.0000	1.0000	1.0000	4 0000	4 0000
.050	.4735+07	1.0033	1.3475	. 9998	9993	9996	9997	.0859	1.0000	1.0000	1.0000	1.0000	1.0000
.100	.943E+07	1.0033	1.3474	. 9991	.9932	.9983	9949	.1711	1.0001	1.0002	1.0003	•9999 •9999	.9961
•150	*141E+D8	1.0033	1.3472	9979	9858	9961	-9889	.2548	1.0001	1.0006	1.0005	1.0000	.9961
.280	.186±+09	1.0032	1.3479	.9962	.9775	.9931	9803	.336?	1.0002	1.9010	1.0010	1.0000	•9963
.250	.230E+08	1.0932	1.3467	.9941	.9588	-9893	.9693	-4147	1.0003	1.0014	1.0016	.9999	•9963 •9964
.300	.273E+08	1.0031	1.3462	.9916	.9414	.9846	9563	4897	1.0005	1.0021	1.0024	•9999	
.350	•313E+08	1.0031	1.3458	•9886	.9213	.9792	9411	•5605	1.0007	1.0028	1.0032	• 9998	.9965
•400	•*52E+98	1.0039	1.3453	•945₹	8959	9731	9241	.5268	1.0009	1.0036	1.0042	.9998	•9966
•45D	.388F+08	1.9929	1.3447	9815	.8743	.9662	9052	.6882	1.0012	1.0046	1.0053	•9997	.9968
•500	•422E+08	1.0028	1.3442	-9773	.8479	9587	8849	.7443	1.0015	1.0058	1.0055	•9997	.9970
•55 D	.453E+08	1.0027	1.3435	.9728	.8198	.950=	8530	7949	1.0018	1.0069	1.0080		9973
•600	.4825+08	1.0026	1.3429	.9650	.7905	+9417	-8481	8798	1.0022	1.0063	1.0095	• 9996 • 9995	9975
.650	.508E+98	1.0925	1.3423	. 9628	.7600	932*	-6159	.8789	1.0027	1.0096	1.0111	• 9993	.9979
.700	.531E+08	1.0024	1.3416	. 9574	.7290	.9224	.7910	9125	1.0032	1.0112	1.0128	• 9993	9981
•750	.551E+08	1.0023	1.3410	.9517	•6972	.9121	.7653	9402	1.0038	1.0126	1.0126	•9990	• 9986
.808	•569E+08	1.0022	1.3405	.9457	•6653	.9013	.7390	9624	1.0045	1.0142	1.0167	•9967	.9989
•85N	•584E+08	1.0021	1.3399	9796	.6333	.8901	.7124	.9797	1.0052	1.0157	1.0187	•9983	•9992
.900	.596E+08	1.0019	1.7395	.9332	.6015	.8785	6856	9911	1.0059	1.0173	1.0208		. 9995
•950	.606±+08	1.0019	1.3391	9266	• 5698	.8666	-6585	9978	1.0058	1.0185	1.0231	•9979 •9971	•9999
1.000	+613E+08	1.0717	1.3389	« 9199	.5388	.8545	6316	1.0000	1.0077	1.0199	1.0254		.9999
1.050	.618E+08	1.0016	1.3387	.9130	.5083	.8420	6047	•9979	1.0086	1.0210	1.0277	• 9963	1.0000
1.199	.6215+D8	1.0015	1.3387	.9060	.4786	-8293	.5792	9919	1.0097	1.0220	1.0300	.9952 .9940	.9999
1.150	•622E+0B	1.0714	1.3389	.8989	-4498	8164	-5520	9823	1.0108	1.0227			.9997
1.200	•620I+08	1.0013	1.3393	.8917	. 4219	.8134	.5262	9693	1.0120	1.0231	1.0324 1.0348	• 9926	.9994
1.250	.6175+08	1.0012	1.3399	. 8844	.3952	.7982	.5012	95 37	1.0132	1.0236	1.0346	+9988	9988
1.300	•613E+08	1.0911	1.3486	.8771	3694	.7768	.4765	9354	1.0145	1.0235		9891	.9983
1.350	.607E+08	1.0010	1.3416	8597	3448	.7633	.4527	9150	1.0159	1.0235	1.0393 1.0415	• 9869 • 984.7	.9974
1.460	•599E+08	1.0009	1.3429	8623	.3213	7497	•+296	8928	1.0173	1.0226	1.0415	.9647	• 9964
1.450	.591E+08	1.0008	1.3445	. 85+8	,23at	.7361	.4072	.8688	1.0188	1.0214	1.0456	• 9822	.9954
1.500	•581E+08	1.0007	1.3464	.8+73	.2777	.7223	3855	.8434	1.0203	1.0196	1.0474	.9793	.9938
1.550	.571E+88	1.0887	1.3487	.8398	.2577	.7085	•7647	8171	1.0219	1.0175		.9760	•9920
1.600	.559E+08	1.0006	1.3514	.8323	.2387	6947	•3446	7906	1.0235	1.0148	1.0490	•9726	•9900
1.650	•547E+08	1.0005	1.3545	. 8249	.2209	-6888	.3254	.7622	1.0251	1.0113	1.0503	• 9688	.9877
1.780	.535E+08	1.0004	1.35R1	. 8174	.2041	•666A	-3069	.7341	1.0268		1.0514	• 9646	.9850
1.750	+522E+08	1.0904	1.3621	80 99	1884	.6528	.2895	.7062	1.0285	1.0073	1.0577	.9601	-9820
1.600	.509F+08	1.0003	1.3667	8025	.1737	6388	.2727	6779	1.0302	1.0031 .9979	1.0527 1.0528	•9557	.9791
1.850	•496E+D8	1.0003	1.3717	.7950	.1599	-6248	2557	.6500	1.0319			•95û7	•9756
1.900	.482E+08	1.0902	1.3774	.7876	.1471	.6107	2416	.6224	1.0319	•9921	1.0525	9456	.9719
1.950	.469E+08	1.0802	1.3837	.7802	.1 351	•5967	.2272	.5951	1.0355	9857	1.0517	.9402	9680
5.000	.455E+08	1.0901	1.3906	.7729	1241	•5826	2136	•5684	1.0369	.9764	1.0504	.9344	.9636
			· -	• • • • •	* * * - *	*>0.E0	• : 100	• 200 4	1+0309	.9707	1.0487	.9286	• 95 92

F. (CONTINUED)

MACH	LOCAL ISENTROPIC	VISCOSITY	THERMAL CONDUCTIVITY	PRANDTL
	EXPANSION COLFF.	G/CM-SEC	CAL/CM-SEC-K	NUMBER
0.000	I	.68423E-0+	.37459E-03	.7027
.150	1.3387	.6828€E-94	.37403E-03	.7028
.100	1.3488	.68225E-04	.37378E-03	.7028
.150	1.3591	.68124E-04	•37337E+03	.7028
.200	1.3512	.67983E-04	.37280E-03	.7028
.250	1.3481	.67803E-04	.372n6E-N3	.7028
. 300	1.3512	.67586E-04	.37117E-03	7028
.350	1.3483	.67331E-04	•37814E+03	.7027
.400	1.3491	.67040E-04	.36896E-03	.7027
.450	1.3485	.66716E-D4	•36764E-03	.7026
.500	1.3499	.66358E-04	.36620E-93	.7024
.550	1.3465	.65969E-04	.36463E-03	.7021
.600	1.3482	.65550E-04	.36264E-03	.7024
•650	1.3455	.65102E-04	.35984E-03	.7039
.700	1.3475	-64678E-84	+35686E+03	.7055
.751	1.3445	.64129E-04	.35377E-93	.7070
.800	1.3445	.63608E-04	.35054E-03	.7086
• 850	1.3438	.63963E+B+	•34718E+03	.7100
900	1.3439	.62499E-84	.34371E-03	.7114
.95n	1.3409	.61917E-04	.34014E-03	.7126
1.000	1.3414	.61317E+84	•33649E-03	.7137
1.050	1.3409	.60700E-04	•33275E-03	.7146
1.100	1.3407	.60069E-04	•32 69 5E-03	.7152
1.150	1.3405	.59424E+04	•32508E+03	.7156
1.200	1.3390	.58767E-04	.32116E-03	.7157
1.250	1.3424	.58997E+04	.31719E-03	.7154
1.390	1.3424	.57416E-04	.31719E-03	.7147
1.350	1.3412	•56725E=04	.309145-03	.7137
1.400	1.3443	.56025E-04		•7122
1.450	1.3446	.5531FE-84	.30507E+03 .30097E+03	-7102
1.500	1.3446	•54597E+04	.29685E-03	.7077
1.550	1.3485	•53670E+04	• 29030E-03	
1.600	1.3509	• •		.7184
1.600		.53134E-84	.28370E-03	.7129
	1.3529	.52391E-04	.277085-03	.7149
1.7 1.750	1.3564	•51639E-04	.27045E+03	•7165
1.800	1.3622	.50880E+04	-26360E-03	.7178
1.859	1.3641	.50113E-04	.25714E-03	.7186
1 • 857 1 • 987	1.3701	.49338E-04	.25046E-03	.7190
1.90"	1.3757	•48555E=04	.24378E-03	.7190
	1.3800	.47765E-04	.23710E-03	.7185
2.000	1.3879	.46967E-04	.23041E-03	.7176

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TABLE III. REAL-GAS ISENTPOPIC EXPANSIONS OF PARAHYEROGEN

		` ∜ 5. ⊺	T = 300.0	K PT =	5.0 ATM	PHOT =	.409E-03	G/CM3	SVT =1313	.208 M/S	€ C		
MACH	95/4	?	CPZCV	TV2\VE	PVPT	1/11	RHOZRHOT	A*/A	SV/SVT	P/PT	1/11	RHO/RHOT	A+/A
		-	0:724	247.361	* * * *	***	KAUF KAUT	м-/н				GAS VALUES	
										u C P w I T A C	. O IDEME	ONS VALUES	,
0.000	0.	1.0930	1.3782	1.0000	1.0000	1.8080	1.0000	0.0000	1.0000	1.9000	1.0000	1.0000	1.0000
•050	•298~+07	1.0770			• 9923	• 9995	.9987	.0863	1.0000	1.0000	1.0000	1.0000	1.0011
•10C	∗ 595€+07	1.0029		-	• 4932	•9981	.9951	-1720	1.0009	1.0002	1.0001	1.0001	1.0012
•15n	. 487E+07	1.0029			DALE	•9957	•9899	.2561	•9999	1.0002	1.0002	1.0001	1.0011
.200	•117E+08	1.8029			.9727	9923	.9802	.3378	• 9999	1.0002	1.0003	1.0000	1.0009
-250	•145 <u>€</u> +88	1.0029			• 9576	+9881	•9693	•4165	•9998	1.0002	1.0004	• 9999	1.0007
•300	•172E+08	1.0728			• 9399	•9830	•9563	.4916	.9997	1.0004	1.0007	• 9999	1.0007
•350	•197E+08	1.0028			• 91 04	•9771	9412	+5628	•9996	1.0006	1.00119	• 9999	1.0007
•400	*222E+03	1.0927			. 8965	.9701	•9243	•6293	.9995	1.0010	1.0012	1.0001	1.0007
•450	.245E+08	1.0926	1.3827	.9798	.8713	.9526	.9055	•6906	. 9994	1.0012	1.0015	1.0000	1.0005
.500	+256ä+08	1.0026			* 6 # r #	. 9542	.8852	.7467	•9993	1.0016	1.0019	1.0001	1.0004
•55 D	.286E+U9	1.0025	1.3813	.9702	.8159	•945?	.8636	.7972	•9992	1.0021	1.0024	1.0002	1.0074
•600	.3048+08	1.4974	1.3884	. 9549	.7860	•9356	.8496	.8418	.9990	1.0025	1.0029	1.0002	1.0003
•651	•321E+98	1.0923	1.3795	. 95 72	.7551	.9253	.4166	.8807	•9989	1.0031	1.0035	1.0002	1.0002
•700	*335E+08	1.0022	1.3784	.9531	.7235	.9146	.7917	.9137	.9988	1.0036	1.0042	1.0001	1.0000
.750	.3485+88	1.0022	1.3773	• 9468	•6915	.9833	.7661	•9+11	9986	1.0042	1.0049	1.0001	.9998
• 600	•359F+08	1.0021	1.3769	.9402	•65°3	.8916	.7401	.9629	.9985	1.0049	1.0057	1.0001	.9997
•650	•369E+08	1.0928	1.3747	.9332	.6272	.8796	.7138	.9795	.9984	1.8060	1.0067	1.0003	.9998
.900	•377E+08	1.0019	1.3733	.9251	.5954	.8672	.6873	•9910	9983	1.0070	1.0077	1.0004	. 99 98
• 95 0	.383E+0A	1.0015	1.3718	.9187	-56-1	.8545	.6608	-9978	•9982	1.0082	1.0088	1.0006	.9999
1.000	•388E+08	1.0017	1.3702	.9112	.5333	.8417	6344	1.0000	.9981	1.0095	1.0100	1.0006	1.0000
1.050	•39±£+88	1.0016	1.7686		• 50 to	.826€	-6981	.9960	.9981	1.0108	1.0113	1.0008	1.0000
1.100	. 393£+08	1.9815	1.3669	.8956	.4740	.8154	-5822	.9921	.9981	1.0121	1.0127	1.0008	1.0000
1.150	·3945+88	1.0015	1.3651	.8576	. 4457	.8021	•5565	.9827	9981	1.0134	1.0143	1.0007	.9999
1.280	.3935+88	1.0014			185	.788	-5314	9702	9982	1.0148	1.0159	1.0005	. 9997
1.250	.3925+08	1.0013	1.3613		.3924	.7754	51169	9552	.9983	1.0165	1.0177	1.0005	.9998
1.300	.769E+08	1.0012			.*675	.7621	4832	9378	9984	1.0183	1.0195	1.0005	1.0000
1.350	.3865+08	1.0012			•3436	.7486	4598	9179	•998€	1.0197	1.0215	1.0000	.9997
1.400	.3815+08	1.0011			.3210	.7353	.4373	8965	•998R	1.0214	1.0236	.9997	.9996
1-450	.376E+88	1.0010			2994	.7221	415-	.8734	•9990	1.0227	1.0257	9990	.9991
1.500	.370E+08	1.0009			.2790	.7989	3943	-8491	9994	1.0241	1.0280	•9982	.9967
1.550	.764E+08	1.0009			2597	6959	.3740	.8240	9998	1.0255	1.0303	.9975	.9983
1.600	.357E+08	1.0008	1.3480		.2416	.6838	7545	7980	1.0002	1.0268	1.0327	9964	.9977
1.650	.349E+08	1.0908			.2245	.6702	-3357	.7715	1.0007	1.0279	1.0351	9952	.9969
1.780	.347E+08	1.0007			2084	.6576	.3176	7444	1.0012	1.0285	1.0376	9935	.9957
1.750	.3334+08	1.9007		7869	.1933	6451	.3003	7173	1.0018	1.0291	1.0401	.9917	.9945
1.800	.3255+08	1.0006			1792	.6327	•2839	6902	1.0025	1.0295	1.0401	.9897	
1.850	.317E+08	1.0006			.1660	6205	2681	.6632	1.0025	1.0295	1.0427		.9932
1.900	.308E+08	1.0005			.1536	-6984	.2531	6365	1.0032	1.0295	1.8477	.9874	.9916
1.950	-299E+08	1.0005	1.3387		1421	.5965	.2388	.6100	1.0746	1.0288	1.0502	.9849	.9899 9870
2.000	.290E+08	1.0004			1313	5848	.2252	.5839	1.0016			.9821	.9879
	32352100	140004	¥ #UU	# 1 7 20	8 7 47 1	• 2 U - 1 1	47625	*2037	4.0020	1.0277	1.0526	.9788	.9854

G. (CONTINUED)

MACH	LOCAL ISENTROPIC	VISCOSITY	THERMAL CONDUCTIVITY	PRANDTL
	EXPANSION COEFF.	G/CM-SEC	CAL/CM-SEC-K	NUMBER
0.000	Ţ	.89665E-04	.4618DE-D3	.7100
.050	1.3858	.89681E-04	.46167E-03	.6899
.100	1.4008	.89593E-04	•46128E-03	.6900
.150	1.3869	. 8944 8E-84	.46064E-03	.690 0
.200	1.3850	.89245E-84	.45975E-03	.6901
.250	1.3846	.88987E-04	.45862E-03	6982
.380	1.3904	.88673E-04	.45724E-03	-6904
.350	1.3882	.88307E-04	.45564E-03	.6905
. 400	1.3901	.87890E-04	.45382E-D3	.6907
•4 5 0	1.3850	.87424E-84	.45179E-13	.6989
.500	1.3866	.86912E-04	.44957E-03	.6912
.550	1.3860	.86356E-04	.44716E-03	.6914
.600	1.3836	.65759E-04	•44458E-03	.6917
•650	1.3626	.85123E-04	.44190E-D3	.6920
.700	1.3803	.84452E-84	.43918E+03	•6922
.750	1.3801	.83747E-04	•43633E-03	6924
.800	1.3783	.83014E-04	.43337E-03	•6926
.850	1.3794	.82253E-84	.43032E-03	•6929
•900	1.3769	.81469E-04	.42719E-83	.6932
.950	1.3763	.80662E-84	.42396E-03	.6935
1.000	1.3743	.79838E-04	.42072E-03	.6939
1.050	1.3717	.78997E-04	-41741E-83	.6942
1.100	1.3699	.78144E-04	.41406E-03	-6946
1.150	1.3667	.77279E-84	.41068E-83	-6951
1.200	1.3652	.76405E-84	•40729E-03	•6955
1.250	1.3659	.75524E-04	.40382E-03	.6968
1.300	1.3639	.74638E-84	.40003E-83	-6971
1.350	1.3585	.7374 8E-04	.39625E-83	6981
1.400	1.3587	.72857E-84	.39246E+03	.6991
1.450	1.3548	-71965E-04	.38873E-03	•6999
1.500	1.3535	-71873E-04	•38500E-03	.7007
1.550	1.3526	.70183E-04	.38131E-03	.7013
1.600	1.3502	-692 95E-84	.37764E-03	.7016
1.650	1.3483	.68411E-04	•37402E-03	.7021
1.700	1.3451	.67530E-04	.37043E+03	.7023
1.750	1.3446	.66652E-04	.36688E-03	.7021
1.800	1.3439	.65780E-84	.36337E-03	.7916
1.850	1.3419	.64911E-84	.35841E-03	.7038
1.900	1.3419	-64048E-04	•35303E-03	.7066
1.950	1.3405	-63190E-04	.34771E-03	.7091
2.000	1.3389	.62336E-04	•34246E-63	.7112
			•	

Da room Quality

TABLE IV. REAL-GAS ISENTROPIC EXPANSIONS OF PARAHYDROGEN

		Δ. ΤΊ	= 40.0	K PT =	8.0 ATM	RHOT =	.566E+0?	G/CM3	SVT = 501	.370 M/S	EC		
MACH	RE/M	7	CP/CV	SV/SVI	P/PT	1/11	RHOZRHOT	A*/A	SV/SVT	P/PT	T/T T	RHOZRHOT	A+/A
							·					GAS VALUES	
0.000	0.	.8589	2.0436	1.0800	1.0000	1.0000	1.0000	0.000	1.0000	1.0000	1.0000	1.0000	1.0000
.050	.6405+08	.8680	2.0437	•9995	.9979	• 9991	.9986	•0900	.9997	• 9996	.9996	1.0000	1.0433
.100	+128E+19	.8578	2.0437	9979	. 9913	•9965	.9950	.1790	.9989	.9982	. 998 5	1.0000	1.0424
·150	•191E+89	.8676	2.0437	9953	.9885	.9921	.9888	• 2662	•9976	.9961	• 9966	1-8000	1.0410
.200	.2526+09	.8572	2.0437	.9918	<u>. 965 g</u>	.9861	.9814	.3507	.9957	. 9932	. 9940	1.0002	1.0392
•250	.3135+89	.9568	2.0436	.9872	• 9473	.9785	•9696	.4315	. 9934	.9894	.9907	1.0002	1.0368
•300	.371E+09	.8662	2.9435	-9818	.9255	•969₹	•9568	.5081	.9906	.9851	.9868	1.0004	1.0341
.350	.428E+09	.8655	2.0435	•9755	,9007	.9588	.9421	.5800	.9874	.9803	.9823	1.9908	1.0312
.400	.483E+09	.8650	2.0433	• 9684	6733	9469	•9255	•6465	.9838	.9750	.9772	1.0013	1.0280
•450	.535E+09	.8642	2.0430	•9606	-8436	•9339	.9073	.7072	.9799	9693	. 9717	1.0020	1.0245
•500	.585E+09	.8635	2.0427	• 9 521	.8124	9196	.8879	.7622	.9756	.9636	. 9657	1,0031	1.0212
•55 B	·632E+89	.8627	2.0422	• 9431	.7796	.9047	.8671	.8110	.9712	9576	.9594	1.0043	1.0177
•600	.E76E+89	.8619	2.0417	. 9334	.7461	•888B	.8454	.8538	•9665	9516	. 9528	1.0059	1.0144
•650	.718E+09	.8611	2.0412	.9234	.7128	•8723	.8229	.6906	.9616	9458	9460	1.0079	1.0114
-700	.757E+09	.8673	2.0405	.9129	+6777	.8551	.7997	9216	• 9566	.9401	9369	1.0103	1.0085
•75 D	•793E+09	. 85 95	2.0397	9122	. 6436	.8375	.7761	.9469	.9515	9346	.9317	1.0131	1.0060
.600	.8265+09	.6587	2.8403	.8913	•6196	.8195	.7520	.9670	.9467	. 9293	9244	1.0163	1.0039
.850	.857E+09	.8579	2.0409	•88 03	•5762	.8011	•7277	.9819	.9418	.9241	.9169	1.0198	1.0022
.908	.886E+09	.8571	2.0+17	.8691	• 5436	.7826	.7035	.9922	•9368	-9194	9094	1.0239	1.0010
•950	•912E+09	. 65-63	2.9474	.8577	.5120	.7648	.6793	.9982	.9319	.9152	.9019	1.0266	1.0003
1.000	.9352+89	.8556	2.0429	. 8462	. 4814	.7453	.6552	.9999	9270	.9112	. 8943	1.0336	9999
1.050	.9575+09	.8549	2.0433	.8347	.4521	.7267	•6317	9982	.9221	.9080	-8869	1.0395	1.0003
1.100	.976E+09	.8543	2.0435	.8231	-4240	.7082	-6984	.9932	.9173	.9053	.8795	1.0459	1.0011
1.150	•993E+09	,8537	2.0433	.8114	.3973	6898	-5856	.9853	9124	.9032	6723	1.0529	1.0025
1.200	.101E+10	.8531	2.0428	.7998	.3719	.6718	.5633	.9748	.9076	.9018	.8652	1.0605	1.0045
1.250	.102F+10	.8576	2.9428	.7881	.3479	6540	5416	.9622	9029	.9012	. 85 83	1.0690	1.0072
1.300	.1035+10	.8521	2.0409	.7766	.3253	6365	-5206	.9477	.8983	.9012	·8517	1.0789	1.0105
1.350	.104E+10	.8516	2.0394	.7651	3039	-6194	-5001	9314	.8937	.9019	.8452	1.0876	1.0143
1.400	.105E+10	.8512	2.8376	.7537	.2878	•6027	-4902	9137	8892	. 90 32	.8389	1.0979	1.0166
1.450	.106E+10	.8598	2.0357	.7424	.2690	+5864	.4611	8951	.8849	9054	. 6329	1.1090	1.0240

TABLE IV. REAL+GAS ISENTROPIC EXPANSIONS OF PARAHYDROGEN

A. (CONTINUED)

MACH	LOCAL ISENTROPIC	VISCOSITY	THERMAL CONDUCTIVITY	PRANDTL
	EXPANSION COEFF.	G/CH-SEC	CAL/CH-SEC-K	NUMBER
	Ť	.22199E-84	.84287E+04	9270
0.000	-			.8278
•050	1.7849	• 22131E-04	.83978E-04	.8283
.100	1.7431	• 22077E-04	.63773E-04	. 8284
. 150	1.7537	•21989£-04	.83431E-84	.8286
.200	1.7614	.21868E-94	.82953E-04	.8289
.250	1.7457	.21712E-04	.82331E-04	• 6293
•300	1.7497	.21527E-04	.81566E-04	.6301
. 350	1.7521	.21312E- 0 4	.80656E-04	-6314
.400	1.7449	•21069E -8 4	.79593E-04	.8332
.450	1.7411	.208 0 2E- 0 4	.78785E-04	-8314
•500	1.7444	.20512E-04	•77 70 6E-04	.8317
•550	1.7352	.20200E-04	.76494E-84	.8326
•600	1.7345	.19871E-04	.75157E-04	.0342
.650	1.7327	-19526E-84	.73698E-84	.8367
.700	1.7279	.19167E-04	.72133E-04	.8399
.750	1.7246	.18796E-04	.70618E-04	.6423
.800	1.7201	.18415E-04	.69032E-04	8452
.850	1.7173	.18025E-04	.67454E-04	.8471
.900	1.7175	.17628E-04	.65976E-04	.8476
950	1.7159	.17227E-84	.64326E-04	.8500
1.000	1.7094	.16823E-04	.62616E-04	.8585
1.050	1.7123	.16418E-04	.61292E-04	.8512
1.100	1.7071	.16013E-04	···	
1.150			.59743E-04	.8524
	1.7051	.15610E-04	•58181E-04	.8541
1.200	1.7013	.15216E-84	.56612E-04	.8563
1.250	1.7007	•14814E-04	.55046E-04	. 8591
1.300	1.6970	•14423E-84	.53780E-84	.8577
1.350	1.6914	.14837E-04	.52479E-04	.8575
1.400	1.6871	.13658E-04	•51123E-04	.8590
1.450	1.6864	•1328 EE -94	.49726E-04	.8621

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TABLE IV. REAL-GAS ISENTROPIC EXPANSIONS OF PARAMYDROGEN

		B. 1	T = +5.0	K PT =	8.0 ATM	PHOT =	.481E-02	CACMS	SVT = 541	1.24 M.C.	=~	•	
				. , . –			8401L-UZ	GF 6143	241 - 241	***** U.\$	LU		
MACH	PEZM	7	CENCA	SV/SVT	PZPT	T/TT	RHOZRHOT	ATZA		P/PT	1/11		A+/A
										RELATIVE	TO IDEAL	GAS VALUES	
0.000	0.	.9087	1.9185	1.0000	1.0000	1.0007	1.0000	0.0000	1.0000	1.0599	1.0000	1.0000	1.0000
•050	.547E+NB	• 9086	1.9186	. 9995	9979	9991	•9988	.0897	+9998	9996	.9996	1.0000	1.0400
.100	.100E+09	. 9085	1.9187	.9960	9913	.9965	9949	.1785	.9990	9982	. 9985	.9999	1.0391
.150	.161E+09	. 90 83	1.9188	.9956	.9808	.9922	9889	-2655	9978	9963	.9967	1.0001	1.0388
.200	.213F+09	.9080	1.9189	•9922	•9661	.9862	9804	.3497	9962	.9935	.9941	1.0001	1.0364
•250	•264E+89	•9076	1.9190	.9373	.9478	.9757	•9696	.4305	•9941	9899	9909	1.0002	1.0343
.300	+₹1.3E+0.9	.9071	1.9191	.98≥8	• 9261	•9696	9568	.5070	9916	.9856	.9870	1.0004	1.0319
• 35 0	• 3615+09	•906E	1.9193	.9768	.9814	.9591	.9420	.5789	+9887	9811	9826	1.0006	1.0293
•400	•487E+89	.9061	1.9193	.9700	.87+1	.9473	9254	.6454	-9854	9760	9776	1.0012	1.0263
.450	+4515+09	.9054	1.9193	•9626	.8446	.9343	9072	.7063	-9819	.9705	9721	1.0019	1.0233
•509	.493E+09	•9048	1.9192	• 9544	• 81 ₹₹	.9292	.8977	.7614	9780	9648	9662	1.0028	1.0202
•55°	.5325+99	.9841	1.9190	.9457	.7806	.9051	.8668	.8104	+9738	9588	9599	1.0020	1.0202
•600	•569E+09	.9034	1.9188	9364	.7471	.8892	.8458	.6533	9695	9529	9532	1.0054	
.650	.604E+09	.9027	1.9184	.9266	.7129	.8726	.9223	.6903	9650	9469	9463	1.0072	1.0139
.700	.636E+09	.9020	4,6190	916+	-6786	.8554	*7991	•9215	9603	9413	9392		1.0110
.750	•666E+N9	9013		9059	.6443	.8377	.7754	9469	• 9555	9357	.9320	1.0095 1.0122	1.0084
.800	.694E+09	.9007	1.9168	8951	.6194	8196	7513	9670	+9507	• 9304	+ 9246		1.0060
.050	•719E+09	.9000	1.9161	.8840	,5770	8013	.7271	9820	9458	.9255	.9171	1.0153	1.0040
•900	.743E+N9	.8994	1.9153	.8725	.5445	.7828	7028	.9922	94118	.9208	9096	1.0189	1.0023
•95 N	.764E+09	.4987		8614	.5128	7541	6786	.9981	9359	.9167	9021	1.0229	1.0010
1,000	.7835409	. 1981	1.9135	8499	.4823	.7455	-5546	1.0000	.9310	• 9130	• 8946	1.0274	1.0002
1.050	.800E+09	.8976	1.9133	8384	4529	•7268	.6309	.9983	9263	.9097	.8871	1.0326	1.0000
1.100	.816E+09	.4970		.8279	42-7	.7982	.6975	. 9933	9216	.9069	8796	1.0382 1.0443	1-0903
1.150	.829F+09	.8965	1.9129	.8155	3978	6898	.5844	9852	9170	.9044	.8722		1.0012
1.290	.841F+89	.8960	1.9127	89 40	3772	.6715	•5 6 20	.9747	9125	.9026	.8650	1.0509	1.0024
1.250	, A525+D9	.8956	1.9125	7926	3440	6536	•5402	9619	9080	.9013		1.0582	1.8043
1.300	.861E+09	. 4952	1,9130	.7812	.3250	.6358	.5188	.9471	• 9036	.9006	.8578 .8588	1,0061	1.0069
1.350	+8695+09	.8948	1,9115	• 7€ 9A	3034	6185	•4992	9307	•8993	.9004		1.5 44	1.0099
1.490	8765+09	.8945	1,9104	.7586	-2832	.6015	.4783	9134	•8950	.9011	. 8439	1.0835	1.0135
1.450	.981E+09	. 8542	1.9099	.7475	.2641	•584R	•459D	.8941	•8989 •8989		.8372	1.0934	1.0179
1.500	-886E+89	.8939	1.9089	.7365	.2462	5686	.4402	6742	•8868	9023	.8307	1.1037	1.0229
1.550	.889E+09	.8936	1.9077	.7256	•2296	5527	+4223	-8538	.8829	.9040	.8244	1.1146	1.0262
1.600	.892E+09	.8935	1.9064	7149	.2140	5373	•4050	.8327		• 9065	.8163	1.1264	1.0345
1.650	.8945+09	.8933	1.9051	7043	.1994	5223	•4020 •3884	.8114	•8790 •8753	.9094	.8124	1.1385	1.0410
1.700	·895E+09	.8931	1.9836	6939	.1859	.5077	•3724			9132	.8067	1.1515	1.0485
1.750	.895E+09	.8930	1.9021	.6837	•1732	.4936	•3724 •3571	•7897	.8717	.9174	.6012	1.1650	1.0563
1.800	8958+09	.8928	1.9007	• 5736	.1614			.7680	-8681	•9223	.7959	1.1791	1.0648
1.850	.894E+09	.8927	1.8993	.6637	.1595	+4799	**424	.7462	.8647	•927£	.7908	1.1938	1-0736
	40375 1117	+47C1	1.0227	.0037	*1545	•4666	.3283	.7246	.8614	. 9336	.7860	1.2091	1.0834

B. (CONTINUED)

MACH	LOCAL ISENTROPIC EXPANSION COEFF.	VISCOSITY G/CM-SEC	THERMAL CONDUCTIVITY CAL/CM-SEC-K	PRANDTL NUMBER
	EXPANSION GUEFF.	GF GM = 3EG	CALFCH-SEL-K	NUMBER
0.000	Ĭ	.24137E-04	.91348E-D4	.7736
.050	1.7551	-2406EE-04	.91029E-04	.7740
.109	1.7157	.24011E-04	.90779E-04	.7742
.150	1.7548	.23920E-04	.90372E-04	.7747
.200	1.7346	.23793E-64	.89399E-04	.7789
. 250	1.7373	.23633E-04	.88765E-84	.7790
.300	1.7341	.23440E-04	.87982E-04	.7794
• 350	1.7372	.23216E-04	.87050E-04	.7801
•400	1.7321	.22964E-04	.85961E-04	.7812
•450	1.7384	.22684E-04	.84863E-84	.7815
•500	1.7307	.22360E-04	.83602E-04	.7825
•550	1.7242	.22054E-04	.82238E-84	.7837
.600	1.7253	.21708E-04	.80785E+04	.7852
.650	1.7218	.?1344E-84	•79250E+04	.7869
.700	1.7231	.20966E-04	.77648E-04	.7869
.750	1.7176	.20574E-04	•76144E-04	.7894
.800	1.7157	.20171E-04	.74592E-04	.7901
.850	1.7133	-1976DE-D4	•72970E-04	.7913
• 900	1.7089	.19342E-04	.71287E-74	.7938
• 950	1.7073	.18919E-04	.69553E-04	.7952
1.000	1.7054	•18492E-04	.67870E-04	.7968
1.050	1.7038	.18062E-04	.66178E-04	.7985
1.100	1.7020	•17632E-04	.64538E-04	.7992
1.150	1.6974	.17201E-04	•62958E+04	.7992
1.200	1.6991	.16772E-04	•61339E-04	.7995
1.250	1.6975	.16346E-04	.59750E-04	.8002
1.300	1.6930	•15923E-84	.58166E-04	.8007
1.350	1.6919	.15506E-04	.56596E-84	.8014
1.400	1.6933	.15095E-04	.55030E-04	.8026
1.450	1.6893	.14689E-04	•53471E-04	.8041
1.500	1.6847	•14291E-84	.52 0 43E-04	.8042
1.550	1.6871	.13900E-84	•50628E-04	.8048
1.600	1.6807	.13517E-04	.49180E-04	.8065
1.650	1.6826	•13142E-04	.47715E-04	.8094
1.700	1.6771	.12775E-04	•46237E-04	.8134
1.750	1.6769	•12417E-04	•44758E-04	.818 5
1.000	1.6728	.12068E-04	.43430E-04	.8220
1.850	1.6718	.11726E-04	•42179E-04	.8250

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TABLE IV. REAL-GAS ISENTROPIC EXPANSIONS OF PARAHYDROGEN

		C. IT	= 50.0	K PT =	8.0 ATM	RHOT =	• 421E-9?	GZCH3	SVT = 576	•160 M/S	EC		
MACH	REZM	7.	CP/CV	SV/SVT	P/PT	1/11	RHOZRHOT	A*/A	SV/SVT	P/PT RELATIVE	T/TT TO IDEAL	RHOZPHOT GAS VALUES	A-/A
0.900	0.	. 93 45	1.8435	1.0000	1.0000	1.0000	1.0000	0.0000	1.0000	1.0000	1.0000	1.0000	1.0000
•050	.466E+0B	. 9344	1.4438	9995	9979	.9991	.9988	.0894	9998	.9996	.9996	1.0000	1.0366
.100	·929E+08	.9343	1.8440	.9981	.9915	.9966	9951	.1780	9991	9985	9986	1.0001	1.0360
.150	.139E+09	•9341	1.8442	.9953	.9809	.9923	-9689	.2646	.9981	. 9964	.9968	1.0000	1.0348
-500	.184E+89	. 9779	1.8446	.9927	. 9664	.9864	.9803	.3487	.9966	.9937	.9943	1.0001	1.0333
.250	•227E+09	.9335	1.8450	•9886	•9482	.9789	• 96 96	.4293	9947	.9903	.9912	1.0002	1.0315
.300	•270E+09	.9332	1.8455	.9837	.9266	• 96 99	• 9567	.5058	.9925	•9863	-9874	1.0003	1.0293
.350	•311E+09	.9327	1.8460	•9780	.9019	• 95 95	.941R	.5775	•9899	•9817	.9830	1.0005	1.0268
•400	.351£+09	.9722	1.8465	.9715	.8748	.9478	.9253	.6442	.9869	.9768	. 9781	1.0011	1.0243
•450	.3895+09	.9317	1.8470	•96+3	.84F4	.9349	.9070	.7052	.9837	.9715	.9727	1.0017	1.0216
•500	•425E+09	•9311	1.8474	• 9565	.8142	•9209	-8874	.7603	.9861	•9658	, 9669	1.0025	1.0187
•550	.458E+119	.9₹05	1.8477	.9480	.7816	.9059	• 9665	.8094	•9763	. 96 0 0	.9607	1.0036	1.0158
-600	.4905+09	. 9299	1.8489	• पुर पृत	.7448	•8900	.8446	.8526	• 9722	. 9541	9541	1.0050	1.0130
•65 D	•520E+09	.9292	1.8481	• 92 95	.7139	.8734	•9219	.8897	.9680	9462	.9472	1.0067	1.0103
•700	.548E+09	.9286	1.8481	-9196	6794	.8562	.7985	.9209	.9636	9424	9401	1.0068	1.0078
.750	•573E+09	.9280	1.8480	• 9093	.6451	.8365	.7748	.9466	.9591	9369	.9329	1.0114	1.0957
.800	•597E+09	.9274	1.8478	.8987	.6111	.8284	.7506	.9667	.9545	-9315	9255	1.8143	1.0037
•8 5 0	•618E+09	.9267	1.8475	8978	.5777	.8021	.7262	.9818	.9498	• 92 65	. 9180	1.0177	1.0021
•900	.638E+D9	• 9262	1.8478	.8767	.5449	.7835	.7913	• 9920	•9450	.9217	.9104	1.0215	1.0008
•950	•656E+09	.9256	1.8466	• B654	-5133	.7648	•6777	.9981	.9403	.9176	.9028	1.0261	1.0003
1.000	•672E+89	.9250.	1.8459	.8540	+4827	.7461	•6536	1.0000	.9355	.9137	.8953	1.0310	1.9000
1.050	•686E+09	.9245	1.845 7	.8425	• +5₹?	.7274	.6298	.9982	.9308	.9103	.8878	1.0365	1.0007
1.100	•699E+09	, 9241	1.8445	.8310	.4250	.7088	.6064	.9931	•9261	.9075	.8803	1.0425	1.0010
1.150	•710E+09	.9236	1.8438	.8195	•3941	•6904	-9835	.9851	.921 5	• 90 5 2	.8730	1.0491	1.0923
1.200	.720E+09	.9232	1.8430	.8079	.3726	.6721	.5611	.9746	•9169	- 90 34	.8657	1.0564	1.0042
1.250	•7285+09	.9227	1.8425	• 7 965	#3483	.6541	•5392	.9618	.9125	.9021	.8586	1.0641	1.0967
1.300	• 735£ +0 9	42.54	1.8421	.785t	.3253	.6364	.5178	.9469	•9882	.9012	8515	1.0723	1.0097
1.350	.741E+09	•9220	1.8417	.7739	. 303€	.6189	.4971	.9305	•9040	.9018	.8445	1.0812	1.0133
1.400	•746E+D9	•9217	1.8412	.7627	.2832	.601F	.4770	.9125	-8998	•9011	.8377	1.0905	1.0173
1.450	.750F+09	.9214	1.8407	.7516	•26•0	-5851	4575	. 8934	.8958	.9019	.8311	1.1005	1.0220
1.500	.754E+09	.9212	1.8402	.7486	.2461	.5687	.4389	.8735	.8918	.9033	.8246	1.1112	1.0274
1.550	•756E+09	.9210	1.6396	.7298	.2293	•5528	.4289	.8529	.8879	. 90 53	.8184	1.1225	1.0334
1.600	+75,85+0.9	.9207	1.8389	.7191	.2136	•5372	•4035	.8318	8842	.9079	.8122	1.1344	1.0399
1.650	.759E+89	.9206	1.8381	.7085	•1 9 89	•5220	-3868	.8102	.0805	.9110	.6063	1.1469	1.0470
1.700	•759E+89	.9204	1.8372	-6981	•1853	.5073	.3708	.7885	.8770	. 91 47	.8886	1.1600	1.0547
1.750	.759E+09	.9283	1.8363	.6879	.1726	.4930	•₹555	.7667	.6735	.9190	.7950	1.1738	1.0630
1.800	.759E+09	.9202	1.8353	.6778	.1608	.4791	.3408	.7448	.8701	-9238	.7896	1.1881	1.0716
1.850	•758E+09	.9201	1.8343	.6579	.1498	•4657	•32E7	.7232	. 8669	.9293	.7844	1.2032	1.0813
1.900	•756E+09	•9200	1.8333	.6582	•1396	.4526	.3132	.7017	.8637	9352	.7794	1.2187	1.0913
1.950	.754E+119	.92BN	1.8323	.6486	.1301	• 4400	.3092	6804	.860£	. 9415	.7746	1,2347	1.1017
2.000	•752E+09	. 91 99	1.8313	.6393	.1212	.4277	.2879	•6595	.8577	. 9486	.7699	1.2515	1.1129

C. (CONTINUED)

	1 0014 TSSNTOORIS	UTCGACTTU	THERMAL COMMISSIONET	PRANDTL
MACH	LOCAL ISENTROPIC	VISCOSITY	THERMAL CONDUCTIVITY	
	EXPANSION COEFF.	G/CM-SEC	CAL/CH-SEC+K	NUMBER
8.000	I	.26049E-04	.98655E-04	.7440
.059	1.7277	.25975E+84	.96342E-04	.7441
.108	1.7349	.25918E-04	.98106E-94	.7442
•150	1.7149	.25824E-84	.97713E-04	.7442
.200	1.7203	.25693E-04	.97168E-04	.7443
.250	1.7222	.25527E-04	.96477E-04	.7445
.300	1.7196	.25327E-04	• 9564 3E-04	.7447
.350	1.7177	.25095E+04	•94674E-04	.7450
.400	1.7249	.24832E-04	.93582E-04	.7454
•450	1.7199	.24542E-B4	•92303E-04	.7464
•500	1.7174	.24225E-04	.90898E-04	.7477
•550	1.7174	.23884E- 0 4	.89361E-04	.7492
•600	1.7162	.23522E-04	.87787E-04	.7508
.650	1.7142	.23141E-04	•85654E-84	•7566
.700	1.7130	.22744E-84	•84005E-04	.7577
.750	1.7136	.22333E-04	.82327E+04	.7588
.800	1.7083	.21909E-04	.80593E-04	.7601
.850	1.7075	.21476E-04	.78817E-04	.7616
•900	1.7039	.21934E-04	.77007E-04	. 7632
• 950	1.7075	.29588E-04	.75186E-84	.7649
1.000	1.7015	.2013EE-04	.73437E-04	.7657
1.056	1.6994	.19682E-04	.71673E-04	.7668
1.100	1.6985	.19228E-84	.69898E-04	.7680
1.158	1.6958	.18773E→04	•68121E-04	.7693
1.200	1.6950	.18320E-04	.66347E+04	.7708
1.250	1.6930	.17869E+04	.645B0E+04	.7724
1.300	1.6907	.17420E-04	.62908E-04	.7728
1.350	1.6912	.16976E-04	.61307E-04	.7727
1.486	1.6860	.16537E-04	.59684E-04	.7729
1.450	1.6869	.16104E-04	.58067E-04	.7734
1.500	1.6863	.15678E-84	.56459E-04	.7742
1.550	1.6854	.15258E+84	•54 8 61E-04	.7753
1.600	1.6835	.14847E-N4	•53261E-04	.7766
1.650	1.6814	.14443E-04	.51725E-04	.7782
1.700	1.6813	.14047E-04	•50250E+04	.7792
1.750	1.6804	.13661E -0 4	.48760E+04	.7812
1.800	1.6768	.13263E-84	.47368E-04	.7822
1.850	1.6782	.12914E+04	.46029E-04	.7631
1.900	1.6757	.12553E-04	.44718E-04	.7842
1.950	1.6718	•12202E-04	•43437E-04	.7855
2.000	1.6741	•11860E-04	.42188E-34	.7871

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TABLE IV. REAL+GAS ISENTROPIC EXPANSIONS OF PARAHYDROGEN

_					-		
U∗	11 =	511 • 11 K	₽1 =	א ט•פ AIM	KH01 =	• 140E-B2 G/CM3	SVT = 634.071 M/SEC

		D. IT	= 60.0	Υ Р Т =	8.0 ATM	RHOT =	.340E-02	G/CM3	SVT = 634	.071 M/S	:c		
MACH	RE/M	Z	CP/CV	SV/SVT	P/FT	1/11	RHOZRHOT	A*/A	SV/SVT	P/PT	1/11	RHOZRHOT	A*/A
												GAS VALUES	
0.000	0.	.9542	1.7450	1.0000	1.0000	1.0000	1.0000	0.0000	1.0000	1.0000	1.0000	1.0000	1.0000
.050	.363E+08	. 9642	1.7457	• 9996	.9979	.9992	.9987	.0887	.9998	.9996	.9997	1.0800	1.0288
.100	.723E+08	.9541	1.7462	• 3984	•9915	.9967	.9949	•1766	.9994	.9985	. 9987	•9999	1.0283
•150	.108E+09	• 9641	1.7470	.9964	•9813	.9926	.9884	.2628	.9986	. 9968	.9971	1.0000	1.0276
.200	.143E+09	.9538	1.7481	. 9936	.9671	.9870	.9804	.3464	.997€	. 9945	.9948	1.0001	1.0266
•250	.177E+09	.9635	1.7494	•9901	. 9493	.9797	• 96 96	•4268	.9962	.9915	.9920	1.0002	1.0254
.300	.21 DE+D9	• 9632	1.7518	.9858	.9279	.9711	•9566	-5938	.9946	- 9877	.9885	1.0003	1.0237
.350	.2425+09	.9628	1.7527	.9807	•9036	.9611	.9417	•5748	.9927	9835	. 9845	1.0005	1.0219
•400	·273E+09	.9624	1.7546	.9750	.8768	•9496	• 92 51	6415	.9904	.9790	.9800	1.0009	1.0201
.450	•3025+08	.9520	1.7565	.9685	.8475	•9369	•9066	.7026	.9879	.9738	• 9749	1.8012	1.0178
•500	•3308+09	.9615	1.7584	.9614	8165	.9232	.8869	.7581	.9851	.9685	• 96 94	1.0020	1.0157
•550	•357E+09	.9611	1.7605	. 9537	•7839	.9884	.8658	.8075	.9821	• 9628	• 9634	1.0027	1.0134
•697	•381E+D9	9676	1.7624	• 9454	•7504	8928	.8437	.8517	.9788	.9571	• 95 71	1.0036	1.0111
.650	, 4045+09	9500	1.7642	9366	.7162	.8764	.8208	.8885	.9753	.9513	• 95 04	1.0054	1.0090
700	.425E+09	9595	1.7658	. 9272	•6815	.8593	.7971	•9199	.9716	. 9453	• 9435	1.0069	1.0067
.750	.445E+09	•9590	1.7673	.9175	•€⇒71	.8416	•7731	• 9459	•9677	• 93 98	•9363	1.0092	1.0050
• 500	•463E+09	. 95 94	1.7685	.91173	• £128	. 8235	•7486	• 9662	•96₹6	9341	. 9290	1.0117	1.0032
.850	.479E+09	.9579	1.7696	.8968	•579?	.8951	.7242	.9816	.9595	•9290	•9215	1.0148	1.0019
•900	•494E+09	.9574	1.7704	.8861	-5463	.7865	•6996	• 9920	•9552	• 92 3 9	•9139	1.0182	1.0008
• 95 0	•507E+09	• 9569	1.7711	.8751	• 5 1 - 3	.7677	.6751	. 9979	•9508	•9193	•9063	1.0221	1.0000
1.000	•519E+09	• 9564	1.7715	.8639	.4836	.7489	.6510	1.0900	• 9464	• 91 5 3	.8987	1.0269	1.0000
1.050	•529£+09	.9559	1.7718	.8526	•45₹8	.7301	.6270	.9981	.9419	. 9116	. 8911	1.0318	1.0001
1.100	.538E+09	. 9555	1.7719	.8412	• 4255	.7114	. 60 35	•9930	.9375	.9084	.8836	1.0375	1.0009
1.150	.546E+09	•9550	1.7718	.8297	.3984	.6929	.5805	.9849	.9338	.9857	.8762	1.8437	1.0021
1.200	.553E+09	.9546	1.7717	.8183	• 3727	•6745	•5581	• 9744	.9286	. 90 37	.8688	1.0507	1.0940
1.250	•559E+09	.9543	1.7714	.8068	•3483	•6564	•5361	.9613	.9243	• 90 21	.8616	1.0589	1.0063
1.300	.564E+09	9539	1.7711	.7954	.3253	•6₹8€	•5148	.9466	. 9200	.9012	. 8545	1.0661	1.0093
1.350	•568 <u>°</u> +09	• 9536	1.7706	.7840	• 3075	•6211	.4942	• 93:00	.9158	• 90 0 8	.8475	1.0747	1.0128
1.400	•571E+09	• 9533	1.7702	.7727	.2331	.6041	.4741	•9120	.9117	•9009	+8407	1.0839	1.0168
1.450	.573E+09	• 95 30	1.7697	.7615	• 2639	.5872	•4548	.8930	•9076	•9017	. 6341	1.0938	1.0216
1.500	•575E+09	•952B	1.7691	.7505	•2459	.5707	.4361	.8729	.9037	.9028	.8276	1.1041	1.0267
1.558	•576E+09	. 9525	1.7685	.7395	• 2292	.5547	4182	.8524	.8998	.9048	.8212	1.1153	1.0327
1.60 0	•576E+D9	• 9523	1.7682	.7288	.2134	.5390	.4009	.8311	.8961	.9071	.8150	1.1269	1.0391
1.650	.576E+09	.9521	1.7678	.7161	1987	•5238	.3842	.8194	.8925	. 90 98	• 80 90	1.1389	1.0459
1.700	•576E+N9	•9520	1.7674	.7977	• 1850	.5098	.36R2	.7876	.8890	.9132	.8031	1.1516	1.0535
1.750	.575E+09	.9518	1.7670	• 6 974	.1722	•4945	.3528	.7656	.8855	.9171	.7975	1.1650	1.0616
1.800	.574£+09	• 95 1 7	1.7665	.6872	• 1604	.4805	.3382	.7438	.8822	.9215	.7919	1.1790	1.0703
1.850	.572E+09	•9516	1.7661	.6772	.1493	.4669	.3241	•7219	.8790	• 9264	.7866	1.1935	1.0794
1.900	.570E+09	•9515	1.7656	. 667∻	• 1 351	.45 TR	• ₹116	.7802	.8758	.9317	.7814	1.2084	1.0990
1.950	•568E+119	.9514	1.7651	. 6578	.1295	.441 n	.297*	.6790	.8728	.9378	.7763	1.2243	1.0995
2.000	.5665+09	9514	1.7645	, 6483	•12N7	.428f	•285 +	6579	.8698	• 9442	.7715	1.2484	1.1103

D. (CONTINUED)

MACH	LOCAL ISENTROPIC	VISCOSITY	THERMAL CONDUCTIVITY	PRANDTL
	FXPANSION COEFF.	G/CM-SEC	CAL/CM-SEC+K	NUMBEP
0.000	I	.29733E-04	.11626E-03	.7013
.050	1.6656	.29653E-04	.11588E-03	.7013
.100	1.6725	• 29594E -0 4	•11559E-03	.7013
• 150	1.6946	.29495E+B4	.11513E-03	.7013
.200	1.6917	·29359E-84	•11447E-03	.7013
.250	1.6910	.29184E-84	.11364E-83	.7014
.300	1.6821	.28974E+04	•11263E-03	.7016
.350	1.6831	.28728E-04	.11146E-03	.7018
.400	1.6933	.28450E-04	•11013E-03	.7022
• 450	1.6867	.28140E-94	•10865E-03	.7027
.500	1.6938	.27802E-04	.10486E-03	.7180
.558	1.6890	•27 43 6E-04	.10325E-03	.7182
.680	1.6932	.27046E-04	.10154E-03	.7186
•650	1.6958	.26634E-N4	.99753E-04	.7191
.700	1.6901	.26203E-04	.97911E-04	.7194
.750	1.6982	.25755E-04	•96006E=04	.7200
.800	1.6917	.25292E-04	.94064E-04	.7206
.850	1.6979	.24817E-84	-92094E-04	.7212
• 900	1.6919	.24333E-84	.90085E+04	.7220
. 951	1.6925	.236415-84	.87952E-04	.7237
1.000	1.6968	•23344E-84	.85818E-04	•7255
1.050	1.6905	.228425-04	•83189E-04	.7317
1.100	1.6925	.22339E-04	.81147E-04	.7331
1.150	1.6895	.21836E-04	.79110E-04	.7345
1.290	1.6920	.21333E-04	.77085E-04	.7360
1.250	1.6872	.20833E-04	.75079E-84	.7376
1.300	1.68 9 5	.2033€E-04	.73116E-84	.7398
1.350	1.6869	•19843E-84	.71223E-04	.7400
1.400	1.6849	.19355E-04	.69359E-04	.7409
1.450	1.6852	.18874E-04	.67528E-04	.7419
1.500	1.6816	.18398E-04	.65732E-04	.7428
1.550	1.6849	•17938E-04	.63976E-04	.7436
1.600	1.6814	.17469E-84	.62257E-04	.7443
1.650	1.6791	.17016E-04	•60554E-04	•7451
1.700	1.6799	•16571E-04	.58867E-04	.7462
1.750	1.6793	.16135E-94	.57204E+84	.7474
1.800	1.6789	.1570 PE-04	.55618E-04	.7482
1.850	1.6772	.1529NE-84	.54065E-04	.7489
1.900	1.6747	.14881E-04	•52562Ë - 04	.7495
1.950	1.6783	.14481E-04	•51101E-04	.7501
2.000	1.6741	.14891E-84	•49682E=94	.7505

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TABLE IV. PEAL+GAS ISENTROPIC EXPANSIONS OF PARAHYGROGEN

									· · · · - · - • · ·				
		₹∙ रा	= 90.0	K PT =	8.9 ATP	PHOT =	.248E-02	G/CM3	SVT = 716	.788 M/S	EC		
MACH	RE/M	7	CP/CV	SV/SVT	FZFT	T/TY	RHOZRHOT	A*/A	SV/SVT	P/PT RELATIVE	T/TT TO IDEAL	RHO/RHOT GAS VALUES	A*/A S
0.000	0.	.9898	1.5896	1.0000	1.0090	1.0080	1.0000	0.0000	1.0000	1.0000	1.0000	1.0000	1.0000
.050	.244F+08	.9889	1.5910	.9997	9981	.9993	.9988	.0670	1.0000	.9999	.9998	1.0001	1.0090
.100	•4865+88	.9889	1.5919	.9989	9922	.9372	.9951	.1733	.9999	• 9992	. 9992	1.0701	1.0069
.150	.7265+08	.9888	1.5935	. 9975	.9825	.9937	•9889	.2580	.9998	.9980	. 9982	1.0000	1.0087
.200	•961E+08	.9887	1.5956	• 9956	• 9691	.9889	.9802	.3483	•9996	.9965	. 9968	1.0000	1.0085
.250	.119E+09	.9845	1.5983	.9932	. 9522	.9827	• 9694	+4196	.9993	•9945	.9958	1.0000	1.0063
•300	•141£+09	.9883	1.6916	•9992	.9320	.9752	•9563	•4953	•9990	• 9920	.9927	•9999	1.0079
.750	.163E+09	.985t	1.6954	• 9866	.9889	• 9664	.9414	•5667	•9986	•9892	.9901	1.0001	1.0076
• - 0 D	.184F+D9	•9878	1.6097	.9825	.8830	.9563	.9244	.6334	.9981	• 9859	•9869	1.0001	1.0072
•450	.203£+09	. 9875	1.6146	• 9779	.8548	•9451	•9858	.6949	.9975	• 9823	.9834	1.0003	1.0067
.500	.222E+09	.9872	1.6198	.9727	.8246	.9328	.8856	.7509	• 9968	.9781	.9794	1.0005	1.0061
·550	.239E+89	.9869	1.6255	.9679	•7926	• 91 93	.8640	.8011	•9959	. 9735	9749	1.000€	1.0054
.600	•256E+09	.9865	1.6314	•96 8 8	.7594	.9049	.8413	. 8455	• 9948	.9686	. 97 00	1.0010	1.0047
•650	.271E+09	•9862	1.6377	• 9541	.7253	.8896	.8177	.8841	•9936	.9635	.9647	1.0016	1.0040
.700	·285E+09	.9858	1.5440	.9468	.6907	.8734	•7933	•9167	•9921	• 95 8 0	•9590	1.0922	1.0032
.750	.298E+09	. 9854	1.6505	9391	.6558	. 8565	.7684	• 9435	•9905	• 9523	•9528	1.0031	1.0024
.800	.309E+09	.9850	1.6569	. 9308	.6210	.8390	.7432	•9648	.9886	.9466	• 9464	1.0043	1.0017
.850	•320E+09	.9846	1.6632	•9221	•5866	.8209	•7177	.9807	•9865	• 9407	• 93 96	1.0057	1.0010
.900	•329£+09	.9842	1.6693	•9130	•5529	.8025	.6923	. 9917	+9841	•9351	•9325	1.0077	1.0005
•950	•338E+09	.9838	1.6750	.9034	•5199	.7837	.6669	. 9978	•9816	•9293	• 9252	1.0098	1.0000
1.000	.345E+09	.983~	1.6005	.8935	.4882	.764B	.6420	1.0000	.9788	. 9241	.9177	1.0126	1.0000
1.050	.351E+09	.9831	1.6854	.8432	. 457E	.7457	.6173	.9981	.9758	• 9 1 90	-9101	1.0159	1.0091
1.100	•357E+09	.9827	1.6899	.8727	• 4283	.7266	•5932	.9927	.9726	. 91 44	.9025	1.0197	1.0006
1.150	•361E+09	.9823	1.6939	-8619	• 4004	.7876	•5695	. 9843	•9692	.9103	.8948	1.0242	1.0015
1.200	.3655+09	.9820	1.6975	.85119	+3741	-6888	•5468	. 9734	.9657	•9068	.8872	1.0294	1.0030
1.250	.368E+89	.9817	1.7005	.8398	.3489	.670?	•5245	•9600	.9621	.9039	.8796	1.0352	1.8049
1.300	.370E+09	.9813	1.7031	8286	•3254	•6519	• 5030	.9447	-9584	.9016	.8722	1.0417	1.0073
1.350	.3725+09	.9811	1.7052	. 8173	.3032	.6338	.4823	.9277	•9547	.8999	.8649	1.0489	1.0103
1.400	.373E+09	.9808	1.7869	.8060	.2824	.6162	•4622	•9092	•9509	.8988	.8577	1.0566	1.0137
1.450	•374E+D9	.9805	1.7083	.7947	• 263t	.5989	.4430	.8899	.9472	.8985	.8507	1.0653	1.0180
1.500	.3745+09	.9883	1.7094	.7635	.2448	.5820	•4244	.8695	.9434	. 8988	.8439	1.0745	1.0227
1.550	.374E+09	.9800	1.7101	.7723	•2279	•5655	•4066	.8485	.9397	.8998	.8373	1.0844	1.0281
1.608	.374E+89	.9798	1.7107	.7612	.2121	•5495	.3895	.8271	.9360	.9014	.8389	1.0950	1.0341
1.650	.373E+09	.9795	1.7111	.750?	•1974	.5339	.3732	.8054	.9324	. 98 37	. 8246	1.1064	1.0408
1.700	.3725+09	• 97 94	1.7113	.7394	•1837	-51.87	.3575	•7 83 5	•9288	.9065	.8186	1.1183	1.0479
1.750	.370E+09	•9793	1.7114	.7287	.1789	.5040	•3425	.7614	•9254	• 98 99	.8127	1.1308	1.0557
1.800	•369E+09	.9791	1.7114	.7182	.1591	.4897	.3281	.7395	•9220	•9148	.8070	1.1439	1.0641
1.650	•367E+09	.9790	1.7114	.7078	.1481	•475 B	•31.43	.7176	.9187	•9185	.8015	1.1576	1.0730
1.900	•365E+89	.9788	1.7112	.6976	.1378	.4624	.3012	.6960	. 95 34	• 9236	. 7962	1.1720	1.0825
1.950	.363E+09	.9787	1.7111	-6876	.1283	.4493	.2885	.6747	•9123	• 92 92	.7910	1.1869	1.0925
2.000	.360E+09	•9786	1.7109	.6777	•11º6	.4367	.2767	.6538	.9093	. 9355	.7860	1.2027	1.1033

E. (CONTINUED)

LCCAL ISENTROPIC	VISCOSITY	THEPMAL CONDUCTIVITY	PRANDTL
EXPANSION COEFF.	G/CM-SEC	CAL/CM-SEC-K	NUMBER
T	766405.07	4 = 0.4 7 = - 0.7	.7054
			•7054
			.7054
			.7054
			.7055
			.7057
			.7059
_			• •
			.7050
			.7035
	• • • • • • •		.7019
			•7003 •6987
			•6972
			•6958 •6946
		· · · · · · · · · · · · · · · · · · ·	.6937
			•693 0
			.6919
			.6908
			•6902
			.6900
			.6902
	· · · · · · · · · · · · · · · · · · ·		.6908
	• - · · · ·		.6918
			.7008
		•	.7006
			.7013
- -			.7021
			.7830
		• • - · · · - - ·	.7040
			.7854
•			.7072
		-	.7117
			.7131
		*	.7146
	_		.7160
	·		.7172
			-7184
			.7193
			.7202
1,6767	.18522E-04	.65422E=04	.7210
		I 3654PE-04 1.6075 36450E-04 1.5771 36392E-04 1.5770 36295E-04 1.5746 36159E-04 1.5780 35986E-04 1.5894 35527E-04 1.5894 35527E-04 1.5945 34925E-04 1.6006 34188E-04 1.6151 3329E-0+ 1.6189 32256E-04 1.6303 31845E-04 1.6338 313845E-04 1.6428 31308E-04 1.6530 29608E-04 1.6530 30187E-04 1.6530 29608E-04 1.6541 29021E-04 1.6586 28428E-04 1.6586 28428E-04 1.6570 27233E-04 1.6670 27233E-04 1.6670 27233E-04 1.6671 22601E-04 1.6712 24867E-04 1.6714 23718E-84 1.6748 23155E-04 1.6755 22601E-04 1.6756 2282601E-04 1.6757 208480E-04 1.6757 3096E-04 1.6757 3096E-04 1.6757 319975E-04	I .3654PE-04 .15047E-03 1.6075 .36450E-04 .14986E-03 1.5771 .36392E-04 .14945E-03 1.5770 .36295E-04 .14945E-03 1.5770 .36295E-04 .14878E-03 1.5746 .36159E-04 .14785E-03 1.5723 .35985E-04 .14665E-03 1.5780 .35774E-04 .14521E-03 1.5894 .35527E-04 .14521E-03 1.5894 .35527E-04 .14521E-03 1.5995 .34925E-04 .14049E-03 1.5995 .34925E-04 .14049E-03 1.6006 .34188E-04 .13653E-03 1.60078 .33773E-04 .13430E-03 1.6151 .33329E-04 .13430E-03 1.6189 .32850E-04 .12944E-03 1.6239 .32363E-04 .12602E-03 1.6348 .31708E-04 .12602E-03 1.6530 .30187E-04 .12400E-03 1.6628 .30755E-04 .12400E-03 1.6650 .29608E-04 .11674E-03 1.6670 .29021E-04 .11039E-03 1.6671 .29021E-04 .11039E-03 1.6671 .29021E-04 .11039E-03 1.6671 .2933E-04 .98333E-04 1.6671 .29021E-04 .1092E-03 1.6671 .2933E-04 .98333E-04 1.6671 .29021E-04 .1092E-03 1.6671 .2733E-04 .98333E-04 1.6671 .27233E-04 .9855E-04 1.6672 .26601E-04 .9855E-04 .8871E-04 1.6674 .27233E-04 .78660E-04 1.6675 .27233E-04 .78660E-04 1.6675 .27233E-04 .78660E-04 1.6676 .24289E-04 .78961E-04 1.66770 .22056E-04 .78961E-04 1.66757 .20480E-04 .7495E-04 .7495E-04 1.66757 .20480E-04 .7495E-04 .76860E-04 1.66740 .18996E-04 .7696E-04 .7696E-04 .7696E-04 .7696E-04 .7696E-04 .76996E-04 .

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Manager and State of the State

TAPLE IV. PHAL-GAS ISENTROPIC EXPANSIONS OF PARAHYCPOGEN

		F. II	= 109.0	K PT =	8.0 ATM	= T0H¢	•197F-D2	G/CM3	SVT = 777	.849 M/S	EC.		
MACH	₽ E /M	7	CP/CV	SV/SVT	₽/PT	7/17	RHOZRHOT	A*/A	SV/SVT	P/PT RELATIVE	T/TT TO IDEAL	RHO/RHOT	A+/A +
0.000	С.	,9332	1.4671	1.0000	1.0000	1.0000	4 8000						
050	•179E+08	.9992	1.4689	.9998	•9981	.9994	1.0000 .9987	0.0000	1.0000	1.0000	1.0000	1.0000	1.0000
.100	.757E+08	9981	1.4596	9991	9927	.9977	•9951	0859	1.0000	• 99 99	.9999	.9999	•596N
150	.533E+DA	9980	1.4708	.9980	9837	9949	•9889	•1711 •2548	1.0001	• 9997	.9997	1.0000	•9962
200	.705E+08	9979	1.4724	9965	.9713	.9909	•9804		1.0003	. 9993	. 9994	1.0000	. 9964
.250	.A745+DA	9978	1.4746	99+5	9554	•9859	•969 4	-3363	1.0005	• 9987	. 9989	1.0001	.9966
₹ 0.0	174-+09	9977	1.4772	• 9972	9363	.9797	•9562	+4148	1.0007	9978	•9982	1.0000	•9968
,350	1195+09	9975	1.4804	9894	9146	.9725		-4899	1.0011	• 9967	.9973	.9998	.9969
400	•134E+09	9973	1.4840	• 90 74 • 9862			9412	-5609	1.0014	. 9955	• 9963	•9999	.9973
.450	.1495+09	9971			•8902	•9642	.9241	.6274	1.0018	• 9940	.9950	• 9998	9977
.500			1.4882	.9825	.8636	9548	.9854	.6890	1.0923	• 9923	• 9935	.9999	.9982
	.162E+09	.9969	1.4930	9785	.83	.9445	8849	.7452	1.0027	• 9901	. 9917	.9997	. 9984
•559	•175£+89	.9966	1.4983	.9741	.895	.9332	.8629	.7958	1.0032	• 98 76	•9896	• 9995	.9987
.600	.186E+09	. 9954	1.5042	• 9694	.7721	•9209	.8399	•8408	1.0037	- 9848	. 9873	•9993	.9990
.650	•197E+D9	•9961	1.5106	. 9642	.7391	9078	.8159	.8801	1.0041	.9818	. 9845	•9993	•9995
.700	•297E+09	. 9958	1.5176	.9587	.7052	-8938	.7908	•9135	1.0046	• 9782	.9814	• 9991	•9997
.757	•216F+09	•9955	1.5252	•9528	.67º8	-8790	. 765?	.9411	1.0050	. 97 42	.9779	.9988	. 9998
.900	.224-+19	. 9952	1.5333	• 9465	.6361	.8634	•73 89	•9630	1.0053	. 9696	.9739	•9985	.9999
.850	•231E+09	. 995∩	1.5419	.9399	•601T	.8471	•7126	.9799	1.8055	•9650	. 9695	-9986	1.0001
.900	.237F+09	. 9947	1.5509	•9329	•5675	.6302	•6861	. 9914	1.0056	• 95 99	. 9647	.9985	1.0902
• 95 0	·2435+09	• 99 • 4	1.5504	• 92 55	-5338	.8127	•6594	.9979	1.0056	. 9542	. 95 94	.9984	1.0000
1.000	•247E+09	.9741	1.5791	.9178	.5018	.7947	.6330	1.0000	1.0054	.9484	.9536	9986	1.0000
1.050	.251E+09	.9938	1.5880	•9097	•4692	•7763	.6871	.9981	1.0050	9424	. 94 75	9991	1.0001
1.100	. 2547+09	. 9935	1.5999	.9012	.4385	.7576	.5816	.9923	1.0043	9363	9409	•9998	1.0002
1.150	•257E+09	.9932	1.5999	.892-	4001	.7386	•5566	.9832	1.0035	•9₹81	. 9340	1.0008	1.0004
1.200	.259E+09	•9929	1.6096	.8832	.7812	.7196	.5325	.9714	1.0024	9243	. 92 68	1.0025	1.0009
1.250	.260E+09	.9927	1.6190	.8737	.3546	.7095	-5090	9569	1.0019	9186	9194	1.0046	1.0016
1.300	.261E+09	.9924	1.6279	.8639	.3296	6815	-4864	9403	.9993	.9132	.9119	1.0073	1.0027
1.350	.2625+09	.9922	1.6363	.8539	.3061	6627	.4647	. 9220	.9974	.9084	9042	1.0107	1.0041
1.400	.262E+09	•99t9	1.6448	.8436	. 2 341	• 6441	.4440	9124	9953	9042	.8965	1.0149	1.0061
1.450	.2625+119	.9917	1.6510	.8331	.2636	.6257	.4241	8817	9929	•9006	.8889	1.0198	1.0086
1.500	.261F+09	.9915	1.6573	.8224	.2445	.6078	4050	.8600	9903	.8977	.8813	1.0254	1.0115
1,550	.2615+09	.9913	1.6529	.8117	2259	•5903	.3871	.8381	-9876	8959	.8739	1.0294	1.0154
1.600	.2605+09	.9911	1.6677	.8008	2105	.5732	.3698	-8156	.9847				
1.650	.258F 09	.9909	1.6718	.7900	.1953	•5566	•3535	7930	.9818	• 8946 8047	-8667	1.0396	1.0197
1.700	.257E+09	9907	1.6753	.7791	.1813	.5405	.3380			.8943	. 85 97	1.0479	1.0248
1.750	·256E+09	9906	1.6782	.7683	•1653	.5249		.7705	.9787	+8950	.8529	1.0572	1.0306
1.800	.254F+09	9904	1.6806	•7675	•1564	•5244 •5097	.3232 .3092	.7480	.9756	.8963	.8463	1.0672	1.8371
1.950	2525+09	9903	1.6825	7469	+1954 +1453	•509/ •495n		•7256 7077	.9725	. 8984	. 84 0 0	1.0779	1.8441
1.900	.2502+49	9901	1.6841	.7364		_	,2959	.7037	.9694	-9014	.8339	1.0696	1.0521
1.950	.2485+09	9910	1.6853	•7350	1351	.4879	.2631	.6818	• 9663	.9050	.8260	1.1018	1.0504
2.000	.246F+09	9199	1.6863	•7157	•1256	•4671	•2711	6605	•9632	9093	8224	1.1148	1.0595
	1170 107	• 2122	K O E GET G	1,12	.1169	.4539	.2596	-6397	•9602	• 91 45	.0170	1.1287	1.0795

F. (CONTINUED)

MACH	LOCAL ISENTROPIC	VISCOSITY	THERMAL CONDUCTIVITY	PRANDTL
	EXPANSION COEFF.	G/CM-SEC	CAL/C'i-SEC+K	NUMBER
դ. ըըո	Ī	.42737E-04	•19637E-03	.7112
.050	1.4442	•42640E=04	.19539E-03	•7115
.100	1.4800	.42586E-04	.19496E-03	•7115 •7114
.150	1.4687	.42496E-84	•19426E-03	.7111
.200	1.4723	.42371E-04	.19325E-03	.7108
.250	1.4680	.42211E-84	•19203E-03	.7103
.300	1.4686	.42015E-04	•19203E-03	.7098
350	1.4778	.41785E-B4	.18871E-D3	.7892
.490	1.4791	-4152NE-84	.1866E-03	.7085
. 450	1.4866	.41222E-04	.16436E-03	.7078
•500	1.4840	.40891E-04	•16161E-03	.7070
.550	1.4896	.40527E-04	.17902E-03	.7062
•600	1.4964	.40131E-04	.17600E-03	.7853
.659	1.5055	.39705E-#4	.17277E-03	.7046
.700	1.5078	.39248E-04	•16932E-03	.7039
.750	1.5151	.38761E-04	.16578E-03	.7928
.800	1.5209	.38247E-04	.16212E-03	.7016
.850	1.5331	.37706E-04	.15829E-03	.7887
. 90 0	1.5390	.37140E-04	.15432E+03	.7080
•950	1.5457	.36550E-04	.15021E-03	•6996
1.000	1.5560	.35939E-84	.14600E-03	•6996
1.050	1.5668	.35308E-04	•14175E-03	-6998
1.100	1.5746	.34661E=04	.13822E+113	•6966
1.150	1.5839	.34000E-04	•13465E+03	.6938
1.200	1.5960	•33329E-84	•13104E-03	.6914
1.250	1.6024	.32649E-04	.12743E-03	•6896
1.309	1.6115	•*1966E+04	.12382E-03	.6884
1.350	1.6198	.31280E-04	+12026E+03	.6876
1.400	1.6282	•30595E - 04	•11692E-03	-6865
1.450	1.6336	.29915E-04	.11360E-03	.686D
1.500	1.6381	.29248E-04	•11034E-03	•6861
1.559	1.6489	.28574E-04	.10715E-#3	.6867
1.600	1.6487	.27916E-04	.10402E-03	.6878
1.650	1.6546	.27269E-04	.10098E-03	.6893
1.700	1.6598	•26634E-84	.97667E-04	•6937
1.750	1.6605	.76011E-04	.95002E-04	•6945
1.800	1.6621	•254DAE-04	.9242BE-04	.6954
1.850	1.6674	•24802£-04	.89938E-04	•6965
1.900	1.6642	-24217E-04	.87531E-04	.6976
1.950	1.6673	.23645E-04	.85183E+04	•6990
2.000	1.6709	.23085E-04	.82885E+04	.7006

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TABLE IV. PEAL-GAS ISENTROPIC EXPANSIONS OF PARAHYCPOGEN

	`*.	€ 6. T	F = 200.9	K PT =	A.O ATM	PHOT =	.977E-03	SZCMR	SVT =1men	.481 MZS	EC		
МАСН	₽EVM	Z	CP/CV	SV/SVT	F/PT	1/11	PHO/RHOT	A+/A	SV/SVT	P/P1	*.**		
_	<u>.</u> .	_	0, 1, 2, 4	34. 34.	, ,	1011	PHUPAHUI	MYPA			T/TT	GAS VALUES	4/4
									,	CENITAE	10 TOF ME	GAS ANTOE?	,
0.000	0.	1.0953	1.3492	1.0000	1.0300	1.0000	1.0000	0.0000	1.0000	1.0000	1.0000	1.0000	1.0000
-050	.7575+07	1.0053	1.7489	•9998	• 9933	•9996	,90#4	.0860	1.9990	1.0001	1.0001	1.8000	9969
.100	.151E+08	1,7053	1.3488	. 9990	, 9972	.9983	.9958	.1712	1.0000	1.0002	1.0003	1.0000	9969
.150	•225E+88	1.8053	1.3486	9078	. 9849	•9961	.9889	-2550	1.0001	1.0005	1.0006	1.0000	9970
.200	.297E+08	1.005?	1.3483	• 4962	.9772	.9931	.9801	.3364	1.0001	1.0007	1.0010	.9999	9968
.250	•368E+08	1.0051	1.3430	. 9940	• 95 A &	.9892	•9695	•4150	1.0002	1.0014	1.0016	1.5/89	.9971
•30 n	•436E+88	1.0059	1.3475	• 9914	• 0412	.9846	.9567	.4899	1.0003	1.0019	1.0023	9999	9971
-35 0	.500E+08	1.0049	1.3471	. 9884	9212	.9792	•9412	•5609	1.0004	1.0027	1.0031	.9999	.9972
-400	•5625+08	1.8049	1.3466	.9850	.6988	• 97 3 0	.9242	.627?	1.0006	1.0035	1.0841	. 9999	9974
.450	.6205+08	1.7746	1.34£0	.9811	.8741	•9661	.9854	-6886	1.0008	1.0044	1.0752	9999	9976
•500	.674€+08	1.0745	1.3454	• 9769	+8475	•9585	.8849	-7446	1.0011	1.0053	1.0064	9997	.9976
.550	•724€ + 08	1.0943	1.3448	.9774	. 9194	.9503	.8631	7951	1.0013	1.0865	1.0078	9997	9978
.600	.770E+08	1.0042	2-3441	. 9574	•790i	.9415	.8402	.8401	1.0017	1.0078	1.0093	9997	9982
•650	.812E+08	1.0040	1.3435	.9622	.753€	.9321	.8160	8792	1.0020	1.0090	1.0109	9995	9984
.700	.849E+08	1.0038	1.3429	.9567	.7255	.9222	7911	9126	1.0025	1.0195	1.9126	.9994	.9987
•75 d	.881E+DR	1.0036	1.3422	9589	•€968	9119	7654	.9403	1.0030	1.0119	1.0145	9992	.9990
.800	.910E+08	1.0935	1.3416	9449	.66+9	.9011	.7393	9626	1.0035	1.0136	1.0164	9991	.9995
-850	.933E+0P	1.0033	1.3411	9386	.6328	.8899	.7125	.9793	1.0041	1.0149	1.0184	.9986	.9996
.900	.953E+08	1.0031	1.3406	.9322	• 6 0 1 D	.8783	6858	9911	1.0046	1.0164	1.0206	•998?	.9998
•950	•969E+08	1.0029	1.3402	9255	. F.694	8664	.6588	.9977	1.0056	1.0177	1.0236	.9974	.9999
1.000	.980E+05	1.0027	1.3799	9167	<u>.</u> 5.₹84	8542	6319	1.0000	1.0064	1.0191	1.0250	9968	1.0080
1.050	.988E+08	1.0025	1.3397	9118	• 5 8 7 B	8418	6050	• 9977	1-0073	1.0200	1.0274	.9956	•9998
1.100	.993E+08	1.0024	1.3397	9047	4783	8291	.57A6	9919	1.0083	1.0212	1.0297	•9947	.9996
1.150	.994E+B8	1.0022	1.3399	8976	44.95	8162	5575	9823	1.0093	1.0212	1.0321	.9934	.9994
1.200	•992E+#8	1.0020	1.3402	.8903	. 4217	.6031	.5268	9695	1.0104	1.0226	1.0544	.9918	
1.250	.987E+08	1.0019	1.3409	.8830	3949	7899	.5017	•9538	1.8116	1.0229	1.0367		.9990
1.300	.9805+08	1.0017	1.3415	8756	3692	7765	.6772	9356	1.0128			•9900	. 9984
1.350	9705+08	1.0016	1.3425	8082	.3446	7631	4533	.9152		1.0230	1.0390	.9881	.9976
1.487	.958F+88	1.0914	1.3478	8607	3212	7495	•4333 •4332		1.0141	1.0227	1.0412	9859	.9967
1.457	.945E+RA	1.0013	1.3454	.8532	2988	735R	4076	.8929	1.0155	1.0221	1.0433	. 9835	- 9956
1.500	•9295+0 A	1.0012	1.3473	.8457	• 2777	7221		.8690	1.0169	1.0209	1.0453	• 9806	.9941
1.558	9135+08	1.0010	1.3496	8382	•2577	7097	•3861 7657	8437	1.0164	1.0193	1.0471	9776	. 9924
1.600	.9955+09	1.0009	1.3522	. 6397	2387	•694F	.3653 .345°	•6175	1.0199	1.0173	1.0487	. 9743	.9905
1.650	.876E+09	1.000	1.7557	.8232	2200	.6806	•3260	•7903	1.0214	1.0145	1.0500	9784	.9880
1.700	8565+78	1.0007	1.3589	1157	2041	•6666		.7627	1.0230	1.0113	1.0511	. 9664	9856
1.750	835E+09	1.0006	1.3629	.9082	.1884		-*176	.7347	1.0246	1.0075	1.0520	9621	.9828
1.800	.814*+98	1.0005	1.3674	• 50 B Z		•6527	.2901	.7867	1.0263	1.0032	1.0524	• 9577	9798
1.859	•7935+BB	1.0004	1.3725	•0007 •7333	•1737	•6387	.2733	6786	1.0279	9981	1.0525	• 9529	.9764
1.900	•7725+08	1.0703	1.3781	•7959	.160N .1471	6247	.2574	.6505	1.0296	.9923	1.0522	.9477	.9727
1.950	.750E+08	1.0003	1.3844	• 7559 • 7785		.610F	2422	•6229	1.0313	.9859	1.0515	.9423	-9687
2.000	.7295+08	1.0702	1.3913	.7711	•1352 •1364	•5966 Enge	•22 ⁷ 8	•5957	1.0329	9789	1.0502	.9368	-9646
	# F C 2. 1 W U	T = 0 -1 10 C	143713	• 1 (11	.1741	•5825	.2142	•5691	1.0346	.9713	1.0485	.9311	-9503

S. (CONTINUED)

MACH	LOCAL ISENTROPIC	VISCOSITY	THEPMAL CONDUCTIVITY	PRANDTL
	EXPANSION COEFF.	G/CM-SEC	CAL/CM-SEC-K	NUMBER
Դ. թթը	•	686777 A.	79.75 L.C. A.S.	
•050	I 1.3695	.68533E-84	.37545E-03	.7032
.100	1.3497	•68594E=04	.37483E-03	.7032
.150	1.3497	•68333E+84	-37463E-03	.7032
.200	1.3487	•68231E+84	.37421E-93	.7032
250	1.3612	.68089E-04	.37363E-03	.7032
.300	1.3517	.67907E+04	•37289E-03	.7032
• 350	1.3555	.67687E-04	.371996-83	.7032
• 400	1.3549	6743BE-04	.37094E-03	.7031
• 450	1.3522	.67137E-114	-36974E-83	.7038
• 490 • 500		.66809E-04	.36841E-03	.7029
•500 •550	1.3499	•66448E-04	•36695E-03	.7027
.60n	1.3513 1.3524	.660566-04	.36536E-03	.7025
.650 .650	1.3486	.65633E-04	.36334E-N3	.7027
• 709		.65182E-04	•36051E-03	.7043
•750	1,3498	•64704E-04	•35753E-03	.7058
• 790 • 800	1.3477	.64202E-04	.35441E-03	.7073
•85n	1.3487	.63677E-04	•35115E-03	.7088
• 900	1.3455	631292-04	.34777E-03	.7193
• 950	1.3459	.62561E-84	.34426E-03	.7116
1.000	1.3437	.61975E-04	.34069E-03	.7129
1.050	1.3442	.61372E-04	.33702E-03	.7139
	1.3420	.60753E-04	•33326E=03	.7148
1.100	1.3447	.60118E+04	.32943E-03	.7154
1.150	1.342?	•59471E-04	• 32554E-03	.7158
1.200	1.342?	•58810E+04	•32160E-03	.7158
1.250	1.3431	.58138E+04	.317615-03	.7155
1.300	1.3439	•57455E-04	.31358E-03	.7149
1.350	1.3440	.56762E-8+	.30952E-03	.7138
1.400	1.3454	•56059E-04	•30543E+03	.7123
1.450	1.3460	·55347E-04	.30131E-03	.7103
1.500	1.3477	•54627£-04	•29716E+03	.7078
1.550	1,3503	•53898E-84	•29057E+03	.7106
1.600	1.3508	•53161E-04	•28 3 96E-03	.7130
1.650	1.3551	•52415E- 0 4	•27 7 32E-03	.7150
1.700	1.3582	•51662E-04	•27067E-93	.7167
1.750	1.3625	.50902E+84	.26401E-03	.7179
1.800	1.3660	.50134E-04	•25733E-03	.7187
1.850	1.3698	•49358E-04	•25065E-03	.7191
1.900	1.3758	•48574E-04	•24396E-03	.7191
1.951	1.3819	•47782€±04	.23726E-03	.7186
2.000	1.3888	•46983E-04	.23056E-93	.7177

ORIGINAL PAGE IS



17

PHALHGAS ISENTROPIC EXPANSIONS OF PAPAHYCPOGEN

	7.17		- -		··			*** OF 7 A					
		н. тт	= 300.9 K	्र प्रच	H.O ATM	PHOT =	•652E=93	G/CH3	SVT =1315	.784 H/Si	EC		
MACH	PE/M	?	CBNLA	SV/SVT	PZPT	TZTT	RHO/RHOT	A+/A	SV/SVT	P/PT FELATIVE		RHOZRHOT GAS VALUES	A+/A
0.000	0.	1.9847	1.3706	1.0000	1.0000	1.0000	1.0000	0.0000	1.0000	1.0000	1.0000	1.0000	1.0000
• 950	.477E+97	1.0047	1.7961	.9997	.998₹	.9995	.9988	.0864	1.0000	1.0001	1.0000	1.0001	1.0917
.100	.951F+N7	1.0047	1.3868	.9990	9930	.9981	9949	1720	1.0000	9999	1.0001	.9999	1.0015
•150	•142E+08	1.9047	1.3858	.9977	9844	9957	9888	.2561	.9999	1.0000	1.0001	.9999	1.0015
.200	.188E+D8	1.0046	1.385€	.9958	.9727	9923	9803	.3379	.9996	1.0002	1.0003	1.0001	1.0015
•250	·2325+08	1.884ć	1.3953	.9935	9576	.9881	- 96 93	• 4167	9997	1.0001	1.0004	9999	1.0013
-300	.275E+0R	1.0745	1.3849	. 9907	.9₹08	.9820	9563	.4920	.9996	1.0003	1,0006	. 9999	1.0012
•350	•316E+08	1.0344	1.3944	. 9874	. 9193	.9769	-9413	•5631	.9995	1.0005	1.0008	1.0000	1.0011
•400	.3555+08	1.80+3	1.3820	.9837	.8963	.9701	.9243	-6295	9993	1.0008	1.0011	1.0001	1.0010
.450	.391E+08	t.00→2	1.3832	9795	•E712	.9625	•9056	•6989	.9997	1.0010	1.0015	1.0001	1.0009
•500	•426E+08	1.9941	1. 7825	.9749	.8441	.9541	.8852	.7469	.9990	1.0013	1.0018	1.0061	1.8007
.550	.457E+118	1.0040	1.3918	. 9699	.8155	.9451	.8635	.7973	9988	1.0017	1.0023	1.0001	1.0006
•600	.486E+88	1.0039	1.3809	• 9645	.7857	.9354	.8407	.8421	9986	1.0022	1.0028	1.5003	1.0006
•650	•513E+08	1.0037	1.3799	.9587	.7547	•925?	.8166	.8808	9994	1.0026	1.0034	1.0002	1.0003
.700	•536E+08	1.0036	1.7789	• 9526	•7273	• 91 44	.7918	9140	9982	1.0032	1.0040	1.0003	1.0002
.750	.557E+08	1.0034	1.7777	. 946?	.6912	.9532	.7663	9412	.9980	1.0036	1.0048	1.0003	1.0000
-800	•575 <u>5</u> +08	1.0033	1.3765	9395	6591	.8915	.7483	• 9632	.9979	1.0046	1.0056	1.0005	1.0000
.850	.590E+08	1.0932	1.3752	•9326	.6270	.8794	.7148	.9797	.9977	1.0055	1.0065	1.0006	.9999
• 900	.603E+08	1.0030	1.3737	.9254	•5 9 51	.8670	•6875	.9911	.9975	1.0065	1.0075	1.0007	, 9999
•950	+61 3E+08	1.4929	1.3722	• 91.80	.56₹7	.8544	.6614	.9978	.9974	1.0076	1.0066	1.0009	.9999
1.000	.621E+0B	1.0027	1.3706	.9184	.5370	.8415	• 63 46	1.0000	.9973	1.0089	1.0098	1.0011	1.0000
1.650	•626E+88	1.0026	1.3690	•9025	.5030	.8285	.6884	.9980	.9972	1.0102	1.0111	1.0012	1.0001
1.100	•629E+08	1,0025	1.3673	.8947	•47₹d	8153	-5825	.992?	.9971	1.0116	1.0126	1.0013	1.0001
1.150	•630E+88	1.0923	1.3554	•846™	- 44-5	•8050	-5568	.9827	.9971	1.0128	1.0141	1.0012	.9999
1.290	+629E+88	1.0922	1.7676	.8786	. 4183	.7886	.5318	.9704	.997.1	1.0144	1.0157	1.0012	. 9999
1.250	.627E+08	1.0021	1.3617	•8703	.3923	.7752	-507 ₹	.9553	.9971	1.0161	1.0175	1.0013	1.0000
1.300	•623£+08	1.0719	1.3597	• 8621	. 3674	.7619	. 4835	.9380	.9972	1.0179	1.0194	1.0013	1.0002
1.350	+617F+0B	1.0019	1.3579	. 8539	.3434	.7485	.4602	9180	.9973	1.0192	1.0213	1.0008	.9998
1.400	. 61 0೯ + 0 9	1.9017	1.3558	.8455	.3208	.7352	.4377	.8966	.9975	1.0209	1.0234	1.0005	.9997
1.450	•601E+08	1.001£	1.3539	-8371	2993	.7220	4158	.8736	•9977	1.0224	1.0256	1.0000	9994
1.500	*592E+08	1.0015	1.3528	.8788	·27#9	.7089	.39+7	.8493	•998D	1.0238	1.0278	9993	.9990
1.550	•582E+08	1.0014	1.3501	8205	.2597	•695 P	.3744	.8242	.9984	1.0253	1.0302	+9986	.9986
1.600	.5715+08	1.0913	1.3483	.8122	.2415	.6829	. ₹549	.7983	9988	1.0267	1.0326	.9977	.9981
1.650	.559F+D8	1.0012	1.3466	. 8747	.2245	.6701	.3361	.7716	.9992	1.0278	1.0350	9965	.9973
1.700	.547F+O8	1.0011	1.3449	• 7953	.20 P4	• 657 5	+3181	.7449	.9997	1.0287	1.0375	9950	.9964
1.750	.534E+08	1.0010	1.3434	.7877	.1933	.6450	- 4098	.7178	1.0003	1.0293	1.0401	•9933	.9953
1.800	• F 2 D F + D A	1.0910	1.3421	• 7797	.1792	.6327	.284T	•6907	1.0009	1 . 02 97	1.0426	9913	9979
1.850	•59 7 € • 0 9	1.0009	1 * 5 42 8	.7717	.16F0	.6205	.2686	.6637	1.0016	1.0298	1.0452	9891	.9923
1.900	.4935+08	1.0008	1.3398	•7639	.1537	.6084	•2536	.6370	1.0024	1.0297	1.0477	9867	.9906
1.950	•479E+88	1.0003	1.3789	•7561	.1422	•5965	.2393	.6106	1.0032	1.0292	1.0502	.9840	9887
2.000	.465E+08	1.0907	1.3383	.7-83	-1314	•584ª	•225 6	.5844	1.0040	1.0261	1.0526	.9807	.9562

H. (CONTINUED)

MACH	LCCAL ISENTROPIC	VISCOSITY	THERMAL CONDUCTIVITY	PRANDTL
	EXPANSION COEFF.	G/CM-SEC	CAL/CM-SEC-K	NUMBER
	EX. WESTON SOCIET	0# GH = 35 C	GAEL CH - 3EC-K	NONDEK
0.000	I	.89712E-04	•46209E-03	.7102
.050	1.4197	.89754E-04	.46196E-03	.6905
.100	1.3750	.89666E-04	.46157E-03	.6905
•150	1.3941	.8952BE-04	.46093E-03	.6905
.200	1.3977	.89316E-04	.46003E-03	-6906
• 25 0	1.3853	.89056E-04	.45889E-03	.6907
.300	1.3927	.88741E-04	.45751E-03	.6909
.350	1.3922	.88373E-04	-4559NE-D3	.6910
.400	1.391?	.87954E-04	·45407E-03	.6912
•450	1.3896	.87486E-84	•45204E-03	•6914
.500	1.3870	.86972E-04	.44980E-03	.6916
•550	1.3883	.86413E+0→	.44739E-03	•6919
•600	1.3882	.85813E-44	.44480E-03	.6922
•650	1.3830	.85175E-04	.44213E-03	•6924
.700	1.3852	.84502E-04	.43941E-03	.6926
.750	1.3814	.83795E-04	.43656E-D3	•6927
• 800	1.3825	.83959E-04	.43361E-03	.6938
• 857	1.3803	.82296E-04	.43055E-03	.6932
• 389	1.3785	•81509E-04	•42742E-03	•6935
• 95 D	1.3776	.80701E-04	.42421E-03	.6938
1.000	1.3760	.79874E-84	-42094E-03	.6941
1.959	1.3738	,790325-84	-41762E-93	.6945
1.100	1.3717	.78176E-04	.41427E-03	.6949
1.150	1.3677	.77310E-04	.41089E-u3	•6953
1.200	1.3679	.76435E=84	•48750E-03	•6957
1.250	1.3663	• 75552E=¶4	.40402E-93	• 5962
1.300	1.3649	.74665E-04	.40023E-03	.6973
1.350	1.3593	.73774E-04	.39644E-03	• 5983
1.400	1.3596	.72881E-04	.39267E-03	•6992
1.450	1.3564	.71988E-84	.386925-03	.7001
1.500	1.3546	.71895E-84	.38519E-03	.7008
1.550	1.3534	.70204E-04	.36149E-03	.7014
1.600	1.3517	.69315E-04	.37782E-03	.7019
1.650	1.3488	.6843DE-04	.37419E-03	.7022
1.700	1.3473	.67549E-04	•37859E÷03	.7023
1.750	1.3455	.66671E-N4	.36704E-03	.7022
1.800	1.3437	•65798E-04	•36353E-03	.7817
1.050	1.3430	.64929E-84	.35856E-93	.7038
1.900	1.3423	.64065E-84	•35318E-93	.7066
1.950	1.3416	.63206E-04	.34786E-03	.7091
2.000	1.3392	.62352E-84	.34260E-03	.7113

ORIGINAL PAGE IS OF POOR QUALITY

TAPLE V. REAL-EAS INENTROPIC EXPANSIONS OF PARAMEROGEN

BHOL = '0716-03 CYCH2 = 2AH = 224"16" = 10H8

							•	* *	•				
0650*1	9541.1	1200.	96 16 *	1298*	7161°	6515.	4805°	£991*	1989*	1566°I	2298*	1135+10	0074
1050.1	19191	6108.	5776*	6598*	1214	8161.	2531	7991.	1969 ·	£ 266° I	6298*	1136+10	069*
1*0+20	8476"	. 8133	1016*	8698	2716	£ 8 8 7 °	6125	1-15.	£101.	1006	8528	01+3211*	009*
65£0°l	1.1348	6010	7906	0 2 Z 8 *	0999*	9527°	1255	9622*	1914.	4000°2	21.58*	175E+10	055*
1.0296	1.1226	7458.	4£ 06 *	6118.	#529°	4£44*	8895*	IonS.	1590	2.0022	9898*	01+2511.	085
1.0237	6011.1	. 8308	1106*	1558.	6768 *	6195*	6483*	8292 *	1072*	2.8033	0798*	.111E+10	054*
7°11'6	1.1003	1458.	566 9 °	7988 °	9216	2195*	7109	1585.	£151 *	2,00,5	5798	01+3011.	004
1,10,1	9600*1	9248*	5 968 •	9 NP 8 *	4116*	010≤•	×819*	•3056	4297.	2.00.5	0499	01+3601.	042*
7°0105	1.9800	7058.	£868.	£368.	7276*	5125	55k9*	2775	8777.	5-00-2	9598*	01+3001*	005.
1708.1	1.0712	£449 *	6969 *	6668	1296*	9275	• 6535	D2+E+	3887.	0500.5	2998*	01+3701.	052.
5400 1	1°06S9	£498 °	0006*	9406*	8746*	9495+	1119*	1175.	0262	8700.5	Pe38.	10 PE+10	032.
1.0023	1990*1	5178.	ST06*	69993	T586*	9985*	2699*	9=6 -	6878.	£766°6	9498*	01+3901	051
1.00.1	E870*T	88 78 .	6£66 *	1-16-	* 8635	66 n 9 e	9707.	7267	٠٥٤٥٠	6500 2	4808.	1036+10	011.
1000*1	2 T 7 O * T	2998*	9906*	0616*	1866*	0753.	1924.	*157*	.6319	50002	26 99	01+3101*	050*1
6666*	7*0229	9£68°	0016*	8726*	6666*	4959*	1692	2087*	5£78°	SF00.5	0078.	60+4486*	00001
1.0002	1.0303	8 T 06 *	5£ 16 *	2626.	8866.	*089*	\$894.	ulta.	2558*	1700*2	8078.	60+3096*	0.56*
1108*1	1.0253	5006 *	5416.	5426*	. 9923	*** 04 *	\$187°	9275*	6998*	2.0050	4178.	60+3££6*	006*
1*0053	1020*1	6516	6126	6616	9888	4821	F 0 0 5 .	8725*	2818.	7800.5	9278	60+3126	038
7*00*T	0710.1	* 65 36	6926*	2546*	. 9672	5251.	3618.	1909.	0068.	*908*2	3878.	90+32540	008.
7900*1	SETO*T	10 E6 *	. 9322	5056*	£476 *	1914	9958	6179	1106.	690D.S	9478.	68+3628°	0.08.
6800 • I	5010°1	0926	1126.	1556*	6126*	6664*	£+48.	D378.	1216.	F700.5	3478	60+3667.	007.
1°0150	1000*1	2546 •	8276	6096*	1168.	1128.	5176.	9012	49227	4200°c	3918.	60+3852*	859*
0510 1	6500*1	1296*	26 % °	8996*	2458	4948*	2888.	9-91	6556.	8700.S	2778.	68+3617	009.
SOTOT	770071	6956 *	0956*	4046.	9110	2798.	2706*	4877.	9276*	6208*2	2878.	60+3899*	055*
1°0550	1.0051	£596 ·	* 9655	£546.	8597.	6488°	1919.	2110	1146°	8700.5	2678.	60+3019*	005*
15201	1.0026	2116	28 96 *	9646	8707.	FY NP .	5556*	92+8*	£096°	42uü°c	7099	68+3996*	097
1.0290	710017	6926*	2716	3116	1479*	9526*	99*6*	8279.	5886.	+100.S	5178.	68+3115*	004*
1.0322	9000°t	0296°	96461	\$486.	9885	8276*	9866	Du06*	7546°	1708.5	1288	60+3£57*	052*
1.0352	7000°T	9985*	9786	9066*	1805.	8956	2696*	9526	7186.	2°00'E	4288 6288*	6.0+3267*	005.
1,0361	1.0003	9066*	2696*	.9933	**350	1 696.	7816°	1476*	5786.	9900°2	7288	80+31FF.	
7040 *1	T000*T	6266*	4 9929	7866.	1155.	7096*	7386.	9596*	7199.	ے 1000 ک م*نانا9ک	7288° U488°	90+3785	*520 *500
1*0#53	1000*1	9966*	0966*	9466*	9992	6986*	1566.	5066	£466°	5*88*2	7788	9043595	002
3£ 70°I	2000**	£866 °	2966	6966*	5641.	0966°	9966	2166*	£790.	2 ± 0 0 ° 2	1788°	60+3521*	011.
9550°7	1000*1	9666 *	9666 *	1066.	1060	8866.	1666'	6466°	5666°	3900°Z	6788*	80+3878	0 S O *
1.0000	0000°T	1.0000	0000.1	1.0000	0000.0	0000.1	0600*1	0000.1	4818.1	2900°2	0288.	• u	
				*				3000 +	4000 \$	2300 2	0366	עי	010.0
	CAS VALUES		3VITAJ3	y									
A1+A	тонялоня		19/9	145/45	ANA	RH0/RH0T	11/1	14/4	TUSIVE	CP/CV	Z	HV38 +	HDDH

SATURATION GOUNDARY REACHED.

A. (CONTINUED)

MACH	LOCAL ISENTROPIC	VISCOSITY	THERMAL CONDUCTIVITY	PRANDTL
	EXPANSION COEFF.	G/CM-SEC	CAL/CM-SEC-K	NUMBER
0.000	Ī	.24535E-04	.93873E-04	.8048
.050	1.8048	-24461E-04	.93536E-84	.8053
.100	1.7541	.24403E-04	.93271E+04	.8056
.150	1.7747	.24308E-04	.92836E-84	.8062
.200	1.7649	.2417EE+04	.92326E-04	.8062
.250	1.7657	.24008E-04	.91652E-04	.8865
.300	1.7581	.23806E-04	.90819E-04	.8070
.350	1.7610	.23573E-04	.89831E-04	.8079
.400	1.7613	.23310E-04	.88714E-04	.8089
.450	1.7518	.23019E-D4	.87390E-84	.8109
.500	1.7556	.22704E-04	-86087E-04	.8120
.550	1.7505	.22366E-04	.84624E-04	.8139
.600	1.7443	.22007E-04	.63007E-04	-8165
.650	1.7493	.21633E-04	.81590E-04	.8168
.700	1.7378	.21242E-84	.79912E-04	.8192
.759	1.7487	.20840E-04	.78437E-04	.8191
.800	1.7357	.20427E-04	.76873E-04	.8197
. B50	1.7273	.20005E-04	.75179E-04	.8213
• 900	1.7293	.19578E-0+	.73385E-04	.8241
• 95 n	1.7217	.19146E-84	•71648E-94	.8261
1.000	1.7195	.187115-04	-69863E-04	.8289
1.050	1.7133	.18272E-04	.68028E-04	.8320
1.100	1.7163	.17833E-04	.66269E-04	.8340
1.150	1.7085	.17393E-D4	-64596E-04	.8348
1.200	1.7120	.16957E-04	.62993E-04	.8349
1.250	1.7067	.16524E-04	.61369E-04	.8355
1.300	1.7025	.16095E-04	.5973+E-04	.8364
1.350	1.7021	.15671E-04	.58099E-0+	.8379
1.400	1.7007	.15255E-94	.56473E-04	.8398
1.450	1.6962	.14845E-04	.54877E-04	.8420
1.500	1.6942	.14442E-04	.53507E-04	.8414
1.550	1.6891	·14048E-04	•52163E-04	.8411
1.600	1.6881	.13663E-04	.50773E-114	.8423
1.650	1.6841	.1328EE-04	.49349E-84	.8451
1.700	1.6814	.12918E-04	.47903E-04	.8494

SATURATION BOUNDARY REACHED.

ORIGINAL PAGE IS OR POOR QUALITY A CONTROL STORY OF ST

3 7

TARLE V. REAL-CAR ISENTROPIC EXPANSIONS OF PARAHYCROGEN

	·	P. TT	= 50.0	C PT =	10.8 ATM	₽H01 =	•535E-8?	SZCM3	SVT = 574	.794 M/S	EC		
MACH	PE/M	7	CBNCA	SVZSVT	FZFT	1/11	RHOZPHOT	4*/4	SV/SVT	P/PT FELATIVE	T/TT	RHO/RHOT GAS VALUES	A+/A
	•											4.5 TACOE.	
0.000	0.	.9181	1.9905	1.0000	1.0000	1.0000	1.0000	7.0000	1.0000	1.0000	1.0000	1.0000	1.0000
.050	• FR4 F + D A	.9180	1.900A	999=	9979	.9991	•9988	.9897	.9998	•9996	- 9996	1.0000	1.0402
100	•116F+09	.9179	1.0911	. 9981	.9912	. 9965	•9949	•1785	,999 0	.998?	. 9985	• 9999	1.0393
•15¶	*174E***9	9176	1.9014	.9955	• 9 80.7	.9922	. 9899	.2655	• 9379	.996?	.9967	1.0001	1.0362
.200 .250	.230 <u>0</u> +19 .2856+09	.9172	1.9719	9923	9560	• 986?	•988+	.3498	.9962	. 9933	• 9941	1.0001	1.0366
300		.916A	1.9024	.9880	. 0475	.9787	96 95	+4305	• 9942	• 98 96	• 9909	1.0001	1.0344
	•339£+0°	.9163	1.9031	.9829	9258	9696	• 9568	.5072	.9917	. 9855	.9870	1.0804	1.0321
•35D	•398£+09	.9156	1.9737	9769	• a d 4 u	•9591	* d + 5 J	•5790	*aBafi	.9807	. 9826	1.0007	1.0295
•40n	• ## DE + # 3	. 01 49	1.9743	.9701	.8775	.9472	.9751	•6455	9955	.9753	.9776	1.0611	1.0265
.450	.487F+09	.9142	1.9950	.9627	.P440	.9342	-9072	.7066	•9420	•9698	.9721	1.0019	1.0236
•500	* £ 325 + 80	• 91 34	1.9056	95.45	•8125	.9201	•887 6	.7616	.9781	.9638	.9661	1.0028	1.0204
.5=0	•57 • 5+09	.9126	1.9060	.9-57	• 77 07	.9050	•8668	.6105	.9739	.9577	9598	1.0039	1.0172
•600	•614E+19	.9117	1.9764	•9₹64	.7461	.8891	.8451	.8536	• 9695	.9517	. 9531	1.0055	1.0142
•657	.E52:+119	. 91 3 9	1.9066	•9266	.7118	.8724	.8223	• 89 0 •	.9649	. 9455	9462	1.0072	1.0111
.708	• E865+09	.9100	1.90€7	•9153	• E 774	•8552	.7992	• 9216	•9602	.9396	.9390	1.0096	1.0085
•750	•718E+09	.9091	1.9867	•9057	<u>.6430</u>	.8375	4775 4	.9470	9553	•9339	.9317	1.0123	1.0061
	•7+8F+119	9083	1.9065	.4948	•6 89 1	.8194	.751+	.9670	.9503	92 84	. 9742	1.0154	1.0039
.850	.775E+D9	9074	1.9762	.8836	.5758	.8010	.7273	•9820	•9+53	. 92 34	.9157	1.0192	1.0023
•901	.800E+09	• 91166	1.90=7	. 9722	• 5 4 7 3	.7824	.7031	• 9923	•9402	.9188	• 9092	1.0234	1.0011
950	•822£•89	.9058	1.9851	.8607	.5116	.7638	•6730	. 9981	.9352	•9145	9016	1.0280	1.0002
1.000	•8+2I+D9	•9159	1.3045	+8+91	.4.912	.7451	6551	1.0000	.9391	9108	.8941	1.0334	1.0000
1.057	*8665*ud	· OF LT	1 •ुप्तर?	.837→	" <u>-</u> 519	.7265	.6315	.9962	.9257	.9076	.8866	1.0392	1.0003
1.100	•876F+D9	• qn 36	1.9029	.8257	· +2*9	.7879	.6993	.9933	9202	9050	. 8793	1.0457	1.0011
1.150	•891F+D9	•9030	1.9019	.8140	•3971	•689€	•5855	-9853	.9154	.9028	.8720	1.0527	1.0025
1.200	•993€+09	•9024	1.9010	.6024	•3717	.6715	.5632	9749	.9186	9014	.8648	1.0604	1.0046
1.250	•914÷+D9	.9018	1.9007	.7999	• 34.75	•653¢	.5413	.9621	9050	.9001	.8577	1.0683	1.0071
1.390	<u>. 9735</u> +99	.9n13	1 duu#	.779+	.3267	.6358	•5201	9475	9016	.8995	. 8507	1.0770	1.0103
1.350	.931∈+89	.9098	1.9702	.7681	• 3031	.6184	4905	9311	.8972	.8994	8439	1.0863	1.0140
1.400	.938F+69	. 9003	1.8000	7559	.2828	.6814	4704	.9133	.8930	.8998	8371	1.0961	1.0183
1.450	•9436+09	. 4999	1.8995	.745A	.2637	.5847	4601	8944	.8888	.9008	.8306	1.1064	1.0231
1.508	• 947F+B9	.8995	1 # 8500	.7348	.2458	.5684	. 4414	.8745	.8848	9024	. 8242	1.1174	1.0286
1.557	•951E+09	.8992	1.8984	.7239	.7291	.5525	4234	8541	-8608	9047	8180	1.1292	1.0340
1.600	• 95 ₹E+ 0 9	.8949	1.4977	.7132	-2135	.5370	4861	.8331	.8770	.907€	.8120	1.1416	
1.650	•9555+09	.8986	1.8969	.7026	.1990	.5220	.3895	8118	.8732	.9112	+8062	1.1547	1.0416 1.0490
1.709	•9555◆#9	.8984	1.8957	.6922	·1854	•507₹	.3735	.7902	.8695	9157	.6006	1.1683	
1.759	.955=+09	. 4947	1.8945	.682N	.1728	4931	35 91	7684	•8650	.9199	.7952		1.0569
1 4 8 11 11	.9555+09	.8988	1.0033	.6719	•1610	4794	.3434	7467	•862£	.9251		1.1825	1.0654
1.0=0	.9547+B0	8978	1.8919	.6629	1581	4660	3293	.7251	.8592		•7900	1.1973	1.0745
1.900	•952F+89	.8977	1.8906	•6F23	•1399	.4530	•3159	7138	• 654°	.9310 .9376	• 7850 7800	1.2126	1.0842
1 • 🕶 n	.950[+09	.9976	1.8867	6428	1375	.44115	. 30 30	.6827	•8529		•780 <u>2</u>	1.2291	1.0946
5.499	•9475+NP	8974	1.8979	6335	1217	4284	.2906	•6619		.9446	. 7755	1.2459	1.1055
	-	•		• • • • •	• • • • • • • • • • • • • • • • • • • •	\$ ~ C UM	♦ t 3 ti C,	10072	•8499	• 9522	.7711	1.2632	1.1169

B. (CONTINUED)

масн	LOCAL ISENTROPIC EXPANSION COEFF.	VISCOSITY G/CM-SEC	THERMAL CONDUCTIVITY CAL/CH-SEC-K	PRANOTE NUMBER
	· ·	07.704.7.01	400015 07	7674
0.000	Ĭ	•26381E-04	.10091E-03	.7631 .7632
.050 .100	1.7650	.26304E-04 .26245E-04	.10058E-03 .10034E-03	• 7632 • 7632
•100 •150	1.7184 1.7607	• 26148E-04	.99933E-04	.7633
			.99378E-84	.7634
• 200	1.7462	-26012E-04		
• 250	1.7334	.25840E-04	.98650E-04	.7635
.300	1.7494	.25633E-04	•97769E-04	.7636
• 350	1.7428	•25393E-04	.96785E-04	.7641
• 400	1.7364	.25121E-04	•95651E-04	.7645
•450	1.7452	.24821E-04	•94311E-04	.7657
.500	1.7365	.24494E-04	.92829E-04	.7672
•550	1.7336	• 24144E-04	.91247E-04	.7690
.690	1.7374	.23772E-04	.89563E-04	.7708
.650	1.7272	.23361E-04	.87564E-04	•7752
.700	1.7327	.22973E-04	.85879E+94	.7764
.750	1.7264	• 22552E-04	.84136E-04	.7776
.800	1.7240	.22119E-04	.82331E-04	.7792
.850	1.7247	.21677E-04	.80475E+04	.7811
• 900	1.7204	•21227E+84	.78578E-04	.7632
.951	1.7147	.207725-04	.76727E-04	7848
1.000	1,7151	.20313E-04	•74965E-04	•7854
1.050	1.7113	•19852E-04	.73155E-04	.7867
1.100	1.7097	•1939NE-84	.71299E-04	.7885
1.150	1.7054	.18929E-114	.69450E-04	.7904
1.200	1.7055	.18471E-04	.67648E-04	.7920
1.250	1.6992	.18013E-04	.65847E-04	.7937
1.300	1.7010	•17559E-04	•64126E-04	.7944
1.350	1.6987	•17189E-84	•62468E=N4	.7945
1.400	1.6958	.16664E-D4	.60804E+04	.7950
1.450	1.6928	•16226E-04	•59164E-04	.7954
1.500	1.6918	.15795E-04	•57556E-04	.7959
1.550	1.6912	.15371E-0→	•55 9 54E+04	.7968
1.600	1.6998	.14956E-04	.54367E-04	.7980
1.650	1,6876	.14549E-84	.52800E-04	•7996
1.700	1.6846	•14150E-04	.51391E-04	•7995
1.750	1.6821	.13761E-04	.49949E-04	.8006
1.800	1.6801	.13301E-04	•48487E-84	.8028
1.850	1.6792	.1301nE-04	.47015E-04	.8060
1.900	1.6787	.12648E-04	•45542E-04	.8104
1.950	1.6759	.12296E-84	.44186E-04	.8136
2.000	1.6732	•11953E=04	.42930E+04	.8161

DRIGINAL PAGE IS OF POOR QUALITY TABLE V. REAL-CA ISENTROPIC EXPANSIONS OF PARAHYDROGEN

		ॅंब्रिंट ग	= 60.0	K PT =	10.0 ATM	₽u0⊺ =	.428F-02	SZCHT	5VT = 534	.188 M/SE	c		
MACH	PE/M	7	COVEN	SV/SVT	P/FT	T/ TT	PHQ/PHQT	A+/A	SV/SVT	P/P1	1/11	RHO/PHOT	A+/A
							•					GAS VALUES	
0.000	0.	0553										. –	
•050	.453E+08	.9557	1 7753	1.0000	1.0000	1.0000	1.0000	0.0000	1.0003	1.0000	1.0000	1.0000	1.0000
•100	.984E+88	•9556 •9555	1.7700	• 9996	.9979	.9992	.9987	.0890	•9998	. 999c	•9997	1.0000	1.0312
.150	.135-+99	.9551	1.7755	.998*	.991€	.9967	9951	.1779	.9993	. 9986	. 9987	1.0001	1.0308
.200	•179E+09	•955B	1.7773	•996₹	9811	.9925	.9888	.2633	-9985	• 9966	.9970	1.0000	1.0298
.250	.2215+09	• 95 • 7	1.7785 1.7799	993	• dass	.9868	.9884	.3471	.9973	. 9942	. 9947	1.0001	1.0288
.300	•263E+09		-	.9897	.9438	.9796	•9696	.4276	• 9 9 5 9	•9910	• 9918	1.0002	1.0274
•300 •359	• Z032+09	.9543	1.7915	• 9952	.9274	•970a	. 9567	•5039	•9941	•9871	- 9883	1.0003	1.0256
•400		.9538	1.7833	.9401	.9030	•9606	,9418	.5757	• 991 9	9825	. 9842	1.0006	1.0236
	.3415+09	.9533	1.7853	.9741	.8758	•9491	9251	•6424	•9495	• 9779	• 97 95	1.0008	1.0214
•450	.3785+09	.9527	1.7873	9674	.8465	.9364	•9068	.7035	.9868	.9727	• 9744	1.0014	1.0192
•500	.413E+89	.9521	1.7804	9501	•81F3	•922 6	.887B	.7589	.9878	.9671	• 9687	1.0021	1.0168
•550	•₩ ₩€ ₹ + ₿9	.9514	1.7317	•9522	.7877	.9078	•9650	.8083	.9816	.9613	.9627	1,0030	1.0144
.600	.477E+110	.9307	1.7936	• 6+ 4 2	.74#9	.8329	.8439	.8515	•°770	• 955 <i>2</i>	• 9563	1.0040	1.0118
•650	•505E+09	• 95 00	1.7955	9346	•71-7	.875€	.8211	.8890	.9733	. 9494	. 9495	1,0057	1.0096
.700	•532E+09	.9493	1.7972	9251	.6801	.8584	.7976	•9205	• 9693	• 9434	. 9425	1.0076	1.0074
•75 D	-5565+89	. 94 86	1.7987	9151	•645€	.8407	•7736	• 9462	•9652	• 937 6	.9353	1.0799	1.0053
•800	•579E+89	.9479	1.8909	•90.+7	. € 11 h	8226	.7493	• 9566	•9609	•9320	•9279	1.0126	1.0036
.851	+599E+89	9472	1.9016	.89.41	•5777	•8042	•7248	.9817	• 9565	- 9266	- 9284	1.0157	1.0020
•900	•618E+09	• 9465	1.8019	.8931	.5449	.7856	.700*	• 9921	•9519	.9216	•9128	1.0194	1.0009
•950	+6345+89	• 9 • 5 A	1.8025	.8719	.5131	.756 9	•6761	.9981	.9474	• 9171	• 90 52	1.0237	1.0092
1.000	•649E+09	945?	1.8029	•8696	• - 823	.748 ⁿ	6529	1.0000	.0427	.9139	.8976	1.0285	1.0000
1.050	•662E+09	.9446	1-8031	.8491	•452B	.7292	• 62 82	• 9982	•93R1	• 90 94	.8900	1.0337	1.0002
1.100	•6745+09	9440	1.8932	.8376	. 4244	•7106	.6047	.9930	.9335	.9062	.8825	1.0396	1.0009
1.150	.684E+89	9434	1.8030	8269	.3975	•6921	.5818	.9850	.9289	• 90 37	.8751	1.0461	1.0022
1.200	•6935+119	9429	1.8929	• B 1 44	•371 <u>9</u>	•67₹7	■ 55 95	.9745	. 9243	.9019	.8678	1.0534	1.0042
1.250	790=+09	.9424	1.8024	.8029	.3476	•6557	.5376	.961E	9198	.9004	.A606	1.0610	1.0065
1.300	.706±+69	.9419	1.891	7914	.3247	.6379	•5164	9469	.9154	.8997	8535	1.0694	1.0097
1.350	+7115+99	49415	1.8914	•7799	.3031	.6285	•495B	.9304	-9111	.8994	.8466	1.0783	1.0133
1.400	•7155+B9	• ⁹ • 1 1	1.8003	•7686	. 2924	.6034	.4759	.9127	• 90 6 B	. 8998	,8₹99	1.0880	1.0176
1.450	+7185+85	•9→97	1.8401	.7574	• 263E	.5865	•4565	.8936	.9027	.9006	.8333	1.0980	1.0222
1.500	•7°15+09	.9+03	1.7995	•746₹	•2•£8	.5783	380	8738	-8986	• 90 22	1269	1.1089	1.0278
1.550	.722E+09	•9480	1.7988	.7353	• 5500	.5543	.4290	.8532	. 6947	9043	. 8206	1.1202	1.0338
1.600	• 72 3E + 0 9	•9397	1.7984	.7246	.2133	.5387	.4927	.8320	8909	9066	.8145	1.1320	1.0402
1.650	•723E+99	.9395	1.7979	•7139	1957	.5235	.3860	.8104	8873	.909ć	. 80 65	1.1444	1.0432
1.700	.722F+09	.9393	1.7975	.7035	.185P	.5087	.3791	.7887	.8837	9132	.8027	1.1576	1.0550
1.750	.7215+89	• 9390	1.7970	6932	.1723	4947	3547	7669	•880 <i>2</i>	9173	.7970	1.1712	1.0633
1.800	•7201+99	.9389	1.7965	.6830	.1004	.4A93	.3400	.7450	.8768	•9218	.7915	1.1854	1.0533
1.85D	.718E+09	.9387	1.7960	.E731	.1+24	•4667	₹259	.7233	8736	9269	•7862	1.2002	
1:900	.716E+09	.9386	1.7994	.6637	1392	.4536	₹1?4	7918	8784	.9327	• 7907 • 7811		1.0814
1.950	•713E+89	.9385	1.7948	.6537	1207	4408	2995	.6805	•8673	•9377 •9388	•7761	1.2158	1.0914
2.000	•711:+89	9384	1.7942	•6+43	1278	.4285	-287?	•6595	.8644	•9455		1.2318	1.1019
			- •		712.0	*~~~	• · · · ·	•0799	9 (. C. ++	• 3422	.7713	1.2484	1.1129

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C. (CONTINUED)

MACH	LOCAL ISENTROPIC	VISCOSITY	THERMAL CONDUCTIVITY	PRANDTL
	EXPANSION COEFF.	G/CM+SEC	CAL/CM-SEC-K	NUMBER
0.000	I	.29990E-04	•11853E-03	.7077
.050	1.6896	.29908E-04	•11619E=03	.7077
.100	1.7151	.29847E-04	.11790E-03	.7077
.150	1.6881	.29746E-04	.11741E-03	.7076
.200	1.7086	.29606E-04	.116) -E-03	.7076
.250	1.7055	.29427E-04	•11589E-03	.7077
300	1.6982	.29219E-04	.11486E-03	•7078
.350	1.7046	-28959E-04	•11365E-03	7080
• • 00	1.7017	.28673E-84	•11229E-03	.7083
.457	1.7067	.28357E-04	•11077E-03	.7088
.500	1.7035	.2801PE-04	.10641E-03	.7276
.550	1.7049	.276376-84	.10476E-03	.7279
.600	1.7016	.27239E-04	.10300E-03	.7283
•65N	1.7105	.26819E-04	.10117F+03	.7287
•700	1.7066	.26380E-04	.99292E-04	.7291
.750	1.7053	.25923E-04	.97345E-04	.7296
.800	1.7970	•25453E-04	.95369E-04	.7392
• 95 n	1.7027	•?4971E+B4	933625-94	.7307
• 900	1.7053	.24479E-B4	.91311E+04	.7315
. 950	1.7049	.23980E-04	•89121E-04	.7334
1.000	1.7026	.23477E-04	.86929E-04	.7354
1.050	1.7083	•22969E+04	.84226E-04	.7420
1.199	1.6988	.2246NE-N4	.82143E-04	.7434
1.150	1.6994	.21951E-0 ₊	.80068E-D4	.7449
1.200	1.6992	•21444E-D4	.78013E+04	•7463
1.259	1.6938	.28939E-84	.75983E-04	.7479
1.300	1.6962	.20437E-04	.73977E-04	.7495
1.350	1.6924	.1994NE-N4	.72841E-04	.7506
1.400	1.6929	•19449£-04	•70122E-04	.7519
1.450	1.6869	•18963E-04	.68246E+04	.7531
1.500	1.6905	.18484E-D+	.66428E-04	.7541
1.550	1.6871	.18013E-04	.64649E-94	.7550
1.600	1.6841	.17548E-84	.62904E-04	.7557
1.650	1.6846	•17092E-04	•61213E+04	.7560
1.700	1.6847	.166445-84	.59547E-04	.7566
1.759	1.6834	•16205E-04	.57692E-04	.7575
1.800	1.6601	•15774E-N4	.56257E-04	.7586
1.850	1.6809	·15354E-04	•54649E=114	•7598
1.900	1.6811	+14943E-04	.53070E-04	.7613
1.950	1.6782	•14541E-04	.51573E-04	.7622
ა • შსშ	1.6776	.14149E-#4	.50150E-94	.7626

NITTANG EOOG BO

OF POOR OUALITY

TAPLE V. REAL-GAS ISENTROPIC EXPANSIONS OF PARAHYCPOGEN

TT = 40.0 K PT = 10.0 ATM PHOT = .3115-02 G/CM3 SVT = 717.913 M/SEC

			= ru.u.	(F'I =	ти. о дем	PH01 =	· 5116-02	SZCM3	SVT = 717	.913 M/S	E C		
MACH	PEVM	7	CENCA	SVZSVT	P/FT	T/TT	#H0/9H0 T	A+/A	TV2VVZ	P/PT FELATIVE	T/TT TO IDEAL	RHOZRHOT	A*/A S
0.000	0.	.9465	1.0017	1.0000	1.0000	1.0000	1.0000	0.0000	1.0000	1.0000	1.0000	1.0000	1.0000
•050	•3 <u>955</u> +9 <i>P</i>	ოც გნ	1.6871	•9997	. 99/1	.999*	.9988	.0872	1.0000	.9998	•9998	1.0000	1.0103
•1 n D	•677: + ₽8	. 98£4	1.6941	.9989	• 9922	.9977	. 7951	.1735	.9999	9992	• 9992	1.0001	1.0103
.150	• 9 116-7414	• पष्ट्र	1.6056	9975	.9824	•993*	.9849	.2583	.9997	. 9980	9942	1.0001	1.0101
.200	·1209+09	.3851	1.637R	. 9355	* déal	.9888	•9803	.3407	.9995	. 9964	9967	1.0000	1.0098
• 25 0	•1+9F+89	.9859	1.6105	.9938	.9520	•9826	•9e 95	.4292	9991	9943	9949	1.0000	1.0095
<u>.</u> 399	•177E+49	.9856	1.6139	.9899	.9317	.975₽	.9564	.4959	.9987	.9917	. 9926	1.0000	1.0091
•354	*5u 4_+U σ	.9853	1.6177	• 9462	• 9¶ 84	9662	-9414	•5673	.9982	9887	-9898	1.0001	1.0086
•400	.229£+09	.9950	1.6222	.9829	.882F	- 95 6 1	9244	• 6 3 4 0	9976	9853	9867	1.0002	1.0081
.450	.2545+09	.9846	1.6271	9773	•85 41	.9448	•9058	-6955	9969	9815	.9830	1.0003	1.0075
•500	•277E+B9	. 9842	1.6324	3770	. A 2 CQ	.9322	-8857	.7515	9960	.9773	.9790	1.0006	1.0069
.550	· .2995+09	.9834	1.£₹₽1	. 3662	.7918	.9199	.BE42	.8017	9950	9726	.9744	1.0008	1.0061
.600	.3195+09	. 99 33	1.6+42	.9E98	.7586	.9044	.9416	.8462	9938	9677	9695	1.0013	1.0054
. 650	•338E+D9	.9929	1.6505	. 9929	.7245	.8898	.8180	8846	.9924	9623	.9641	1.0019	1.0046
.700	.35 EE+09	9824	1.6569	.9455	.6897	.8728	.7936	.9171	9918	.9567	9583	1.0026	1.0036
.750	•3725+09	.9819	1.6634	. 9376	.6548	.8558	.7687	.9438	.9890	9509	9521	1.0035	1.0027
"ធ្វ	•3877+09	9914	1.6699	.9293	.6200	.8383	.7435	.96₹1	9869	.9451	9455	1.0048	1.0019
-850	•40 DF + C 9	•9908	1.6762	.9204	•585€	.8202	•7182	.9809	.9847	9393	9387	1.0064	1.0012
.900	.4115+89	.9903	1.6823	• 9111	•5519	.8017	.6927	.9917	.9822	.9333	9316	1.0082	1.0005
.950	.4225+09	9798	1.6881	•9015	.5190	7829	•6675	.9980	.9794	.9278	.9243	1.0106	1.0001
1.707	4415+89	, 9793	1.6935	.8914	. 4A73	.7640	-5425	1.0000	.9765	9224	9168	1.0136	1.0000
1.050	•439E+03	. 9744	1.6985	+8511	5£#	.7.49	6180	.9981	9734	917	.9092	1.0170	1.0001
1.100	.4467+89	GY44	1.7030	.8784	.4276	.7259	-5939	9928	9700	9129	.9015	1.0210	1.0007
1.150	•452£+89	.0779	1.7070	8595	3997	7069	.57N4	9844	9666	90 6a	.8939	1.0257	1.0016
1.200	•456E+09	.9775	1.7105	.8485	3774	.6881	-5476	9735	.9630	.9054	.8863	1.0757	1.0031
1.258	·460E+09	. 9770	1.7135	.8373	.3485	6695	•5255	.9603	.9593	90 25	•8787	1.0372	1.0052
1.300	.463E+09	.9766	1.7161	826D	.3249	6512	-5040	.9450	9555	•9003	.8713	1.0438	1.0076
1.350	•466E+B9	.9763	1.7181	.8147	.3029	.6332	.4833	9281	9517	.8988	• 85 + B	1.0512	1.0107
1.400	.467E+89	•9759	1.7198	.803₹	2877	.6156	+61+	.9099	9.478	.8980	.8569	1.0593	1.0144
1.459	.4E8E+119	9756	1.7211	7920	.2628	•598₹	4441	8904	9448	.8976	8499	1.0680	1.0185
1.500	• 68E+89	+9752	1.7221	.7P07	.2446	-5815	•4256	.8701	9481	8981	.8432	1.0774	1.0234
1.550	•4685+89	.9749	1.7229	.7695	.2?77	.5651	.4079	8493	9363	.8993	•8366	1.077	
1.600	.4685+89	9747	1.7234	.7584	2120	-5+91	1998	,8279	.9326	•6553			1.0290
1.650	.467E+89	.9744	1.7237	.7475	1973	-5335	• 3744	.0062	9289	.9033	• 8302 4348	1.0985	1.0351
1.700	•465E+99	.9742	1.7238	.736b	1836	.5183	·3587	.7843	9253	• 9063	. 62 4 0	1.1100	1.0417
1.750	.464E+09	9730	1.7238	.7259	1709	.5036	3437	.7624	.9218		8180	1.1221	1.0490
1.800	462E+09	9737	1.7238	.715÷	1591	.4894	•3294	.7405	.9184	•9100	·8121	1.1350	1.0571
1.850	.46nF+09	.9736	1.7236	7751	1461	.4755	• ₹156			+9142	.8065	1.1484	1.0656
1.900	4575+99	9734	7234	6949	.1379	4621	• 3025	•7188 •073	.9151	9189	.8010	1.1624	1.0747
1.950	4555+09	9732	1.7232	•6848	.1285	• 4491		6972	.9118	• 9242	. 7957	1.1770	1.0843
2.000	.452F+89	0731	1.7229	•6750	.1196		•2899 2770	•6760 65.0	.9087	.9300	• 7906	1.1923	1.0946
	*->5 *** 3	• + I	10 663	• 6/90	• 1146	.436°	•2779	.6549	• 905 E	.9361	.7857	1.2079	1.1052

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D. (CONTINUED)

м∆Сн	LOCAL ISENTROPIC	VISCOSITY	THERMAL CONDUCTIVITY	PRANCTL
r FOR	EXPANSION COFF.	G/CM+SEC	CAL/CM-SEC+K	NUMBER
	TANAMATON COLFF.	0761-350	GALVON-SEC-K	NONCEF
។	I	.36723E-04	.15188E-93	.7085
.050	1.5974	.36633E-04	•15126E-03	.7085
.100	1.5910	.35573E-04	.15065E-03	.7085
.150	1.5833	.364742-84	.15016E-03	.7086
.200	1.5850	.36336E-84	.149215-03	.7087
.250	1.5878	.36159E-8+	.14799E-03	.7088
.300	1.5887	.35944E-04	.14651E-03	.7090
.350	1.5949	.35692E-04	.14504E-03	.7081
• 40 0	1.5976	.35403E-04	.14348E-83	.7066
•450	1.6022	.35079E+0+	.14174E-03	.7849
.500	1.6089	.34721E-04	.13982E-03	.7033
.555	1.6995	.34331E-04	.1.3772E-03	.7016
•600	1.6179	.33917E-04	.13547E-93	.7000
•650	1.6211	.33459E-0→	.13307E+93	.6986
.700	1.6248	.32982E-84	.13054E-03	-6974
.750	1.6303	.32481E-04	.12788E-03	-6964
.800	1:6381	•31957E-04	•12513E-03	-6957
• 650	1.6428	.31414E-04	.12245E-03	6945
• 900	1.6453	.30855E-04	.11975E-03	.6933
• 950	1.6528	•30282E -0 4	•11699E-03	.6925
1.000	1.6578	.2969 RE -04	•11418E-03	•6922
1.050	1.6681	.29105E-04	•11134E-93	•6923
1.100	1.5657	•28508E+04	.10849E-03	•6929
1.150	1.6677	.27907E-8+	•10563E+03	•6 93 9
1.200	1.6720	.27305E-0+	.10156E-03	.7036
1.250	1.6752	+26705E-04	.98953E-D4	.7042
1.300	1.6737	•26107E-04	.96389E-114	.7849
1.350	1.6777	.25514E-04	.93878E-04	.7057
1 + 400	1.678 <u>1</u>	• 24926E-04	•91425E-04	.7066
1.450	1.6761	.24345E-04	• 890 25E-N4	.7075
1.500	1.6788	•?₹7 7 2E=04	#86672E=114	.7090
1.550	1.6805	.23207E-04	.84260E-94	.7108
1.600	1.6788	•22651E-04	.81585E-04	.7158
1.650	1.6782	•22104E-04	.79390E-04	.7173
1.790	1.6785	•21567E-84	.77254E-D4	.7187
1.750	1.6802	•21040E-04	.75176E-04	.7201
1.800	1.6785	.20523E+04	.73157E-04	.7215
1.850	1.6776	•20016E-04	•71200E=04	.7227
1.900	1.6767	.195205-04	•693 <u>06E=04</u>	.7238
1.950	1.6770	· 19034E-0-	.67479E-#4	.7247
ა • ცს <i>ო</i>	1.6739	.18559E-04	.65707E-04	•7255

ORIGINAL PAGE IS OF POOR QUALITY

TABLE V. REAL-GAS ISENTPOPIC EXPANSIONS OF PARAHYDROGEN

TT = 100.0 K PT = 10.0 ATM PHOT = .246E-02 SZCM3 SVT = 778.515 MZSEC

		·-•	- 13041	`	1010 MI	4-131 -	E SEPTEMBER A	37 C 13	201 - 175	ינותי כותי	a.C		
MACH	PEZM	7	CENCA	SV/SVT	P.V₽Ţ	7/17	440 / 940*	Δ+/Δ	SV/SVT	P/PT	T/TT	RHO/PHOT	A*/A
										PELATIVE	TO TOEAL	GAS VALUES	5
0.000	9.	. 3979	1.4728	1.9900	1.0000	1.8880	1.6000	0.0000	1.0500	1.0000	1.0000	1.0000	1.0000
.050	•224 <u>5</u> +π8	.9979	1.4748	୍ ପ୍ରମନ	9982	9094	9988	.0860	1.0000	1.0000	,9999	1.0001	.9970
1115	*4465+99	9079	1.4755	9991	9928	9977	9951	.1713	1.0001	9997	9997	1.7001	.9971
.150	•665F+09	.9977	1.4767	9380	9876	9949	9888	.2550	1.0002	9992	9993	1.0900	9971
.200	•991E+08	9975	1.4783	9964	.9711	. 9959	9803	.3365	1.0004	.9986	9988	1.0001	9974
.250	.1095+09	.9974	1.4805	99+4	9553	.9859	9695	4152	1.0006	.9977	9981	1.0001	.9976
. 30C	•12¤=•0¤	.9972	1.4832	.9921	.9362	9796	.9563	4902	1.0008	9965	9972	9999	.997E
.35 D	·149:+89	,0070	1.4863	.9891	. 91-3	9723	9+11	.5613	1.0011	•9951	9951	9998	9979
.400	•1+85+D9	• 9964	1.4900	.9558	. A895	9640	9242	.6278	1.0015	.993€	9948	9999	9982
•450	.1855+B9	.9355	1.4943	9221	.5631	9546	.9054	.6893	1.0016	9918	. 9933	9999	.9986
•E00	*2025*N9	•9962	1.4901	•9780	.83-2	9442	• 9 8 5 17	.7455	1.0022	.9896	. 9914	9998	.9989
•550	.218=+R9	.9050	1.5044	.9735	.03€	9329	.9631	.7961	1.0026	.9870	9893	9996	9991
.600	•233E+B9	,9956	1.5103	.9687	•7715	.9206	.9400	.8411	1.0029	.9841	. 9869	9995	9994
-659	·246f+09	.9952	1.516	9634	.73°3	9971	.8159	.8881	1.0033	9807	.9841	9993	9995
.700	.258°+09	• 0049	1.5239	.957ª	.7046	8937	.7911	.91 37	1.0036	.9773	9819	.9993	.9999
•750	. 26.95 + 8.9	.9945	1.5315	.9F18	.6700	8785	.7653	.9411	1.0839	9730	9773	9990	9998
.800	•2905+09	.9941	1.5396	9454	.6354	.8529	.7392	.9631	1.0041	- 9686	9733	.9989	.9999
•85 O	.298E+09	.9938	1.5482	.9387	.6010	8465	.7128	9798	1.0042	.9638	. 9689	9989	1.0001
• 500	*2965*B9	.9334	1.5573	•931 5	.5658	.8296	-6863	.9913	1.0042	•9586	9640	9989	1.0001
.9F (i	∙ ኛባ [‡] ፫ ቀበ፡፡	.9030	1.5669	• 9741	. F ₹₹₽	.8121	.65 QA	9979	1.0941	.9531	9586	.9991	1.0001
1.000	. ₹ŋ 9 5+99	9926	1.5765	.9163	. = ng4	.7941	.6335	1.0700	1.0038	.9472	. 9529	9993	1.0000
1.050	•314#+DA	,0027	1.5965	. 9041	• • 66.7	.7756	-6077	.9981	1 = 0 0 3 2	.9413	.9467	1.0000	1.0002
1.100	• 31 8E + 9 G	.0319	1.5965	. 8 <i>93</i> 6	• = 38 ti	•756°	•5822	.9924	1.0025	.9352	. 9401	1.0008	1.0002
1.158	•3211+09	.9915	1.6064	.8907	.4846	.73AA	.5572	.983?	1.0016	, 929n	9332	1.0019	1.0004
1.200	.3241+09	.9912	1.6162	.8814	.3807	.7180	.5371	.9714	1.0003	.9232	.9260	1.0037	1.0009
1.250	.3265+09	• 9 9 g a	1.6256	.8719	.35-2	.5990	•5097	•9570	9989	9176	9186	1.0060	1.0016
1.300	•327÷+09	.9985	1.6345	.8520	.3292	.680°	. +872	.9405	.9971	.9123	.9110	1.0088	1.0028
1.350	.328E+09	.9902	1.6429	.8519	•39∓8	•6620	.4655	9222	9951	9075	. 90 34	1.0124	1.0744
1.400	.728E+09	• 9899	1.6506	•8 -16	.2838	.6+3E	4447	9025	,9329	. 90 33	.8957	1.0166	1.0762
1.459	.328E+09	• q a g 6	1.6575	.8310	.2634	+6252	.4249	.6820	.9905	8999	.8881	1.0218	1.0090
1.500	•3275 + 99	. 9893	1.6634	. 8204	. 2444	.6073	.4059	.8605	9878	.8972	.8806	1.0277	1.0121
1.550	.3262+0P	.9891	1.6693	. 8396	.22£7	.5899	.3976	.8384	.9851	. 8952	. 8732	1.0344	1.0156
1.600	+ 325°+119	.9888	1.6741	.7987	.2104	•572P	• 777 7	•816°	.9821	. 8944	.8660	1.0422	1.0204
1.659	* 45 45 + B o	• 9R R E	1.6782	.7878	1953	•5562	. 4544	.7937	.9791	. 8942	.8590	1.0507	1.0256
1.700	•322±+09	. 9384	1.6817	.7770	.1813	•5 • 0 1	.3389	.7711	9760	8948	.8522	1.0600	1.0314
1.750	•320F+09	.9482	1.6845	.7652	·1683	.5245	.3241	.7486	9729	.8962	.8457	1.0702	1.0380
1.800	• 31 8F + 0 9	.9380	1.6869	.7554	.1564	.5094	*3101	.7264	•96 9 8	. 8985	. 6394	1.0811	1.0452
1.850	• 31 65 + N B	* ciá 4 b	1.6888	.744A	.14E3	.4947	.2967	.7843	.9666	•901F	.8334	1.0928	1.0531
1.900	• 31 35 + 9 9	•9876	1.6903	.7342	·1351	.4806	.2841	.6827	.9635	.9054	.8275	1.1054	1.0618
1.950	.3115+09	. 9475	1.6915	.7239	.1257	• 4669	.2720	.6614	•9604	. 90 98	.8219	1.1186	1.0710
2.000	•308T+09	. 9473	1.6924	.7136	•11÷9	• 4536	.2505	•6405	.9574	•9149	.8165	1.1325	1.0809
												•	

MACH	LOCAL ISENTROPIC	VISCOSITY	THERMAL CONDUCTIVITY	PRANDTL
	EXPANSION COEFF.	G/CM-SEC	CAL/CM-SEC+K	NUMBER
0.000	ī	.42882E-04	•19757E-03	.7126
.050	1.5067	.42784E-04	.19652E-03	.7130
.100	1.4764	.42730E-04	•19610E=03	.7128
.150	1.4666	.42638E-84	.19538E-03	.7126
. 200	1.4778	.42511E-04	·19439E-03	.7123
.250	1.4787	.42348E-04	•19311E-03	.7118
.300	1.4730	.42150E-04	•19157E-03	.7113
•350	1.481?	.41916E-04	.18975E-03	.7107
.408	1.4867	.41648E-04	.18767E-03	.7100
• 450	1.4901	.41345E-04	.18533E+03	.7092
•500	1.4917	.41009E-04	.16275E-03	.7084
•550	1.4958	.40641E-04	.17992E-03	.7976
•640	1.5020	.40240E-04	.17686E-03	.7068
. 650	1.5059	.39808E-04	.17358E-03	.7060
.700	1.5170	.39346E-84	.17009E-03	.7053
.750	1.5170	.38854E-04	•1665 <i>2</i> E-03	.7043
.800	1.5283	.38335E-84	•16283E-03	.7831
.850	1.5365	.37789E-84	•15896E-83	.7921
• 900	1.5436	.37217E-04	•15495E-03	.7014
• 950	1.5519	.36622E-04	-15081E-03	.7011
1.000	1.5603	.36006E-04	•14656E-113	.7011
1.050	1.5717	.75371E-04	.14231E-03	.7012
1.100	1.5787	.34720E-04	.13877E-D3	.6979
1.150	1.5872	•34055E-04	.13518E+03	•6950
1.200	1.5988	.33380E+84	•13155E+03	.6927
1.250	1.6078	•32697E-04	.12792E-03	.6909
1.300	1.6143	.32010E-04	.12430E-03	•6 89 6
1.350	1.6235	.31322E-04	•12075E-03	.6887
1.400	1.6287	.30635E-04	.11739E-03	.6876
1.450	1.6395	•29953E+04	•11407E-03	.6870
1.500	1.6425	•29276E-04	.11089E-03	.6871
1.550	1.6471	.28607E-04	.10760E-03	#6876
1.600	1.6562	•27948E-04	•10447E-03	.6887
1.650	1.6574	.27300E-04	•10141E-03	•6902
1.700	1.6597	•26663E-94	•97967E+84	•6954
1.750	1.6633	• 260 39E-04	.95294E-114	•6962
1.800	1.6652	.25427E-84	•92714E-04	•6971
1.850	1.6665	.24828E-04	•90217E+04	.6981
1.900	1.6701	• 24242E-04	.87884E+84	•6992
1.957	1,6693	.23669E-04	.85447E-04	.7006
2.000	1.6697	.23109E-04	.83136E-04	.7022

ORIGINAL FAGE IS

OF POOR QUALITY

Manager Company

TABLE V. REAL+GAS ISENTROPIC EXPANSIONS OF PARAHYDROGEN

TT = 200.0 K PT = 10.0 ATM RHOT = .122E-02 G/CH3 SVT =1062.277 M/SEC MACH 7 PE/M CP/CV SV/SVT PIFT T/TT RHO/RHOT A*/A SV/SVT P/PT T/TT RHO/RHOT A* / A -----RELATIVE TO IDEAL GAS VALUES--0.000 1.0067 1.3501 0. 1.0000 1.0000 1.9000 1.0000 0.0000 1.0000 1.0000 1.0000 1.0000 1.0000 .050 1.7067 .9455+07 1.3498 . 9990 . 9982 .9996 .9907 .0860 1.0000 1.0000 1.0001 .9999 .9973 .100 1.3497 .188E+08 1.0066 .9990 .9932 .9983 9950 1.0000 1.0003 .1713 1.0001 .9999 .9973 ·150 ·281E+08 1.0066 1.3495 . 9978 .98+8 .9961 .9887 .2550 1.0000 1.8004 1.9006 .9999 .9973 .200 .371E+08 1.0965 1.3492 .9961 .9733 .9931 .9802 .3365 1.0001 1.0008 1.0010 1.0000 .9974 .250 .459E+08 1.0064 1.3488 . 9939 .9586 · 98 92 .9693 .4151 1.0001 1.0016 1.0012 .9999 .9974 .300 .5445+88 1.0063 1,3484 .9913 .9412 .9846 .9564 .4902 1.0002 1.0023 1.0019 .9976 1.0000 .625E+08 •350 1.0061 1.3479 . 9887 . 9211 .9791 .9413 .5611 1.0003 .9976 1.0025 1.0031 1.0000 -40 D .702F+08 1.0060 1.3474 .9848 .8985 .9729 .9241 .9976 .6274 1.0004 1.0032 1.0041 .9998 .450 .775=+08 1.0058 1.3468 .9809 .8739 .9660 .9054 .6888 1.0006 .9978 1.0041 1.0051 .9999 .500 .842E+08 1.0956 1.3462 .9767 .8473 .9584 .8850 .7448 1.0008 1.0051 1.0064 .9998 .9979 .550 .905E+08 1.0054 1.3456 .9720 .8192 .9502 .7953 1.0077 .8632 1.0010 1.0062 .9997 .9981 .600 .962F+08 1.0052 1.3449 .9671 .7899 .9414 .8483 .8493 1.0013 1.0075 1.0092 .9998 .9984 .650 .101E+09 1.0050 1.3442 .7594 .9618 .9320 .8794 .8162 1.0016 1.0058 1.0106 .9997 .9986 ▶700 *106E+09 1.0048 1.3436 .9562 .7282 .9221 .7912 .9127 1.0020 1.0101 1.0125 .9995 .9988 .750 .110E+09 1.0946 1.3429 .9504 .6966 .9117 .7656 .9405 1.0024 1.0116 1.0143 . 9994 .9992 .800 ·114E+89 1.0043 1.3423 . 9443 .9009 .6645 .7393 .9626 1.0029 1.0130 1.0162 . 9991 . 9994 .850 ·1175+89 1.0041 1.7418 .9360 .8897 .6325 .9794 .7128 1.0035 1.0144 1.0183 .9988 .9996 .900 ·1195+89 1.0039 1.3413 .9715 .6007 .8781 .6868 .9911 1.8941 1.0159 1.0204 .9999 .9984 .950 .1215+09 1.0736 1.3409 .9248 .5691 1.0000 .6662 .6591 .9979 1.0046 1.0173 1.0226 .9979 1.000 .122E+09 1.0034 1.3406 .9179 .5381 .8540 -5321 1.0000 1.0056 1.0186 1.0248 .9971 1.0000 ·123E+09 1.050 1.0032 1.3484 .9110 .5076 .8416 .6053 .9978 1.0054 1.0196 1.0271 .9961 .9998 1.100 .124F+09 1.007 1.3484 .9033 .4780 .8289 .5789 .9919 1.0073 1.0207 1.0295 . 9951 .9997 •174E+99 1.150 1.09% 1.3405 .8907 . 449? .8169 .5527 .9822 1.0083 .9993 1.0214 1.0318 .9938 1.209 .1245+09 1.0025 1.3409 .8894 .4215 .8030 .5271 • 96 96 1.0094 1.0222 1.0342 . 9924 .9991 1.250 .1235+09 1.0023 1.3414 .8820 .3948 .7897 •5020 .9539 1.0105 1.0225 1.0365 .9906 . 9985 ·1225+09 1.300 1.0021 1.3421 .8746 .3690 .7764 .4775 . 9356 1.0117 1.9225 1.0388 .9888 .9977 1.350 ·1215+09 1.0020 1.3431 .8671 .3445 .7620 . 4537 .9153 1.0129 1.0410 1.0223 .9867 .9968 1.400 .120E+09 1.0018 1.3444 .8597 .3211 .7494 .4396 .6931 1.0143 1.0218 1.0431 .9958 . 9844 •118E+09 1.450 1.0016 1.3460 .8521 .2986 .7357 .4882 .8692 1.0156 1.0207 1.0451 .9943 .9816 1.500 *116F + 09 1.0014 1.3479 . 8446 .2776 .7220 .8439 1.0178 .3865 1.0191 1.0469 .9926 .9785 1.550 .114E+09 1.0013 1.3501 .8371 .2576 .7082 .3657 .8177 1.0185 1.0170 1.0485 .9752 .9907 1.600 .112E+09 1.0911 1.3528 .8296 .2327 .6944 . 3457 .7907 1.0200 1.0145 1.0499 .9717 .9865 1.650 *109E+09 1.0010 1,3559 .8220 .2208 .6805 .3264 .7629 1.0216 1.0111 1.0510 .9675 .9858 1.700 .107E+09 1.0009 1.3504 .8145 .2041 .6665 .30 PO .7351 1.0232 1.0075 1.0518 .9635 .9832 1.750 .1045+09 1.0007 1.3634 .8978 .1884 .6526 .2905 .7871 1.0248 1.0033 1.0523 . 95 92 .9804 1.800 ·1025+09 1.9986 1.7689 .7996 .1738 .6386 .2777 •6790 1.0264 . 9984 1.0524 .9544 .9771 1.850 .992E+98 1.0005 1.3730 .7921 ·1600 .624€ .2577 .6509 1.0281 .9925 1.0521 .9492 .9733 1.900 .965E+08 1.0004 1.3787 .7847 1.0297 .9695 .1472 ·6105 1.0513 .2425 .6234 .9863 .9440 1.950 **■938€+08** 1.0103 1.3849 .7773 .1353 .5965 .2282 .5961 1.0314 .96>3 9793 1.0501 .9385 2.000 .911F+08 1.0002 1.3919 .7699 .1242 .5824 .2146 ₩695 1.0330 .9716 1.0484 . 9328 .9610

F. COONTINUEDE

MACH	LCCAL ISENTROPIC	VISCOSITY	THERMAL CONDUCTIVITY	PEANCTL
	EXPANSION COEFF.	G/CM-SEC	CAL/CM-SEC-K	NUMBER
0.000	ī	.68606E-04	.37602E+03	.7034
.050	1.3451	.68467E-04	.37545E-03	.7035
.100	1.3579	.68405E-84	•37519E-03	.7035
.150	1.3571	.68302E-04	.37477E-03	.7035
.200	1.3602	68159E-04	.37418E-03	.7034
.250	1.3568	.67976E-04	.37343E-03	.7034
.300	1.3598	.677552+84	.37253E-03	.7034
• 350	1.3567	.67496E-04	.37147E-03	.7034
• 400	1.3531	.67201E-04	.37027E-03	.7033
• 450	1.3562	.66571E+04	.36892E-03	.7032
.500	1.3538	.66508E-04	.36745E-03	.7029
•550	1.3533	.66113E-04	.36585E+N3	.7027
.600	1.3550	.65688E-04	.36380E-03	.7030
•650	1.3518	.65235E-04	•36096E-03	.7045
.700	1.3505	.64755E-04	•35797E+03	.7060
.750	1.3511	•64251E-04	.35483E-13	.7075
.800	1.3483	.63723E-04	.35156E-03	.7090
.850	1.3485	.63173E-04	.34817E-03	•7105
• 900	1.3480	.62603E-04	.34466E-03	.7118
.950	1.3463	.62015E-04	.34106E-03	.7130
1.000	1.3449	.61417E-04	.33737E-03	.7141
1.050	1.3440	.60788E-04	.33360E-03	.7149
1.100	1.3453	.60151E-04	•32975E-03	•7155
1.150	1.3431	.59502E-04	.32565E+03	.7159
1.200	1.3449	.58847E-04	.32190E-03	•7159
1.259	1.3448	•58165E-04	·31789E-03	•7156
1.309	1.3440	.57480E-04	•31365E-03	•7149
1.350	1.3454	.56786E-84	.30977E-03	.7139
1.400	1.3469	•56082E-04	.30567E=03	.7123
1 • 450	1.3472	•55369E-04	.30154E-03	.7103
1.500	1.3480	.54647E-0+	.29735E-03	.7079
1.550	1.3509	•53917E-04	.29075E-03	.7107
1.600	1.3533	•53179E-04	-28413E-03	.7131
1.650	1.3543	.52432E-04	.27748E-03	.7151
1.700	1.3601	•5167PE-04	.27082E-03	.7168
1.750	1.3634	.50917E-0+	-26415E-03	.7180
1.800	1.3668	.50148E-04	•25747E-03	.7188
1.851	1.3701	.49371E-04	.25077E-03	.7192
1.900 1.950	1.3772 1.3822	.48587E-04	.24408E-03	.7192
2.000	1.3522	.47794E-04	.23737E-03 .23067E-03	.7187
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MACH	LOCAL ISENTROPIC	VISCOSITY	THERMAL CONDUCTIVITY	FRANDTL
	EXPANSION COEFF.	G/CM-SEC	CAL/CM+SEC-K	NUMBER
0.000	Ĭ	.89743E=84	.46223E-03	.7104
.050	1.3899	.898D₹E-04	.46215E-03	•690 8
.100	1.3870	,89715E-04	.46176E-03	•6908
. 150	1.3938	. P956PE-04	.461125-03	•6909
.200	1.3916	.89363E-84	.46022E-03	.6918
.250	1.3983	.99102E+04	.45908E-N3	.6911
* 300	1.7917	.88787E-04	.45769E-03	"6912
.350	1.3944	.88+17E-84	.45688E-03	.6913
.400	1.3914	.87997E+04	.45424E-03	.6915
. 450	1.3909	.875275-84	.45220E=33	.6917
•500	1.3919	.87011E-04	.44996E-83	.6920
•5គ្នា	1.7874	•86451E-04	.44754E+83	.6922
• 684	1.3884	.85850E=04	-44494E-83	.6925
•650	1.3872	.85210E-04	.44229E-03	•6927
.700	1.3846	.845352-04	.43957E-03	•6928
•750	1.3841	.83826E-04	.43672E-03	.6931
.800	1.3836	.83089E-04	.43376E-03	•6932
.850	1.3813	.82324E-04	.43070E-03	-6934
.900	1.3818	.91536E-0+	.42757E-03	.6937
.950	1.3791	.807265-04	.42436E-03	.6940
1.000	1.3769	.79899E=04	.42109E-03	.6943
1.050	1.3757	.7905FE-04	.41777E+03	•6947
1.100	1.3704	.78198E-04	+61441E=03	. 6950
1.150	1.3702	.77331E-N4	•41193E+93	•6955
ייוב• ו	1.369	.764545-84	.4076+E+03	•695 8
1.250	1.3665	.755715-84	.40415E=03	•6964
1.300	1.365+	.74683E-04	.40036E+03	.6974
1.350	1.3018	.73791E-84	.396575-03	.6984
1 . 480	1.3599	.72898E-04	.39280E-03	.6993
1.450	1.3572	.72004E-84	.3890+E-03	.7002
1.500	1.3555	·*1110E-04	.33531E-G3	.7809
1.550	1.3536	.702195+04	.38161E-03	.7015
1.600	1.3511	.69320E=#4	.37793E+03	.7020
1.650	1.3503	.684445-04	.374305-93	.7023
1.790	1.3487	67562=-84	.37071F+03	.7024
1.750	1 • 3 • 55	.66683E-04	.36715E-03	.7022
1.877	1.3446	.658105-04	.363635-03	.7018
1.951	1.3433	.64941E-84	*35865E=#3	.7839
1 900	1.3427	640765+0→	.35327F-03	.7067
1.950	1.3411	.63217E-04	.347955-03	.7092
7.000	1.3.05	.62363£-04	.342695+03	.7113
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TABLE V. REAL-GAS ISENTROPIC EXPANSIONS OF PARAHYDROGEN

		',45.° T	F = 300.0	K PT =	10.0 ATM	RHOT =	.814E-03	G/CM3	SVT =1317	.507 H/S	EC		
MACH	RE/M	7.	CPZCV	SV/SVT	P/PT	T/TT	RHOZRHOT	A+/A	SV/SVT	P/PT	1/11	RHO/RHOT	A7/A
î .												GAS VALUES	
0.000	Ů.	1.0059	1.3709	1.0000	1.0000	1.0000	1.0000	0.0000	1.0000	1.0000	1.0000	1.0000	1.9900
050	.596E+07	1.0059	1.3865	. 9997	• 9982	•9995	•9987	.0864	1.0000	1.0000	1.0000	1.0000	1.0019
.100	•119E+08	1.0059	1.3864	.9989	9938	9981	9949	.1721	.9999	.9999	1.0001	.9999	1.0018
•150	·177E+08	1.0058	1.3862	.9976	. 9844	.9957	.9887	.2562	9999	1.0000	1.0001	•9999	1.0017
•200	.234E+08	1.0058	1.3859	.9958	.9725	9923	.9801	.3380	9998	1.0000	1.0003	.9999	1.0016
.250	.290E+08	1.0057	1.3556	• 9935	.9576	.9881	.9694	.4169	9997	1.0002	1.0084	1.0000	1.0016
.300	.343E+08	1.0056	1.3852	•9907	.9307	9829	.9563	.4921	.9995	1.0002	1.0806	9999	1.0014
.350	•395E+08	1.0055	1.3847	•9873	•9192	.9769	.9413	•5632	.9994	1.0004	1.0008	1.0000	1.0013
.400	.443E+08	1.0054	1.3842	•9836	.8961	.9701	•9243	• 6296	.9992	1.0006	1.0011	1.0000	1.0011
.450	.489E+08	1.0053	1.3836	. 9794	.8709	.9624	.9055	.6909	.9990	1.0008	1.0014	1.0000	1.0009
•500	.572E+08	1.0051	1.3829	. 9747	.8440	• 9541	.8853	.7470	•9988	1.0011	1.0018	1.0002	1.0009
•550	.571E+08	1.0050	1.3421	. 9697	.8153	•9450	.8635	.7973	9986	1.0014	1.0022	1.0001	1.0006
•600	.608E+08	1.0048	1.3812	.9642	.7854	•9354	.8406	.8420	•9983	1.6918	1.0027	1.0002	1.0004
•650	•64DE+08	1.0946	1.3802	.9584	.7545	.9251	.8167	.8898	.9981	1.0023	1.0033	1.0002	1.0003
.700	.670E+08	1.0045	1.3792	• 9523	.7229	.9143	.7918	•9138	.9979	1.0027	1.0039	1.0002	1.0001
•750	•695E+08	1.0043	1.3780	,9459	•6909	.9031	.7663	-9412	.9977	1.0034	1.0047	1.0003	.9999
.800	.716E+08	1.0041	1.3768	• 9391	.E588	.8914	-7404	.9630	.3974	1.0042	1.0055	1.0005	.9999
.850	•737E+08	1.0039	1.3755	.9321	•6766	8793	.7148	.9795	.9972	1.0050	1.0064	1.0006	.9998
.900	.753E+08	1.0038	1.3740	.9249	• 5949	•8669	.6877	.9911	.9978	1.0062	1.0074	1.0009	.9999
•950	.766E+U8	1.0036	1.3725	. 9175	• 5636	.8543	-5612	. 9978	.9968	1.0074	1.0065	1.0012	1.0000
1.000	•775E+08	1.0034	1.3709	• 90 9B	•5328	.8414	.6348	1.0000	.9967	1.0086	1.0097	1.0014	1.0000
1.050	.782E+08	1.0032	1.3693	.9020	.5028	.8284	.6087	.9981	•9966	1.0100	1.0110	1.0016	1.0001
1.100	.786E+08	1.0031	1.3675	.8941	47٬5	.8152	•5826	.9920	.9964	1.0111	1.0124	1.0015	.9999
1.150	.787E+08	1.0029	1.3657	.8861	.4453	.8019	•5570	. 9827	•9964	1.0125	1.0140	1.0015	•9999
1.200	.786E+08	1.0027	1.3638	.8779	.4182	.7885	.5320	.9784	.9963	1.0141	1.0156	1.0017	.9999
1.250	.783E+D8	1.0026	1.3619	.8697	.3921	•7752	.5075	.9553	.9963	1.0157	1.0174	1.0017	.9999
1.300	.778E+08	1.8024	1.3600	.8614	.3672	.7618	.4837	.9779	.9964	1.0175	1.0193	1.0017	1.0901
1.350	.771E+08	1.0033	1.3550	.8531	.3434	.7484	•4605	.9182	.9965	1.0191	1.0212	1.0015	.9999
1.400	.762E+08	1.0021	1.3561	.8447	.3207	.7351	.4379	.8967	.9967	1.0207	1.0233	1.0012	.9998
1.450	.752E+08	1.0020	1.3541	•B364	.2992	.7219	•4161	.8737	•9969	1.0222	1.0255	1.0007	. 9995
1.500	.740E+08	1.0019	1.3522	.8261	.2789	.7088	.3950	.8495	.9971	1.0237	1.0278	1.0001	.9991
1.550	.727E+08	1.0017	1.3504	. 51 98	.2596	•6958	.3747	. 8243	•9974	1.0251	1.0301	.9993	.9987
1.600	.713E+08	1.0016	1.3485	.8115	.2415	-6829	3551	.7983	9978	1.0263	1.0325	.9983	.9961
1.650	•699E+08	1.0015	1.3468	.8032	.2244	.6701	.3364	.7719	9982	1.0276	1.0350	.9973	.9974
1.700	.683E+08	1.8814	1.3451	.7951	.2084	.6575	3184	.7451	9987	1.0287	1.0375	•996 D	.9967
1.750	.667E+08	1.0013	1.3436	.7569	+19*3	•6450	.3011	.7100	.9993	1.0293	1.0400	9943	.9955
n na e	-6505+08	1 0012	4 7/.22	7700	4.700	6705	2016		2000				